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NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

TECHNICAL NOTE

No. 1143

CHARTS FOR DETERMINING THE CHARACTERISTICS OF
SHARP-NOSE AIRFOILS IN TWO-DIMENSIONAL
FLOW AT SUPERSONIC SPEEDS

By H. Reese Ivey, George W. Stickle,
and Alberta Schuettler

Langley Memorial Aeronautical Laboratory
Langley Field, Va.

FOR REFERENCE



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SUMMARY

Solutions of the Hugoniot shock equations and Meyer expansion equations are plotted in such a manner as to permit the pressure distribution, the local Mach number, and the angles of shock waves on arbitrary sharp-nose airfoils at supersonic speeds to be obtained directly.

INTRODUCTION

Ackeret, in reference 1, gives a method for calculating the pressure distribution over thin, sharp, two-dimensional airfoils at supersonic speeds. This method, based on the theory of small disturbances, is only a first approximation and therefore is most accurate for thin airfoils.

The exact relationship for the pressure rise through a normal shock wave, as given by Hugoniot, is discussed in reference 2. According to reference 3, the corresponding relations which apply directly to the pressures on a straight surface of an airfoil immediately behind an oblique shock were obtained by Meyer as early as 1908. A discussion of Meyer's equations for the expansion of supersonic flow around an infinite corner is also given in reference 3. Frequently, interference exists between

shock and expansion waves caused by the intersection of two or more of these waves. When this intersection is close to the airfoil, as, for instance, when the airfoil has considerable curvature, the calculations yielded by the aforementioned equations are not exact.

It has been shown by Ferri (reference 4) that the equations for an oblique shock combined with the expansion equations give a close approximation to experimental results as reviewed in the section "Presentation of Figures" in this report. The use of the equations, however, involves long and difficult computations. The purpose of this paper is to give graphic solutions of these equations in a form suitable for rapid calculation. Because the size of the graphs limits their accuracy, tables are given from which computational graphs of much greater accuracy may be plotted. The relations given herein apply directly to a two-dimensional, or cylindrical, flow in which the transverse velocity is supersonic. As pointed out by Buserann (reference 5) they may be adapted to the case of oblique motion of the cylindrical airfoil by the addition of an arbitrary axial velocity. Thus, as in reference 5, the relations may be applied to the case of a swept-back airfoil lying ahead of the Mach lines, in which case the velocities and Mach numbers used in the calculation are those corresponding to the transverse component of the flight velocity. In case the airfoil is swept behind the Mach lines the flow will be of a different type as discussed in reference 6.

SYMBOLS

M	Mach number
p	static pressure
q	dynamic pressure
β	change in direction of flow (see fig. 1)
γ	ratio of specific heat at constant pressure to specific heat at constant volume = 1.4 for air
θ	angle of shock wave relative to direction of flow before shock

v angle around which the flow would have to expand from $M = 1$ to the given local Mach number

p density of gas

Subscripts:

a for conditions after a disturbance

b for conditions before a disturbance

n for local condition under consideration

o free stream

PRESENTATION OF FIGURES

A supersonic two-dimensional air flow around an airfoil may change its direction either by deflection or by expansion around a corner. In case the change in air-flow direction occurs by deflection, a shock wave is set up, and in case the change is by expansion, an expansion wave is set up. In either case, the change of state of the gas can be presented as a function of the local Mach number before the disturbance and the change in direction of the gas.

The equations from which the charts presented herein are derived are given in the appendix. Values of local Mach number, pressure ratio, and pressure coefficient across shock waves are given in table I. The local Mach numbers before and after expansions are presented in table II and the static relations across expansion waves, in table III. Table IV gives the pressure ratios based on free-stream dynamic pressure for various Mach numbers.

Before the method of determining pressure distribution, lift, drag, and moments may be discussed, a method of measuring the angles that cause expansions and shocks must be selected. Figure 1 shows the method used in the present paper for measuring angles causing expansions; figure 2 shows that for measuring angles causing shocks. The angle causing the disturbance is designated β in both cases; β is considered negative if the disturbance set up is an expansion wave and positive if it is a shock wave.

Figure 3 shows the manner in which the flow changes when the angles are made too large for the given speeds. If the angle causing the shock is too great, the shock wave separates from the airfoil surface. In figure 4 are given the maximum angles that may exist before the shock wave separates, calculated as the boundary condition between the region giving two solutions and the region for which no solution exists. If the trailing portion of the airfoil is too blunt, the flow may separate from the airfoil and leave a turbulent wake. Figure 3(b) shows that the expansion of the flow outside the wake is actually less than it would have been had it followed the surface. The pressure on the back of the airfoil does not decrease so much as it would if the flow failed to separate. The drags calculated if no separation is assumed will therefore be higher than those actually experienced.

The local Mach number after a disturbance (shock or expansion) is shown in figure 5 to be a function of the local Mach number before the disturbance and the angle causing the disturbance. For example, if a flow at a Mach number of 4.0 impinges on a surface set at 5° to that flow, a shock wave is set up behind which the local Mach number is 3.64, while the flow behind the shock wave is parallel to the surface. On the other hand, the same flow expanding around a 5° corner produces a local Mach number equal to 4.4 on the surface behind the expansion.

Figure 6 gives the ratio of static pressures across shock and expansion waves. For example, assume that a flow at a local Mach number of 4.0 is shocked by a surface slope change of $\beta = 5^\circ$. From figure 6 the pressure ratio across the shock is 1.61, which means that the pressure is much higher on the surface behind the shock than on the surface before it. If the flow at $M = 4.0$ had expanded 5° , then the pressure would have dropped to 0.588. From this example it is seen that the 5° shock increased the pressure by 61 percent, whereas the 5° expansion decreased the pressure only 41 percent. Ackeret's method in reference 1 predicts equal changes in pressure for both the shock and the expansion, since it is based on small disturbances. Present results indicate, therefore, that angles as large as 5° require a more accurate approximation than that given by Ackeret.

The use of figures 5 and 6 can be demonstrated by solving for the local Mach numbers and pressures on the simple airfoil shown in figure 7. The coordinates of figures 5 and 6 are based on conditions before the disturbance and conditions after the disturbance. In figure 7 the conditions after one disturbance are noted to be the conditions before another disturbance. The numerical subscripts found in the symbols of figure 7 are to be associated, therefore, for use in the charts of figures 5 and 6, with the subscripts a and b, according to their relative positions with respect to the disturbance. The airfoil of figure 7 is a symmetrical, double-wedge airfoil having a 2° included angle at the leading and trailing edges. For use in this example the airfoil is at a positive angle of attack of 3° and is moving at a free-stream Mach number of 4.0. The pertinent angles as well as the conditions to be determined are shown on figure 7.

Enter figure 5 at $M_0 = 4.0$ and $\beta_1 = -2^{\circ}$, and read off $M_1 = 4.16$. This Mach number is used to obtain $M_2 = 4.33$. Values for the lower surface of the airfoil are obtained in a similar manner. At coordinates of $M_0 = 4.0$ and $\beta_3 = 4^{\circ}$, $M_3 = 3.70$; and, similarly, when the flow at M_3 is expanded 2° , M_4 is found to be 3.84. A shock wave and an expansion wave are shown at the trailing edge; however, since these disturbances do not affect the pressures on the airfoil, they will be neglected, and M_1 , M_2 , M_3 , and M_4 are the only Mach numbers which are discussed.

The pressure ratios across the shock and expansion waves can be determined from figure 6. Enter figure 6 at $M_0 = 4.0$ and an expansion angle of 2° and read

$\frac{p_1}{p_0} = 0.817$. At coordinates of $M_1 = 4.16$ and $\beta_2 = -2^{\circ}$, $\frac{p_2}{p_1}$ is found to be 0.809. Then

$$\frac{p_2}{p_0} = \frac{p_1}{p_0} \frac{p_2}{p_1} = 0.817 \times 0.809 = 0.661$$

For the lower surface of the airfoil, p_3/p_0 is found at coordinates $M_0 = 4.0$, $\beta_3 = 4^\circ$ to be $\frac{p_3}{p_0} = 1.47$.

At $M_3 = 3.70$, $\beta_4 = -2^\circ$, $\frac{p_4}{p_3} = 0.829$. Then

$$\frac{p_4}{p_0} = \frac{p_4}{p_3} \times \frac{p_3}{p_0} = 1.219$$

The pressure ratios $\frac{p_a}{p_b}$ may be converted to local pressure coefficients $\frac{\Delta p}{q_0}$ by the use of the plot given in figure 8. The results obtained for the local Mach numbers, pressure ratios, and pressure coefficients are illustrated in figure 9.

Once the pressure distribution is determined, the lift, drag, and moment coefficients can be obtained by integrating plots of the types given in figures 10, 11, and 12. The lift coefficient is obtained by integrating the projection of the airfoil pressure distribution on a plane parallel to free-stream direction. For the example airfoil at Mach number 4.0 and angle of attack 3° , the lift coefficient is 0.0540. The drag coefficient is found in the same manner except that the integration is over the projection of the airfoil pressure distribution on a plane perpendicular to free stream. The pressure drag coefficient for the example airfoil is 0.00315. The total section drag coefficient is the sum of the viscous and pressure-drag coefficients; for instance, if the viscous-drag coefficient is 0.0060, then the total drag coefficient is $0.0060 + 0.00315 = 0.00915$. The moment coefficient, obtained by integrating the elemental moments about the point desired, becomes 0.001112 when taken about the center for the example airfoil.

In the preceding examples step-by-step calculations were made along the airfoil, in which case the results obtained at any point are dependent on the accuracy of those at the preceding points. The results thus obtained on the rear of the airfoil may be subject to greater inaccuracies than are necessary. A method is consequently

given for determining the conditions behind each of a series of expansions independently of the conditions existing at intermediate points. For the example airfoil of figure 7, the free-stream flow was expanded around a 2° corner to obtain the conditions on the front of the upper surface and these conditions were then expanded around the second 2° corner to give the conditions on the rear of the upper surface. These last conditions, however, could have been found directly by referring the rear of the upper surface to the free-stream conditions and expanding through the total angle (4°) at once. Theoretically the results obtained are exactly the same regardless of which method is used, provided no shock waves are present between the end-points of the calculation. This method of adding angles does not apply when there are intermediate shock waves because of loss of total head in the shock wave.

If it is desired to calculate only the pressure distribution, it is not necessary to find M_1 , M_2 , $M_{1\perp}$, or p_2/p_1 for an airfoil similar to the type in the example given.

Figure 13 is taken from reference 4 to compare the experimental pressure distribution on an airfoil with the calculated distribution. Even though the wind-tunnel tests were of a very small model and although the airfoil is not of a type particularly suitable for calculations, the calculated and experimental values seem to compare favorably except for the region of separated flow near the upper trailing edge of the airfoil. The method of the present report is not exact for an airfoil of this type, which has considerable curvature along its entire length. The inaccuracy caused by the curvature, however, seems to be small. The thickness ratio and angle of attack of the example airfoil are somewhat higher than those for which the method is recommended. Reference 4 explains the separated region of flow.

Langley Memorial Aeronautical Laboratory
National Advisory Committee for Aeronautics
Langley Field, Va., April 4, 1946

APPENDIX

METHOD OF ANALYSIS

Shock Waves

Supersonic air flow about an airfoil may be said to consist of expansions and shocks. Reference 2 mentions the fact that a change in entropy occurs through a shock wave. Three conditions are shown, however, to apply to the velocities, pressures, and densities at the two sides of the shock wave, namely:

- (a) Continuity of mass
- (b) Balance between pressure difference and change of momentum
- (c) Conservation of energy

These conditions lead to the three basic equations:

or

$$\frac{\rho_a}{\rho_b} = \frac{\tan \theta}{\tan (\theta - \beta)} \quad \left. \begin{array}{l} \\ \end{array} \right\} (1)$$

$$\frac{\Delta P}{P_a} = \frac{\sin \beta}{\sin \theta \times \cos (\theta - \beta)}$$

$$\left. \begin{array}{l} \frac{\Delta P}{P_b} = 2 \sin^2 \theta \frac{\Delta P}{P_a} \\ = \frac{2 \sin \beta \times \sin \theta}{\cos (\theta - \beta)} \end{array} \right\} (2)$$

$$\frac{\Delta p}{\Delta \rho} = \gamma \frac{p_b + \frac{\Delta p}{2}}{p_b - \frac{\Delta p}{2}} \quad (3)$$

Then, by use of the relation

$$\frac{\Delta p}{q_b} = \frac{2}{\gamma M_b^2} \left(\frac{p_a}{p_b} - 1 \right) \quad (4)$$

it follows that

$$\frac{p_a}{p_b} = \frac{\gamma M_b^2 \sin \beta \sin \theta}{\cos(\theta - \beta)} + 1 \quad (5)$$

$$\frac{1}{M_b^2} = \sin^2 \theta - \frac{\gamma + 1}{2} \frac{\sin \beta \sin \theta}{\cos(\theta - \beta)} \quad (6)$$

$$M_a = M_b \frac{\cos \theta}{\cos(\theta - \beta)} \sqrt{\frac{p_b}{p_a} \frac{\rho_a}{\rho_b}} \quad (7)$$

By substitution of arbitrary values of θ and β in equations (1) and (6), the corresponding values of density ratio across the shock and Mach number before the shock are obtained. If the simultaneous values of θ , β , and M_b are used with equations (5) and (7), the pressure ratio across the shock and the Mach number after the shock are obtained.

Figure 14 shows the angle of the shock wave as a function of the Mach number before the shock M_b and the angle defining the change in direction of the flow β .

The pressure ratios and the Mach numbers after the shock have already been discussed for figures 5 and 6. Use of the ratio of pressure after any shock wave to free-stream static pressure, together with free-stream Mach number in equation (4), makes possible the determination of the pressure coefficient behind that shock wave. Figure 8 has shown the graph for converting pressure ratios to pressure coefficients.

Expansion Waves

The flow after the shock wave may be considered adiabatic as long as the flow is expanding. By the use of such flow conditions, the velocities, densities, and pressures may be calculated. Experimentally some trouble is encountered when extremely large angles of expansion are used. The flow may break down and form a turbulent wake of somewhat higher static pressure than might be expected if the flow had continued to expand around the corner.

Reference 3 considers that a flow at a Mach number of 1 expands around some angle v and reaches a higher Mach number M defined by the relation

$$v = \sqrt{\frac{\gamma + 1}{\gamma - 1}} \tan^{-1} \left(\sqrt{M^2 - 1} \sqrt{\frac{\gamma - 1}{\gamma + 1}} \right) - \cos^{-1} \frac{1}{M} \quad (8)$$

By expanding around an angle v_b , the flow reaches a Mach number M_b ; and by expanding around some larger angle v_a , the flow reaches some higher Mach number M_a . A flow at the first Mach number M_b can then reach the higher Mach number M_a by expanding around the small angle,

$$-\beta = v_a - v_b \quad (9)$$

Equations (8) and (9) serve as the basis for calculating the expansion lines in figure 5 showing the variation of local Mach number with change in surface slope.

Another equation derived from the work of reference 3 gives the pressure ratio across expansion waves as

$$\frac{p_a}{p_b} = \left[\frac{2 + (\gamma - 1) M_b^2}{2 + (\gamma - 1) M_a^2} \right]^{\frac{\gamma}{\gamma-1}} \quad (10)$$

From equations (5), (9), and (10), it is possible to calculate the part of figure 6 that gives the pressure ratio across expansion waves as a function of the local Mach number before the expansion and the change in surface slopes.

The figures shown in this report, because of their limited size, may not be accurate enough for routine calculations. It may be desirable to plot the graphs to a larger scale before using them. For this reason the values are listed in tabular form for the main graphs.

Tables I and II should be accurate to all the figures shown, but table II may not be exact in the last figure since the expansion calculations required graphical interpolation between very close computed points.

REFERENCES

1. Ackeret, J.: Air Forces on Airfoils Moving Faster than Sound. NACA TM. 317, 1925.
2. von Kármán, Th.: The Problem of Resistance in Compressible Fluids. GALCIT Pub. No. 75, 1936.
(From R. Accad. d'Italia, cl. sci. fis., mat. e nat., vol. XJV, 1936.)
3. Taylor, G. I. and MacColl, J. W.: The Mechanics of Compressible Fluids. Two-Dimensional Flow at Supersonic Speeds. Vol. III of Aerodynamic Theory div. H, ch. IV, w. F. Durand, ed., Julius Springer (Berlin), 1935. pp. 238-245.
4. Ferri, Antonio: Experimental Results with Airfoils Tested in the High-Speed Tunnel at Guidonia. NACA TM No. 946, 1940.
5. Busemann, A.: Aerodynamic Lift at Supersonic Speeds. 2844, Ae. Techl. 1201, British A.P.C., Feb. 3, 1937.
(From Luftfahrtforschung, Bd. 12, Nr. 6, Oct. 3, 1935, pp. 210-220.)
6. Jones, Robert T.: Properties of Low-Aspect-Ratio Pointed Wings at Speeds below and above the Speed of Sound. NACA TN No. 1032, 1946.

use supplement

TABLE I.- VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO,
AND PRESSURE COEFFICIENT ACROSS SHOCK WAVES

θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_a, b}{q_b}$	θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_a, b}{q_b}$
8	0	7.18516	7.18516	1.00000	0	16	6	4.91653	4.35137	2.00221	0.05891
8	10	7.180125	7.54749	1.20824	.00120	8	7	5.33220	4.25154	2.85426	0.06803
8	20	8.60435	8.07261	1.50622	.00977	9	8	5.82225	4.79190	2.83915	0.07118
8	30	6.39264	6.39264	1.00000	0	10	9	6.47621	5.08655	3.595104	0.08699
8	40	6.39264	7.06779	1.42052	.01241	11	10	7.40814	5.15671	4.69797	0.09636
8	50	8.21634	7.54385	1.47881	.01646	12	11	8.00088	5.155816	6.85594	0.10559
8	60	5.75876	5.75876	1.00000	0	13	12	4.2032	3.12032	1.00000	0
8	70	6.16267	5.95876	1.02126	.00614	14	13	5.5532	4.91038	1.09391	0.10631
8	80	6.61119	6.20817	1.27585	.01241	15	14	6.62125	5.27318	1.20313	0.02133
8	90	6.61119	7.16849	1.0132	.0132	16	15	6.62125	5.27318	1.20313	0.02133
10	0	7.12344	7.12344	1.00000	0	17	17	7.40814	5.15671	4.69797	0.09636
10	10	7.02263	7.10485	2.02372	.02372	18	18	4.2032	3.12032	1.00000	0
10	20	5.21082	5.21082	1.00000	0	19	19	5.5532	4.91038	1.09391	0.10631
10	30	5.55967	5.42448	1.14669	.00676	20	20	6.62125	5.27318	1.20313	0.02133
10	40	6.04237	6.04237	1.01419	.01419	21	21	6.62125	5.27318	1.20313	0.02133
10	50	6.04237	7.75948	1.02829	.02829	22	22	6.62125	5.27318	1.20313	0.02133
10	60	6.04237	8.35611	2.41547	.041547	23	23	6.62125	5.27318	1.20313	0.02133
11	0	5.21082	5.21082	1.00000	0	24	24	6.62125	5.27318	1.20313	0.02133
11	10	5.55967	5.42448	1.14669	.00676	25	25	6.62125	5.27318	1.20313	0.02133
11	20	6.04237	6.04237	1.01419	.01419	26	26	6.62125	5.27318	1.20313	0.02133
11	30	6.04237	7.75948	1.02829	.02829	27	27	6.62125	5.27318	1.20313	0.02133
11	40	6.04237	8.35611	2.41547	.041547	28	28	6.62125	5.27318	1.20313	0.02133
12	0	9.80977	9.80977	1.00000	0	29	29	6.62125	5.27318	1.20313	0.02133
12	10	9.07359	9.69551	1.13314	.00739	30	30	6.62125	5.27318	1.20313	0.02133
12	20	9.07359	9.29378	1.29217	.02921	31	31	6.62125	5.27318	1.20313	0.02133
12	30	9.07359	9.29378	1.29217	.02921	32	32	6.62125	5.27318	1.20313	0.02133
12	40	9.07359	9.29378	1.29217	.02921	33	33	6.62125	5.27318	1.20313	0.02133
13	0	6.80911	6.80911	1.00000	0	34	34	6.62125	5.27318	1.20313	0.02133
13	10	8.55172	8.05282	1.05087	.05087	35	35	6.62125	5.27318	1.20313	0.02133
13	20	6.80911	6.80911	1.00000	0	36	36	6.62125	5.27318	1.20313	0.02133
13	30	6.80911	6.80911	1.00000	0	37	37	6.62125	5.27318	1.20313	0.02133
13	40	6.80911	6.80911	1.00000	0	38	38	6.62125	5.27318	1.20313	0.02133
14	0	4.44543	4.44543	1.00000	0	39	39	6.62125	5.27318	1.20313	0.02133
14	10	4.44543	4.44543	1.00000	0	40	40	6.62125	5.27318	1.20313	0.02133
14	20	4.44543	4.44543	1.00000	0	41	41	6.62125	5.27318	1.20313	0.02133
14	30	4.44543	4.44543	1.00000	0	42	42	6.62125	5.27318	1.20313	0.02133
14	40	4.44543	4.44543	1.00000	0	43	43	6.62125	5.27318	1.20313	0.02133
15	0	6.21350	6.21350	1.00000	0	44	44	6.62125	5.27318	1.20313	0.02133
15	10	5.32439	5.32439	1.12771	.012771	45	45	6.62125	5.27318	1.20313	0.02133
15	20	5.32439	5.32439	1.12771	.012771	46	46	6.62125	5.27318	1.20313	0.02133
15	30	5.32439	5.32439	1.12771	.012771	47	47	6.62125	5.27318	1.20313	0.02133
15	40	5.32439	5.32439	1.12771	.012771	48	48	6.62125	5.27318	1.20313	0.02133
15	50	5.32439	5.32439	1.12771	.012771	49	49	6.62125	5.27318	1.20313	0.02133
15	60	5.32439	5.32439	1.12771	.012771	50	50	6.62125	5.27318	1.20313	0.02133
15	70	5.32439	5.32439	1.12771	.012771	51	51	6.62125	5.27318	1.20313	0.02133
15	80	5.32439	5.32439	1.12771	.012771	52	52	6.62125	5.27318	1.20313	0.02133
15	90	5.32439	5.32439	1.12771	.012771	53	53	6.62125	5.27318	1.20313	0.02133
15	100	5.32439	5.32439	1.12771	.012771	54	54	6.62125	5.27318	1.20313	0.02133
16	0	3.86369	3.86369	1.00000	0	55	55	6.62125	5.27318	1.20313	0.02133
16	10	4.44543	4.44543	1.00000	0	56	56	6.62125	5.27318	1.20313	0.02133
16	20	4.44543	4.44543	1.00000	0	57	57	6.62125	5.27318	1.20313	0.02133
16	30	4.44543	4.44543	1.00000	0	58	58	6.62125	5.27318	1.20313	0.02133
16	40	4.44543	4.44543	1.00000	0	59	59	6.62125	5.27318	1.20313	0.02133
16	50	4.44543	4.44543	1.00000	0	60	60	6.62125	5.27318	1.20313	0.02133
16	60	4.44543	4.44543	1.00000	0	61	61	6.62125	5.27318	1.20313	0.02133
16	70	4.44543	4.44543	1.00000	0	62	62	6.62125	5.27318	1.20313	0.02133
16	80	4.44543	4.44543	1.00000	0	63	63	6.62125	5.27318	1.20313	0.02133
16	90	4.44543	4.44543	1.00000	0	64	64	6.62125	5.27318	1.20313	0.02133
16	100	4.44543	4.44543	1.00000	0	65	65	6.62125	5.27318	1.20313	0.02133
17	0	3.62792	3.62792	1.00000	0	66	66	6.62125	5.27318	1.20313	0.02133
17	10	3.62792	3.62792	1.00000	0	67	67	6.62125	5.27318	1.20313	0.02133
17	20	3.62792	3.62792	1.00000	0	68	68	6.62125	5.27318	1.20313	0.02133
17	30	3.62792	3.62792	1.00000	0	69	69	6.62125	5.27318	1.20313	0.02133
17	40	3.62792	3.62792	1.00000	0	70	70	6.62125	5.27318	1.20313	0.02133
17	50	3.62792	3.62792	1.00000	0	71	71	6.62125	5.27318	1.20313	0.02133
17	60	3.62792	3.62792	1.00000	0	72	72	6.62125	5.27318	1.20313	0.02133
17	70	3.62792	3.62792	1.00000	0	73	73	6.62125	5.27318	1.20313	0.02133
17	80	3.62792	3.62792	1.00000	0	74	74	6.62125	5.27318	1.20313	0.02133
17	90	3.62792	3.62792	1.00000	0	75	75	6.62125	5.27318	1.20313	0.02133
17	100	3.62792	3.62792	1.00000	0	76	76	6.62125	5.27318	1.20313	0.02133
18	0	3.62792	3.62792	1.00000	0	77	77	6.62125	5.27318	1.20313	0.02133
18	10	3.62792	3.62792	1.00000	0	78	78	6.62125	5.27318	1.20313	0.02133
18	20	3.62792	3.62792	1.00000	0	79	79	6.62125	5.27318	1.20313	0.02133
18	30	3.62792	3.62792	1.00000	0	80	80	6.62125	5.27318	1.20313	0.02133
18	40	3.62792	3.62792	1.00000	0	81	81	6.62125	5.27318	1.20313	0.02133
18	50	3.62792	3.62792	1.00000	0	82	82	6.62125	5.27318	1.20313	0.02133
18	60	3.62792	3.62792	1.00000	0	83	83	6.62125	5.27318	1.20313	0.02133
18	70	3.62792	3.62792	1.00000	0	84	84	6.62125	5.27318	1.20313	0.02133
18	80	3.62792	3.62792	1.00000	0	85	85	6.62125	5.27318	1.20313	0.02133
18	90	3.62792	3.62792	1.00000	0	86	86	6.62125	5.27318	1.20313	0.02133
18	100	3.62792	3.62792	1.00000	0	87	87	6.62125	5.27318	1.20313	0.02133
19	0	3.62792	3.62792	1.00000	0	88	88	6.62125	5.27318	1.20313	0.02133
19	10	3.62792	3.62792	1.00000	0	89	89	6.62125	5.27318	1.20313	0.02133
19	20	3.62792	3.62792	1.00000	0	90	90	6.62125	5.27318	1.20313	0.02133
19	30	3.62792	3.62792	1.00000	0	91	91	6.62125	5.27318	1.20313	0.02133
19	40	3.62792	3.62792	1.00000	0	92	92	6.62125	5.27318	1.20313	0.02133
19	50	3.62792	3.62792	1.00000	0	93	93	6.62125	5.27318	1.20313	0.02133
19	60	3.62792	3.62792	1.00000	0	94	94	6.62125	5.27318	1.20313	0.02133
19	70	3.62792	3.62792	1.00000	0	95	95				

TABLE I.- VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO,
AND PRESSURE COEFFICIENT ACROSS SHOCK WAVES - Continued

θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_{a,b}}{q_o}$	θ (deg)	β (deg.)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_{a,b}}{q_o}$
21	0	2.79041	2.79041	1.00000	0	25	0	2.36619	2.36619	1.00000	0
	1	2.88113	2.83236	1.07736	.01331		1	2.13311	2.39158	1.06692	.016149
	2	2.98066	2.87953	1.16450	.02645		2	2.50490	2.42023	1.14078	.032053
	3	3.08951	2.93252	1.26352	.03914		3	2.58255	2.45239	1.22268	.047767
	4	3.20981	2.99660	1.37704	.05228		4	2.66584	2.48815	1.31121	.063162
	5	3.34375	3.05910	1.50857	.06498		5	2.75692	2.52825	1.41711	.078398
	6	3.47911	3.12563	1.64697	.07636		6	2.85665	2.57296	1.53377	.093442
	7	3.66576	3.22034	1.84678	.09002		7	2.96666	2.62291	1.66728	.10831
	8	3.86318	3.31777	2.06948	.10237		8	3.08899	2.67881	1.82163	.12301
	9	4.09428	3.42921	2.31504	.11633		9	3.22162	2.71136	2.00218	.13755
	10	4.37040	3.55785	2.63520	.12679		10	3.38185	2.81164	2.21653	.15196
	11	4.70837	3.70460	3.15498	.13887		11	3.56060	2.89100	2.47509	.16622
	12	5.13650	3.88429	3.78653	.15088		12	3.76908	2.98103	2.79352	.18036
	13	5.70365	4.09575	4.70770	.16282		13	4.01684	3.08381	3.19547	.19438
	14	6.50821	4.35408	6.17984	.17470		14	4.31849	3.20211	3.71940	.20831
	15	7.78248	4.67778	8.90838	.18653		15	4.69712	3.33960	4.43072	.22214
22	0	2.66944	2.66944	1.00000	0	26	0	2.28118	2.28118	1.00000	0
	1	2.75318	2.70503	1.07435	.014012		1	2.34464	2.30339	1.06582	.01710
	2	2.84397	2.74795	1.15755	.027827		2	2.41071	2.32980	1.13624	.03349
	3	2.94508	2.79153	1.25145	.044472		3	2.48294	2.35720	1.21505	.04585
	4	3.05197	2.84677	1.35832	.056956		4	2.55991	2.38997	1.30255	.06595
	5	3.17212	2.90542	1.48108	.068287		5	2.64389	2.42442	1.40051	.08165
	6	3.30680	2.97131	1.62361	.081470		6	2.73534	2.46403	1.51078	.09752
	7	3.45826	3.04552	1.79138	.094530		7	2.83560	2.50808	1.63601	.11300
	8	3.63087	3.12950	1.99170	.10746		8	2.91639	2.55727	1.77964	.12830
	9	3.83033	3.22198	2.23535	.12029		9	3.06978	2.61226	1.94606	.14342
	10	4.06462	3.33411	2.53821	.13301		10	3.20634	2.64370	2.14123	.15838
	11	4.34571	3.45998	2.92528	.14564		11	3.36613	2.74282	2.57366	.17319
	12	4.69181	3.60650	3.43731	.15817		12	3.54771	2.82071	2.65513	.18786
	13	5.13349	3.77921	4.14768	.17065		13	3.76027	2.90907	3.00338	.20441
	14	5.72501	3.98579	5.19945	.18304		14	4.00005	2.99945	3.44555	.21855
	15	6.57835	4.23809	6.91836	.19538		15	4.32457	3.10529	4.02623	.23116
23	0	2.55931	2.55931	1.00000	0	27	0	2.20269	2.20269	1.00000	0
	1	2.63663	2.59191	1.07155	.014703		1	2.31209	2.30158	1.06314	.01644
	2	2.72021	2.62864	1.15151	.029212		2	2.40696	2.32166	1.13222	.03260
	3	2.81097	2.66964	1.24071	.043519		3	2.48322	2.35717	1.20820	.04823
	4	2.91011	2.71559	1.34175	.057649		4	2.55095	2.37983	1.29226	.06416
	5	3.01917	2.76708	1.45693	.071610		5	2.73159	2.41239	1.38571	.07958
	6	3.14004	2.82478	1.58952	.085411		6	2.71871	2.44871	1.49044	.09479
	7	3.27510	2.88954	1.74381	.099068		7	2.81393	2.48911	1.60857	.10980
	8	3.42766	2.95435	1.92598	.11259		8	2.91652	2.53412	1.74297	.12461
	9	3.60192	3.04481	2.14416	.12628		9	3.03424	2.58826	1.89742	.13925
	10	3.80388	3.13837	2.41057	.13927		10	3.16334	2.64029	2.07680	.15373
	11	4.04200	3.24533	2.74332	.15214		11	3.30871	2.70290	2.28776	.16804
	12	4.32897	3.36862	3.17120	.16551		12	3.47453	2.77291	2.53991	.18222
	13	4.68441	3.51192	3.71484	.17850		13	3.66599	2.85242	2.84643	.19627
	14	5.11181	3.68084	4.51240	.19141		14	3.89094	2.94227	3.22752	.21019
	15	5.76160	3.88284	5.74606	.20424		15	4.16067	3.04466	3.71441	.22400
24	0	2.45857	2.45857	1.00000	0	28	0	2.13006	2.13006	1.00000	0
	1	2.53038	2.48739	1.06915	.015428		1	2.18546	2.11729	1.06148	.01839
	2	2.60761	2.51974	1.14573	.030617		2	2.24436	2.16698	1.12856	.03616
	3	2.69120	2.55602	2.23122	.045607		3	2.30713	2.18917	1.20202	.05422
	4	2.78202	2.59660	1.32717	.060389		4	2.37434	2.21407	1.28293	.07170
	5	2.88137	2.64194	1.43578	.074985		5	2.44661	2.24198	1.37252	.08890
	6	2.99085	2.69267	1.55985	.089410		6	2.52465	2.27308	1.47228	.10585
	7	3.11235	2.74947	1.70294	.10367		7	2.60945	2.30767	1.58125	.12258
	8	3.24831	2.81309	1.86990	.11778		8	2.70205	2.34617	1.71071	.13906
	9	3.40126	2.88381	2.06753	.13183		9	2.89976	2.37065	1.85492	.14525
	10	3.57857	2.96549	2.30507	.14559		10	2.91678	2.45671	2.02095	.17413
	11	3.78354	3.05730	2.59633	.15930		11	3.04296	2.48992	2.21132	.18735
	12	4.02611	3.16209	2.96196	.17291		12	3.18538	2.54937	2.44239	.20308
	13	4.31993	3.28285	3.13525	.18642		13	3.34818	2.61606	2.71591	.21866
	14	4.80616	3.42514	4.07188	.19984		14	3.53684	2.69124	3.01990	.23410
	15	5.16169	3.58857	4.97574	.21317		15	3.75932	2.77640	3.16732	.24941

TABLE I.- VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO,
AND PRESSURE COEFFICIENT ACROSS SHOCK WAVES - Continued

θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_{a,b}}{q_0}$	θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_{a,b}}{q_0}$
29	0	2.06266	2.06266	1.00000	0.	36	0	1.70130	1.70130	1.00000	0
	1	2.11505	2.07774	1.06001	.01910		1	1.73955	1.70539	1.05304	.025040
	2	2.17054	2.09196	1.12523	.03797		2	1.77947	1.71085	1.10969	.049487
	3	2.22957	2.11155	1.19617	.05616		3	1.82126	1.71772	1.17023	.073358
	4	2.29236	2.13521	1.27431	.07457		4	1.86536	1.72606	1.23585	.096630
	5	2.36005	2.16131	1.36067	.09251		5	1.91119	1.73654	1.30563	.11953
	6	2.43270	2.18895	1.45616	.11011	38	6	1.95980	1.74734	1.38147	.14189
	7	2.51121	2.21966	1.56258	.12744		7	2.01121	1.76042	1.46381	.16580
	8	2.59661	2.25386	1.68225	.14455		8	2.06585	1.77522	1.55356	.18530
	9	2.69358	2.29151	1.82347	.16209		9	2.12402	1.79185	1.65178	.20639
	10	2.79292	2.33402	1.97234	.17808		10	2.18626	1.81048	1.75992	.22713
30	11	2.90717	2.38101	2.15090	.19454	38	11	2.25305	1.83118	1.87943	.24749
	12	3.03508	2.43337	2.35935	.21081		12	2.32517	1.86418	2.01251	.26754
	13	3.17954	2.49183	2.66602	.22690		13	2.40336	1.87960	2.16155	.28728
	14	3.34576	2.55740	2.90292	.24285		14	2.48870	1.90778	2.32982	.30673
	15	3.53866	2.63123	3.26710	.25864		15	2.58245	1.93889	2.52146	.32591
31	0	2.00000	2.00000	1.00000	0	40	0	1.62127	1.62127	1.00000	0
	1	2.04970	2.01309	1.05869	.01996		1	1.66000	1.62610	1.05191	.02691
	2	2.10220	2.02817	1.2228	.03953		2	1.69720	1.62925	1.10711	.05312
	3	2.15786	2.04536	1.19144	.05873		3	1.73595	1.63363	1.16595	.07867
	4	2.21712	2.06489	1.26708	.07743		4	1.77646	1.63934	1.22888	.10361
	5	2.28038	2.08676	1.35004	.09616		5	1.81891	1.64639	1.29635	.12796
	6	2.34624	2.11124	1.44166	.11142	40	6	1.86348	1.65484	1.36892	.15177
	7	2.412132	2.13857	1.54331	.13239		7	1.91042	1.66171	1.44727	.17507
	8	2.50046	2.16931	1.65693	.15010		8	1.95999	1.67607	1.53211	.19788
	9	2.58664	2.20259	1.78180	.16757		9	2.01354	1.68903	1.62441	.22023
	10	2.68100	2.24016	1.92978	.18479		10	2.06039	1.70361	1.72524	.24217
32	11	2.78510	2.28175	2.09572	.20180	40	11	2.12800	1.71998	1.83585	.26369
	12	2.90088	2.32799	2.28775	.21861		12	2.19194	1.73827	1.95797	.28484
	13	3.03082	2.37952	2.51256	.23523		13	2.26069	1.75819	2.09337	.30562
	14	3.17820	2.43701	2.77947	.25167		14	2.33512	1.77819	2.24461	.32607
	15	3.34766	2.50119	3.10201	.26795		15	2.41604	1.80577	2.41463	.34621
33	0	1.88707	1.88707	1.00000	0	40	0	1.55572	1.55572	1.00000	0
	1	1.93213	1.89664	1.05659	.02158		1	1.58940	1.55556	1.05106	.02887
	2	1.97956	1.90799	1.11716	.04271		2	1.62431	1.55660	1.10515	.05693
	3	2.02958	1.92112	1.18287	.06342		3	1.66120	1.55877	1.16355	.08167
	4	2.08253	1.93620	1.25420	.08373		4	1.69841	1.56224	1.22384	.11085
	5	2.13875	1.95330	1.33195	.10367		5	1.73791	1.56694	1.28916	.13677
	6	2.19868	1.97256	1.41711	.12326	40	6	1.77912	1.57276	1.35914	.16209
	7	2.26277	2.00680	1.51078	.14251		7	1.82243	1.57993	1.45451	.18681
	8	2.33163	2.01807	1.61145	.16146		8	1.86797	1.58841	1.51532	.21098
	9	2.40576	2.04478	1.72982	.18011		9	1.91577	1.59826	1.60291	.23462
	10	2.48665	2.07445	1.85915	.19849		10	1.96679	1.60950	1.69799	.25777
34	11	2.57171	2.10730	2.00522	.21662	42	11	2.02072	1.62230	1.80165	.28046
	12	2.67149	2.11373	2.17150	.23150		12	2.07818	1.63666	1.91519	.30272
	13	2.77856	2.18409	2.36269	.25215		13	2.13960	1.65272	2.04007	.32156
	14	2.89812	2.22897	2.58506	.26560		14	2.20564	1.67062	2.17838	.34603
	15	3.03292	2.27584	2.84700	.28684		15	2.27484	1.69040	2.33224	.36713
35	0	1.78829	1.78829	1.00000	0	42	0	1.49448	1.49448	1.00000	0
	1	1.82960	1.79193	1.05453	.023271		1	1.52616	1.49254	1.05017	.03094
	2	1.87291	1.80309	1.11302	.046028		2	1.55953	1.49172	1.10379	.06096
	3	1.94837	1.81285	1.17591	.060285		3	1.59084	1.48920	1.16026	.09046
	4	1.96630	1.82127	1.24532	.090089		4	1.63013	1.49331	1.22140	.11902
	5	2.01688	1.83741	1.31735	.11115		5	1.66642	1.49592	1.28389	.14604
	6	2.07054	1.85237	1.39734	.13240	42	6	1.70602	1.50047	1.35186	.17270
	7	2.12758	1.86926	1.48470	.15297		7	1.74533	1.50437	1.42453	.19909
	8	2.18819	1.88821	1.58061	.17318		8	1.78759	1.51037	1.50251	.22465
	9	2.25576	1.90935	1.68638	.19304		9	1.83196	1.51758	1.58642	.24962
	10	2.32103	1.93285	1.80374	.21259		10	1.87871	1.52603	1.67703	.27402
36	11	2.40006	1.95894	1.93476	.23182	42	11	1.92809	1.53583	1.77522	.29790
	12	2.48279	1.96794	2.08213	.25078		12	1.98043	1.54697	1.88207	.32128
	13	2.57339	2.01986	2.49293	.26948		13	2.03608	1.55958	1.99882	.34119
	14	2.67317	2.05523	2.50204	.26797		14	2.09550	1.57370	2.12706	.36667
	15	2.78406	2.07055	2.66102	.30614		15	2.15919	1.58941	2.26861	.38873

TABLE I.- VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO,
AND PRESSURE COEFFICIENT ACROSS SHOCK WAVES - Continued

θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_{a,b}}{q_0}$	θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_{a,b}}{q_0}$
44	0	1.43955	1.43955	1.00000	0	52	0	1.26902	1.26902	1.00000	0
	1	1.47017	1.43595	1.05016	.03325		1	1.29670	1.25918	1.0514	.04370
	2	1.50175	1.43540	1.10300	.06524		2	1.32498	1.25103	1.10516	.08557
	3	1.53433	1.43194	1.15878	.09634		3	1.35392	1.24361	1.16131	.12571
	4	1.56816	1.43151	1.21777	.12651		4	1.38359	1.23720	1.22017	.16430
	5	1.60320	1.43215	1.28033	.15581		5	1.41140	1.23173	1.28189	.20140
	6	1.63960	1.43385	1.34680	.18429		6	1.44536	1.22720	1.34680	.23715
	7	1.67754	1.43659	1.41765	.21202		7	1.47766	1.22354	1.41517	.27163
	8	1.71712	1.44014	1.49329	.23900		8	1.51097	1.22079	1.48728	.30491
	9	1.75655	1.44536	1.57435	.26532		9	1.54543	1.21981	1.56357	.33709
	10	1.80201	1.45143	1.66148	.29101		10	1.58114	1.21788	1.64446	.36826
	11	1.841775	1.45668	1.75542	.31608		11	1.61819	1.21814	1.73036	.39845
	12	1.88597	1.46707	1.85710	.34062		12	1.65677	1.21818	1.82188	.42775
	13	1.94702	1.47675	1.96754	.36461		13	1.69700	1.21989	1.91963	.45620
	14	2.00123	1.48774	2.08804	.37774		14	1.73905	1.22229	2.02439	.48364
	15	2.05902	1.50014	2.22011	.41113		15	1.78314	1.22557	2.13679	.51075
46	0	1.39016	1.39016	1.00000	0	54	0	1.23606	1.23606	1.00000	0
	1	1.41969	1.38498	1.05010	.03551		1	1.26353	1.22509	1.05243	.04691
	2	1.45008	1.38088	1.10274	.06980		2	1.29155	1.21520	1.10710	.09172
	3	1.48138	1.37779	1.15815	.10294		3	1.32018	1.20650	1.16416	.13456
	4	1.51372	1.37573	1.21661	.13505		4	1.34943	1.19873	1.22383	.17560
	5	1.54715	1.37464	1.27839	.16615		5	1.37942	1.19190	1.28831	.21495
	6	1.58181	1.37460	1.31384	.19631		6	1.41018	1.18607	1.35186	.25277
	7	1.61778	1.37540	1.42234	.22562		7	1.44181	1.18109	1.42075	.28914
	8	1.65521	1.37744	1.48728	.25408		8	1.47440	1.17701	1.49329	.32417
	9	1.69426	1.38037	1.56626	.28181		9	1.50801	1.17379	1.56982	.35796
	10	1.73507	1.38431	1.65076	.30881		10	1.54274	1.17135	1.65074	.39059
	11	1.77783	1.38936	1.74144	.33512		11	1.57871	1.16378	1.73648	.42214
	12	1.82273	1.39545	1.83915	.36080		12	1.61605	1.16899	1.82758	.45269
	13	1.87015	1.40266	1.94174	.38589		13	1.65487	1.16904	1.92455	.48229
	14	1.92023	1.41102	2.05931	.41041		14	1.69536	1.17087	2.02809	.51099
	15	1.97330	1.42055	2.18408	.45441		15	1.73765	1.17155	2.13897	.53888
48	0	1.34562	1.34562	1.00000	0	56	0	1.20621	1.20621	1.00000	0
	1	1.37431	1.33697	1.05028	.03803		1	1.23369	1.19378	1.05375	.05045
	2	1.40376	1.33334	1.10299	.07166		2	1.26160	1.18252	1.10263	.09845
	3	1.43404	1.32876	1.15835	.11000		3	1.29013	1.17236	1.16799	.14119
	4	1.46522	1.32515	1.21660	.14413		4	1.31923	1.16331	1.22687	.18787
	5	1.49738	1.32253	1.27799	.17712		5	1.34896	1.15521	1.29250	.22963
	6	1.53062	1.32084	1.34285	.20906		6	1.37943	1.14807	1.35916	.26964
	7	1.56467	1.32016	1.41075	.23968		7	1.41067	1.14184	1.42906	.30801
	8	1.60075	1.32034	1.48134	.27003		8	1.44280	1.13650	1.50253	.34487
	9	1.63785	1.32151	1.56185	.29919		9	1.47583	1.13188	1.57987	.38033
	10	1.67656	1.32364	1.64444	.32752		10	1.50992	1.12828	1.66148	.41449
	11	1.71700	1.32672	1.73283	.35511		11	1.54513	1.12540	1.74774	.44745
	12	1.75929	1.33077	1.82758	.38198		12	1.58159	1.12331	1.82915	.47924
	13	1.80370	1.33585	1.92951	.40816		13	1.61925	1.12200	1.92582	.50988
	14	1.85044	1.34190	2.02959	.43727		14	1.65874	1.12114	2.03961	.52978
	15	1.89980	1.34908	2.15885	.45968		15	1.69971	1.12167	2.14992	.56862
50	0	1.30541	1.30541	1.00000	0	58	0	1.17918	1.17918	1.00000	0
	1	1.33348	1.29731	1.05072	.04075		1	1.20686	1.16522	1.05542	.05436
	2	1.36225	1.29028	1.10380	.07991		2	1.23498	1.15255	1.11302	.10586
	3	1.39174	1.28425	1.15940	.11756		3	1.26357	1.14102	1.17297	.15476
	4	1.42204	1.27920	1.21777	.15284		4	1.29271	1.13061	1.23547	.20130
	5	1.45322	1.27510	1.27916	.18884		5	1.32214	1.12122	1.30071	.24564
	6	1.48536	1.27194	1.34383	.22263		6	1.35284	1.11286	1.36892	.28796
	7	1.51656	1.26972	1.41210	.25529		7	1.38394	1.10536	1.41036	.32846
	8	1.55292	1.26837	1.48136	.28693		8	1.41582	1.09861	1.51533	.36724
	9	1.58554	1.26795	1.56095	.31756		9	1.44663	1.09309	1.59409	.40445
	10	1.62554	1.26845	1.61237	.34729		10	1.48236	1.08819	1.67705	.44017
	11	1.66408	1.27385	1.72917	.37617		11	1.51713	1.08408	1.74457	.47454
	12	1.70126	1.27204	1.82185	.40122		12	1.55305	1.08076	1.85710	.50762
	13	1.74634	1.27525	1.92125	.43154		13	1.59024	1.07621	1.95517	.53958
	14	1.79047	1.27937	2.02809	.46214		14	1.62880	1.07640	2.05932	.57042
	15	1.83687	1.27004	2.14331	.49407		15	1.66888	1.07531	2.17022	.60023

TABLE I.- VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO,
AND PRESSURE COEFFICIENT ACROSS SHOCK WAVES - Concluded

θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_{a,b}}{q_0}$	θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_{a,b}}{q_0}$
60	0	1.15470	1.15470	1.00000	0	66	0	1.09463	1.09463	1.00000	0
	1	1.16281	1.15913	1.05748	.05869		1	1.12559	1.07321	1.06691	.07545
	2	1.21128	1.12492	1.11715	.11107		2	1.15578	1.05388	1.13626	.16547
	3	1.21021	1.11200	1.17919	.16645		3	1.18829	1.03613	1.20818	.21062
	4	1.26963	1.10024	1.24379	.21606		4	1.21761	1.01850	1.27689	.26680
	5	1.29959	1.08956	1.31115	.26318		5	1.25245	1.00511	1.36067	.32847
	6	1.33016	1.07991	1.38199	.30802		6	1.28523	.99157	1.44166	.38197
	7	1.36159	1.07123	1.45505	.35075		7	1.31856	.97920	1.52616	.43233
	8	1.39336	1.06349	1.52211	.39149		8	1.35250	.96785	1.61445	.47986
	9	1.42614	1.05661	1.61296	.43053		9	1.38715	.95764	1.70686	.53374
	10	1.45981	1.05056	1.69801	.46792		10	1.42256	.94829	1.80374	.56738
	11	1.49446	1.04530	1.78756	.50775		11	1.45577	.94000	1.89687	.60453
	12	1.53015	1.04083	1.88204	.53817		12	1.49601	.93219	2.01255	.64630
	13	1.56705	1.03711	1.98204	.57130		13	1.53428	.92522	2.12537	.68296
	14	1.60524	1.03411	2.08804	.60321		14	1.57368	.92268	2.24461	.71796
	15	1.64485	1.03163	2.20066	.63397		15	1.61434	.91388	2.37080	.75142
62	0	1.13257	1.13257	1.03000	0	68	0	1.07854	1.07854	1.00000	0
	1	1.16134	1.11527	1.06001	.06356		1	1.11113	1.05481	1.07157	.08281
	2	1.19044	1.09445	1.12228	.12326		2	1.14392	1.03325	1.18574	.15911
	3	1.21994	1.08503	1.18693	.17943		3	1.17698	1.01361	1.22268	.22964
	4	1.24988	1.07187	1.25420	.23246		4	1.21035	.99570	1.30259	.29508
	5	1.28033	1.05987	1.32425	.28258		5	1.24412	.97935	1.38571	.35599
	6	1.31132	1.04897	1.39734	.33010		6	1.27834	.96440	1.47229	.41287
	7	1.34294	1.03907	1.47368	.37521		7	1.31308	.95070	1.56259	.46613
	8	1.37527	1.03015	1.55357	.41832		8	1.34843	.93821	1.65696	.51616
	9	1.40834	1.02212	1.63750	.45902		9	1.38446	.92678	1.75568	.56322
	10	1.44225	1.01497	1.72524	.49808		10	1.42122	.91635	1.85916	.60756
	11	1.48051	1.01097	1.81770	.53293		11	1.45885	.90685	1.96784	.64966
	12	1.51292	1.00303	1.91519	.57190		12	1.49741	.89825	2.08216	.68895
	13	1.54988	.99818	2.01813	.60549		13	1.53698	.89042	2.20262	.72727
	14	1.58806	.99116	2.12710	.63846		14	1.57772	.88338	2.32987	.76322
	15	1.62757	.99077	2.24268	.67016		15	1.61972	.87707	2.46455	.79749
64	0	1.11260	1.11260	1.00000	0	70	0	1.06118	1.06118	1.00000	0
	1	1.14230	1.09339	1.06311	.06909		1	1.09890	1.03765	1.07737	.09153
	2	1.17229	1.07566	1.12854	.13362		2	1.13106	1.01384	1.15827	.17580
	3	1.20263	1.05981	1.19646	.19405		3	1.16883	.99194	1.24074	.25174
	4	1.23329	1.04513	1.26705	.25082		4	1.20418	.97213	1.32717	.32233
	5	1.26456	1.03163	1.34052	.30420		5	1.23990	.95409	1.41710	.38759
	6	1.29631	1.01963	1.41710	.35459		6	1.27606	.93764	1.51080	.41814
	7	1.32862	1.00852	1.49702	.40223		7	1.31270	.92100	1.60854	.50450
	8	1.36159	.99844	1.58060	.44739		8	1.34994	.90880	1.71071	.55714
	9	1.39526	.98927	1.66809	.49026		9	1.38786	.89621	1.81765	.60643
	10	1.42974	.98100	1.75989	.53105		10	1.42754	.88510	1.93274	.65386
	11	1.46509	.97358	1.85635	.56993		11	1.46606	.87417	2.04755	.69626
	12	1.50112	.96697	1.95793	.60706		12	1.50653	.86458	2.17117	.73736
	13	1.53881	.96113	2.05507	.61255		13	1.54805	.85582	2.30216	.77624
	14	1.57739	.95602	2.17835	.67655		14	1.59076	.84788	2.44024	.81307
	15	1.61725	.95161	2.29836	.70916		15	1.63475	.84069	2.58643	.84805

NATIONAL ADVISORY
COMMITTEE FOR AERONAUTICS

TABLE II - LOCAL MACH NUMBERS BEFORE AND AFTER EXPANSION

		Local Mach number after expansion, M_a														
$\frac{c}{c_0}$	β	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°
1.0	1.0	1.0813	1.1327	1.1764	1.2185	1.2577	1.2938	1.3298	1.3648	1.4000	1.4350	1.4690	1.5032	1.5368	1.5706	
1.1	1.1	1.1476	1.1908	1.2313	1.2694	1.3056	1.3413	1.3772	1.4124	1.4467	1.4806	1.5142	1.5480	1.5822	1.6160	
1.2	1.2	1.2403	1.2780	1.3111	1.3497	1.3850	1.4200	1.4544	1.4882	1.5228	1.5566	1.5896	1.6231	1.6572	1.6912	
1.3	1.3	1.3365	1.3714	1.4061	1.4406	1.4747	1.5090	1.5433	1.5768	1.6107	1.6444	1.6782	1.7126	1.7467	1.7808	
1.4	1.4	1.4545	1.4886	1.5026	1.5368	1.5708	1.6044	1.6388	1.6727	1.7062	1.7408	1.7747	1.8092	1.8442	1.8788	
1.5	1.5	1.5338	1.5675	1.6016	1.6361	1.6698	1.7036	1.7388	1.7725	1.8066	1.8420	1.8762	1.9113	1.9420	1.9827	
1.6	1.6	1.6355	1.6675	1.7020	1.7359	1.7705	1.8045	1.8386	1.8739	1.9096	1.9453	1.9808	2.0175	2.0540	2.0912	
1.7	1.7	1.7359	1.7684	1.8026	1.8371	1.8727	1.9082	1.9425	1.9790	2.0156	2.0507	2.0893	2.1272	2.1650	2.2030	
1.8	1.8	1.8329	1.8688	1.9018	1.9398	1.9765	2.0125	2.0487	2.0858	2.1236	2.1613	2.1998	2.2368	2.2780	2.3179	
1.9	1.9	1.9361	1.9720	2.0077	2.0449	2.0819	2.1185	2.1568	2.1944	2.2324	2.2713	2.3122	2.3522	2.3933	2.4348	
2.0	2.0	2.0363	2.0732	2.1105	2.1493	2.1869	2.2256	2.2644	2.3038	2.3426	2.3815	2.4260	2.4680	2.5107	2.5562	
2.1	2.1	2.1372	2.1753	2.2112	2.2525	2.2924	2.3324	2.3731	2.4116	2.4561	2.4980	2.5420	2.5858	2.6308	2.6761	
2.2	2.2	2.2381	2.2748	2.3181	2.3583	2.3997	2.4410	2.4829	2.5258	2.5698	2.6136	2.6587	2.7053	2.7521	2.7996	
2.3	2.3	2.3302	2.3805	2.4218	2.4640	2.5061	2.5486	2.5937	2.6385	2.6810	2.7308	2.7783	2.8235	2.8748	2.9250	
2.4	2.4	2.4415	2.4832	2.5264	2.5702	2.6141	2.6599	2.7059	2.7526	2.8004	2.8477	2.8980	2.9482	2.9970	3.0520	
2.5	2.5	2.5129	2.5868	2.6319	2.6775	2.7235	2.7702	2.8190	2.8677	2.9167	2.9665	3.0193	3.0724	3.1263	3.1812	
2.6	2.6	2.6047	2.6902	2.7372	2.7842	2.8324	2.8812	2.9319	2.9828	3.0358	3.0887	3.1415	3.1968	3.2530	3.3112	
2.7	2.7	2.7170	2.7942	2.8412	2.8915	2.9412	2.9929	3.0450	3.0955	3.1513	3.2092	3.2663	3.3232	3.3823	3.4432	
2.8	2.8	2.8484	2.8976	2.9480	2.9998	3.0510	3.1055	3.1602	3.2118	3.2710	3.3316	3.3905	3.4507	3.5137	3.5783	
2.9	2.9	2.9500	3.0020	3.0532	3.1078	3.1625	3.2175	3.2744	3.3337	3.3930	3.4527	3.5163	3.5804	3.6460	3.7130	
3.0	3.0	3.0527	3.1060	3.1593	3.2163	3.2728	3.3305	3.3907	3.4527	3.5142	3.5778	3.6440	3.7107	3.7792	3.8510	
3.1	3.1	3.1516	3.2098	3.2660	3.3218	3.3844	3.4474	3.5074	3.5711	3.6365	3.7050	3.7725	3.8422	3.9157	3.9897	
3.2	3.2	3.2568	3.3143	3.3720	3.4311	3.4965	3.5602	3.6241	3.6920	3.7597	3.8302	3.9021	3.9762	4.0552	4.1305	
3.3	3.3	3.3588	3.4188	3.4749	3.5411	3.6081	3.6756	3.7421	3.8121	3.8810	3.9518	4.0326	4.1108	4.1910	4.2720	
3.4	3.4	3.4634	3.5236	3.5876	3.6557	3.7208	3.7901	3.8602	3.9316	4.0089	4.0858	4.1662	4.2468	4.3316	4.4175	
3.5	3.5	3.5612	3.6380	3.6957	3.7645	3.8335	3.9067	3.9814	4.0564	4.1348	4.2164	4.2992	4.3847	4.4730	4.5635	
3.6	3.6	3.6666	3.7332	3.8055	3.8750	3.9474	4.0240	4.1008	4.1804	4.2624	4.3483	4.4334	4.5240	4.6165	4.7118	
3.7	3.7	3.7693	3.8385	3.9116	3.9859	4.0611	4.1407	4.2213	4.3014	4.3901	4.4786	4.5698	4.6612	4.7609	4.8617	
3.8	3.8	3.8757	3.9437	4.0200	4.0975	4.1762	4.2594	4.3318	4.4300	4.5193	4.6111	4.7070	4.8063	4.9080	5.0132	
3.9	3.9	3.9747	4.0491	4.1293	4.2046	4.3766	4.4404	4.5155	4.6184	4.7148	4.8152	4.9193	5.0557	5.1672		
4.0	4.0	4.0768	4.1517	4.2372	4.3202	4.4072	4.4960	4.5874	4.6820	4.7808	4.8803	4.9860	5.0945	5.2064	5.3219	
4.1	4.1	4.1800	4.2670	4.3462	4.4328	4.5228	4.6152	4.7112	4.8100	4.9120	5.0179	5.1264	5.2408	5.3575	5.4797	
4.2	4.2	4.2823	4.3668	4.4562	4.5460	4.6361	4.7300	4.8221	4.9278	5.0241	5.1262	5.2269	5.3278	5.4311	5.5395	
4.3	4.3	4.3860	4.4739	4.5768	4.6852	4.7879	4.8856	4.9808	5.0864	5.1879	5.2925	5.4126	5.5274	5.6304		
4.4	4.4	4.4896	4.5800	4.6756	4.7720	4.8733	4.9771	5.0855	5.1971	5.3133	5.4353	5.5588	5.6886	5.8216	5.9637	
4.5	4.5	4.5924	4.6861	4.7851	4.8857	4.9900	5.0939	5.2038	5.3278	5.4490	5.5705	5.7048	5.8398	5.9828	6.1300	
4.6	4.6	4.6951	4.7927	4.8951	5.0003	5.1085	5.2220	5.3376	5.4601	5.5858	5.7164	5.8530	5.9943	6.1427	6.2986	
4.7	4.7	4.7989	4.9005	5.0050	5.1116	5.2275	5.3400	5.4569	5.5822	5.7160	5.8594	6.0022	6.1524	6.3053	6.4670	
4.8	4.8	4.9001	5.0072	5.1161	5.2296	5.3406	5.4683	5.5940	5.7250	5.8624	6.0017	6.1526	6.3080	6.4698	6.6382	
4.9	4.9	5.0054	5.1147	5.2264	5.3424	5.4650	5.5921	5.7234	5.8592	6.0010	6.1500	6.3052	6.4665	6.6362	6.8133	
5.0	5.0	5.1081	5.2220	5.3382	5.4600	5.5899	5.7168	5.8522	5.9951	6.1140	6.2979	6.4586	6.6275	6.8086	6.9902	
5.1	5.1	5.2121	5.3293	5.4490	5.5763	5.7062	5.8410	5.9823	6.1211	6.2940	6.4458	6.6136	6.7900	6.9750	7.1686	
5.2	5.2	5.3150	5.4370	5.5621	5.6813	5.8262	5.9677	6.1157	6.2677	6.3280	6.5054	6.7070	6.9542	7.1470	7.3188	
5.3	5.3	5.4196	5.5443	5.6731	5.8083	5.9189	5.9696	6.2180	6.4058	6.5720	6.7462	6.9290	7.1244	7.3213	7.5235	
5.4	5.4	5.5238	5.6522	5.7853	5.9218	6.0702	6.2220	6.3792	6.5457	6.7178	6.8893	7.0885	7.3084	7.5000	7.7194	
5.5	5.5	5.6271	5.7610	5.8982	6.0418	6.1920	6.3489	6.5127	6.6844	6.8632	7.0513	7.2563	7.4576	7.6772	7.9086	
5.6	5.6	5.7315	5.8688	6.0111	6.1597	6.3114	6.4774	6.6172	6.8213	7.0117	7.2072	7.4125	7.6296	7.8581	8.1000	
5.7	5.7	5.8356	5.9772	6.1248	6.2780	6.4382	6.6058	6.7616	6.9658	7.1600	7.3634	7.5774	7.8026	8.0420	8.2937	
5.8	5.8	5.9391	6.0858	6.2382	6.3960	6.5512	6.7355	6.9170	7.1088	7.3093	7.5218	7.7443	7.9780	8.2262	8.5110	
5.9	5.9	6.0434	6.1942	6.3519	6.5157	6.6864	6.8653	7.0535	7.2519	7.4600	7.6798	7.9117	8.1564	8.4156	8.6896	
6.0	6.0	6.1480	6.3030	6.4652	6.6338	6.8115	6.9970	7.1920	7.3970	7.6127	7.8396	8.0815	8.3360	8.6055	8.8220	
6.1	6.1	6.2522	6.4120	6.5800	6.7552	6.9360	7.1290	7.3309	7.5411	7.7660	8.0029	8.2515	8.5173	8.7968	9.0967	
6.2	6.2	6.3561	6.5216	6.6932	6.8752	7.0520	7.2593	7.4682	7.6889	7.8200	8.1618	8.4250	8.6998	8.9924	9.3044	
6.3	6.3	6.4608	6.6300	6.8070	6.9593	7.1880	7.3920	7.6081	7.8350	8.0760	8.3323	8.6012	8.8867	9.1934	9.5166	
6.4	6.4	6.5657	6.7400	6.9229	7.1145	7.3147	7.5260	7.7500	7.9842	8.2326	8.4968	8.7780	9.0725	9.3910	9.7287	
6.5	6.5	6.6710	6.8500	7.0381	7.2318	7.4421	7.6600	7.8314	8.1334	8.3913	8.6634	8.9547	9.2630	9.5932	9.9443	
6.6	6.6	6.7755	6.9500	7.1522	7.3565	7.5598	7.7952	8.0241	8.2916	8.5520	8.8293	9.1550	9.4551	9.7933	10.1650	
6.7	6.7	6.8817	7.0680	7.2622	7.4761	7.6920	7.9308	8.2261	8.5116	8.7210	9.0052	9.3166	9.6500	10.0052	10.3888	
6.8	6.8	6.9861	7.1789	7.3858	7.296	7.8262	8.0650	8.3181	8.5887	8.7471	9.0171	9.2570	9.5200	9.8163	10.2177	
6.9	6.9	7.0898	7.2898	7.5009	7.7221	7.9561	8.2030	8.4638	8.7430	9.0360	9.3528	9.6877	10.0468	10.4313	10.8452	
7.0	7.0	7.1949	7.4000	7.6158	7.8431	8.0840	8.3405	8.6092	8.8968	9.2030	9.5286	9.8747	10.2482	10.6167	11.0778	
7.1	7.1	7.3006	7.5109	7.7336	7.9690	8.2146	8.4778	8.7565	9.0528	9.3679	9.7041	10.0653	10.4492	10.8658	11.3155	
7.2	7.2	7.4052	7.6210	7.8507	8.0909</td											

TABLE II.- LOCAL MACH NUMBERS BEFORE AND AFTER EXPANSIONS - Concluded

$x_b^{-\beta}$	Local Mach number after expansion, M_a															
	15°	16°	17°	18°	19°	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	30°
1.0	1.6016	1.6382	1.6721	1.7061	1.7408	1.7752	1.8098	1.8446	1.8796	1.9148	1.9503	1.9860	2.0235	2.0600	2.0968	2.1320
1.1	1.6198	1.6537	1.7179	1.7522	1.7867	1.8208	1.8550	1.8905	1.9258	1.9621	1.9978	2.0340	2.0712	2.1092	2.1465	2.1852
1.2	1.7256	1.7526	1.7941	1.8292	1.8641	1.8990	1.9352	1.9705	2.0065	2.0431	2.0800	2.1179	2.1560	2.1938	2.2322	2.2709
1.3	1.8158	1.8509	1.8861	1.9213	1.9579	1.9928	2.0288	2.0655	2.1025	2.1302	2.1781	2.2164	2.2557	2.2950	2.3361	2.3769
1.4	1.9140	1.9458	1.9859	2.0223	2.0590	2.0958	2.1338	2.1715	2.2100	2.2491	2.2886	2.3287	2.3689	2.4100	2.4506	2.4910
1.5	2.0192	2.0558	2.0927	2.1308	2.1686	2.2064	2.2455	2.2855	2.3250	2.3647	2.4065	2.4481	2.4900	2.5325	2.5765	2.6278
1.6	2.1286	2.1650	2.2047	2.2438	2.2820	2.3212	2.3600	2.4001	2.4400	2.4804	2.5220	2.5759	2.6200	2.6708	2.7157	2.7610
1.7	2.2118	2.2812	2.3213	2.3628	2.4027	2.4433	2.4850	2.5299	2.5755	2.6182	2.6655	2.7092	2.7561	2.8072	2.8510	2.9015
1.8	2.3582	2.3988	2.4408	2.4828	2.5253	2.5688	2.6110	2.6599	2.7052	2.7515	2.7989	2.8400	2.8970	2.9470	2.9985	3.0493
1.9	2.4768	2.5193	2.5627	2.6072	2.6528	2.6980	2.7460	2.7926	2.8401	2.8899	2.9401	2.9912	3.0422	3.0959	3.1497	3.2069
2.0	2.5984	2.6436	2.6892	2.7357	2.7823	2.8305	2.8795	2.9292	2.9801	3.0320	3.0850	3.1395	3.1945	3.2512	3.3090	3.3702
2.1	2.7220	2.7690	2.8161	2.8648	2.9154	2.9659	3.0182	3.0715	3.1210	3.1788	3.2429	3.2952	3.3510	3.4118	3.4725	3.5349
2.2	2.8673	2.9097	2.9474	2.9967	3.0501	3.1050	3.1582	3.2150	3.2720	3.3296	3.3892	3.4506	3.5128	3.5762	3.6424	3.7085
2.3	2.9752	3.0281	3.0804	3.1355	3.1890	3.2460	3.3036	3.3619	3.4222	3.4812	3.5470	3.6130	3.6795	3.7470	3.8170	3.8875
2.4	3.1056	3.1601	3.2155	3.2720	3.3305	3.3908	3.4501	3.5133	3.5775	3.6421	3.7105	3.7795	3.8495	3.9225	3.9972	4.0730
2.5	3.2368	3.2947	3.3537	3.4110	3.4752	3.5370	3.6030	3.6692	3.7362	3.8070	3.8778	3.9518	4.0262	4.1042	4.1838	4.2652
2.6	3.3703	3.4312	3.4950	3.5611	3.6210	3.6800	3.7500	3.8260	3.8959	3.9725	4.0480	4.1260	4.2066	4.2900	4.3750	4.4650
2.7	3.5056	3.5600	3.6250	3.6918	3.7702	3.8408	3.9159	3.9878	4.0635	4.1425	4.2239	4.3075	4.3922	4.4805	4.5725	4.6650
2.8	3.6125	3.7102	3.7794	3.8492	3.9222	3.9970	4.0704	4.1518	4.2335	4.3180	4.4035	4.4921	4.5855	4.6780	4.7750	4.8768
2.9	3.7818	3.8556	3.9262	4.0070	4.0767	4.1565	4.2375	4.3200	4.4080	4.4962	4.5885	4.6804	4.7804	4.8821	4.9860	5.0995
3.0	3.9235	3.9977	4.0752	4.1534	4.2352	4.3180	4.4050	4.4940	4.5845	4.6800	4.7765	4.8785	4.9822	5.0900	5.2030	5.3179
3.1	4.0657	4.1411	4.2258	4.3092	4.3948	4.4832	4.5780	4.6760	4.7752	4.8752	4.9710	5.0792	5.1900	5.3052	5.4252	5.5520
3.2	4.2118	4.2942	4.3792	4.4681	4.5578	4.6515	4.7485	4.8485	4.9520	5.0590	5.1700	5.2810	5.4280	5.6280	5.8290	7.0290
3.3	4.3573	4.4450	4.5354	4.6288	4.7210	4.8210	4.9260	5.0320	5.1325	5.2361	5.3410	5.4470	5.5569	5.6938	5.8290	6.2293
3.4	4.5071	4.5990	4.6935	4.7920	4.8937	4.9990	5.1080	5.2196	5.3370	5.4581	5.5878	5.7150	5.8902	5.9931	6.1100	6.2293
3.5	4.6975	4.7516	4.8557	4.9588	5.0662	5.1768	5.2918	5.4115	5.5352	5.6645	5.7995	5.9385	6.0810	6.2265	6.3600	6.5600
3.6	4.8105	4.9129	5.0183	5.1279	5.2110	5.3250	5.4380	5.5685	5.7080	5.8460	5.9870	6.1260	6.2645	6.4265	6.5772	6.8350
3.7	4.9649	5.0733	5.1803	5.3000	5.4200	5.5455	5.6730	5.8080	5.9468	6.0945	6.2460	6.4059	6.5720	6.7460	6.9285	7.1220
3.8	5.1223	5.2355	5.3528	5.4750	5.6015	5.7336	5.8700	6.0130	6.1619	6.3175	6.4780	6.6465	6.8275	7.1029	7.2100	7.4160
3.9	5.2810	5.4007	5.5218	5.6521	5.7870	5.9255	6.0710	6.2220	6.3800	6.5455	6.7190	6.8855	7.0900	7.2893	7.5000	7.7200
4.0	5.4432	5.5682	5.6985	5.8319	5.9747	6.1225	6.2753	6.4260	6.6010	6.7800	6.9650	7.1575	7.3600	7.5755	7.8000	8.0400
4.1	5.6066	5.7280	5.8750	6.0180	6.1623	6.3230	6.4863	6.6500	6.8245	7.0200	7.2185	7.4245	7.6412	7.8700	8.1120	8.3695
4.2	5.7718	5.9105	6.0560	6.2058	6.3526	6.5270	6.6960	6.8800	7.0700	7.2680	7.4775	7.6985	7.9300	8.1760	8.4350	8.7120
4.3	5.9407	6.0852	6.2273	6.3924	6.5622	6.7375	6.9100	7.1100	7.3095	7.5210	7.7439	7.9795	8.2265	8.4900	8.7718	9.0695
4.4	6.1106	6.2658	6.4215	6.5913	6.7657	6.9490	7.1410	7.3400	7.5575	7.7850	8.0210	8.2710	8.5360	8.8195	9.1218	9.4385
4.5	6.2830	6.4440	6.6125	6.7680	6.9725	7.1667	7.3700	7.5850	7.8120	8.0500	8.3025	8.5705	8.8545	9.1580	9.4820	9.8260
4.6	6.4580	6.6282	6.8044	6.9815	7.1845	7.3887	7.6043	7.8300	8.0730	8.3225	8.6055	8.8800	9.1865	9.5045	9.8550	10.2373
4.7	6.6352	6.8134	6.9955	7.1950	7.3998	7.6161	7.8168	8.0820	8.3100	8.6085	8.8955	9.2020	9.5270	9.8700	10.2650	10.6490
4.8	6.8158	7.0026	7.1972	7.1028	7.3189	7.8471	8.0875	8.3120	8.6135	8.9020	9.2035	9.5298	9.8805	10.2500	10.6536	11.0850
4.9	6.9997	7.1940	7.3998	7.6170	7.8445	8.0815	8.3060	8.6950	9.0245	10.2465	10.7465	11.0770	11.5400			
5.0	7.1850	7.3895	7.6037	7.8313	8.0722	8.3257	8.5960	8.8800	9.1810	9.5100	9.8542	10.2270	10.6265	11.0560	11.5160	12.0220
5.1	7.3751	7.5876	7.8150	8.0618	8.3053	8.5700	8.8560	9.1600	9.4820	9.8260	10.1641	10.5610	11.0180	11.4760	11.978	
5.2	7.5440	7.7886	8.0250	8.2767	8.5128	8.8250	9.1270	9.4470	9.7690	10.1580	10.5172	10.9580	11.4280	11.9220		
5.3	7.7576	7.9330	8.2109	8.5668	8.7668	9.0850	9.4010	9.7385	10.1040	10.4820	10.8208	11.2108	11.6320	11.9515		
5.4	7.9545	8.2006	8.4620	8.7395	9.0345	9.3490	9.6820	10.0425	10.4200	11.2895	11.7680					
5.5	8.1532	8.4115	8.6887	8.9772	9.2883	9.6190	9.9760	10.3530	10.7600	11.2040	11.6763					
5.6	8.3550	8.6270	8.9150	9.2207	9.5180	9.8950	10.2207	10.6000	11.1040	11.5780	12.0950					
5.7	8.5520	8.8117	9.1168	9.4582	9.8123	10.1800	10.5200	10.9980	11.4570	11.9550						
5.8	8.7695	9.0561	9.3287	9.7215	10.0821	10.4687	10.8890	11.2140	11.6820	12.1060						
5.9	8.9793	9.2930	9.6235	9.9781	10.3580	10.7670	11.2060	11.6820								
6.0	9.1966	9.5212	9.8690	10.2140	10.6110	11.0710	11.540									
6.1	9.4154	9.7552	10.1188	10.5085	10.9297	11.3820	11.8714									
6.2	9.6258	9.9920	10.3732	10.7820	11.2232	11.7025										
6.3	9.8626	10.2340	10.6314	11.0643	11.5272	12.0292										
6.4	10.0890	10.4790	10.8950	11.3162	11.8354											
6.5	10.3226	10.7288	11.1668	11.6397												
6.6	10.5590	10.9825	11.4413	11.9380												
6.7	10.7995	11.2110	11.7214	12.0092												
6.8	11.0450	11.5067														
6.9	11.2938	11.7748														
7.0	11.5424	12.0465														
7.1	11.8010															
7.2	12.0600															

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TABLE III.- STATIC PRESSURE RATIO ACROSS EXPANSION WAVES

		Ratio of static pressure after to static pressure before expansion, p_a/p_b														
M_b	β	0°	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°	11°	12°	13°	14°
1.0	1	0.90721	0.85100	0.80486	0.76192	0.72329	0.68896	0.65588	0.62488	0.59181	0.56608	0.53921	0.51325	0.48875	0.46512	
1.1	1	0.91222	0.89109	0.84150	0.80215	0.76171	0.72819	0.69275	0.65930	0.62795	0.59815	0.56975	0.54234	0.51571	0.49054	
1.2	1	0.91939	0.90167	0.85511	0.81749	0.78377	0.74080	0.70538	0.67156	0.63907	0.60835	0.57938	0.55105	0.52394	0.49781	
1.3	1	0.91151	0.90820	0.86267	0.82202	0.78281	0.74496	0.70823	0.67462	0.64159	0.61039	0.58005	0.55075	0.52301	0.49558	
1.4	1	0.91232	0.90701	0.86361	0.82167	0.78169	0.74595	0.70871	0.67176	0.63872	0.60632	0.57570	0.54610	0.51755	0.49071	
1.5	1	0.95205	0.90615	0.86205	0.81855	0.77852	0.73967	0.70155	0.66630	0.63249	0.59908	0.56706	0.53827	0.50922	0.48197	
1.6	1	0.95115	0.90124	0.85851	0.81561	0.77405	0.73469	0.69726	0.66011	0.62498	0.59129	0.55966	0.52663	0.49939	0.47122	
1.7	1	0.95003	0.90151	0.85563	0.81159	0.76835	0.72739	0.68869	0.65180	0.61572	0.58111	0.54886	0.51751	0.48762	0.45947	
1.8	1	0.95081	0.89979	0.85116	0.80630	0.76189	0.72019	0.68688	0.64211	0.60556	0.57090	0.53752	0.50971	0.47560	0.44681	
1.9	1	0.94568	0.89444	0.84615	0.79856	0.75373	0.71173	0.67047	0.63216	0.59566	0.56048	0.52575	0.49987	0.46341	0.43408	
2.0	1	0.94504	0.89218	0.84172	0.79217	0.74692	0.70301	0.66159	0.62203	0.58952	0.54851	0.51391	0.48134	0.44600	0.40998	
2.1	1	0.94353	0.88893	0.83644	0.78776	0.74007	0.69517	0.65234	0.61110	0.57882	0.53622	0.50110	0.46807	0.43698	0.40746	
2.2	1	0.94169	0.88573	0.83121	0.78061	0.73172	0.68601	0.64269	0.60121	0.56152	0.52171	0.48940	0.45553	0.42376	0.39425	
2.3	1	0.94051	0.88374	0.82658	0.77103	0.72160	0.67861	0.63279	0.59015	0.55043	0.51233	0.47630	0.44265	0.41117	0.38111	
2.4	1	0.93750	0.87832	0.82126	0.76729	0.71632	0.66824	0.62225	0.57905	0.53839	0.50097	0.46415	0.43026	0.39824	0.36823	
2.5	1	0.92552	0.87336	0.81507	0.75270	0.70761	0.65891	0.61160	0.56795	0.52732	0.48915	0.45188	0.41714	0.38531	0.35551	
2.6	1	0.92228	0.87009	0.80942	0.74228	0.69981	0.64981	0.60185	0.55152	0.51441	0.47721	0.43999	0.40553	0.37217	0.34111	
2.7	1	0.92040	0.86426	0.76489	0.69429	0.60631	0.52677	0.47424	0.40601	0.36165	0.32750	0.29752	0.26123	0.23099	0.20100	
2.8	1	0.92882	0.86210	0.79888	0.73947	0.68452	0.51118	0.48029	0.42716	0.39776	0.35296	0.32160	0.28170	0.24897	0.21853	
2.9	1	0.92725	0.85754	0.79430	0.72320	0.67558	0.62285	0.57313	0.52582	0.48269	0.44310	0.40476	0.36972	0.33728	0.30728	
3.0	1	0.92117	0.85269	0.78891	0.72544	0.66790	0.61419	0.56305	0.51517	0.47200	0.43145	0.39323	0.35841	0.32612	0.29566	
3.1	1	0.92232	0.85032	0.78316	0.72897	0.65961	0.60524	0.55229	0.50513	0.46154	0.42198	0.38213	0.34740	0.31408	0.28476	
3.2	1	0.92014	0.84624	0.77756	0.71173	0.65139	0.59522	0.54590	0.49504	0.45083	0.40926	0.37115	0.33610	0.30358	0.27100	
3.3	1	0.91533	0.84237	0.77205	0.70478	0.64379	0.58631	0.54338	0.49511	0.45400	0.39926	0.36075	0.32513	0.29305	0.26357	
3.4	1	0.91582	0.83852	0.76596	0.69582	0.63618	0.57808	0.52129	0.47528	0.43011	0.38863	0.35022	0.32054	0.28542	0.25342	
3.5	1	0.91317	0.83193	0.75981	0.69097	0.62874	0.56930	0.51195	0.46607	0.42036	0.37797	0.33972	0.30465	0.27259	0.24355	
3.6	1	0.91113	0.83069	0.75133	0.68436	0.62058	0.56032	0.50620	0.45613	0.41025	0.36711	0.32991	0.29156	0.26275	0.23390	
3.7	1	0.90881	0.82874	0.74877	0.67771	0.61325	0.55228	0.49731	0.44771	0.40041	0.35934	0.31946	0.28153	0.25310	0.22161	
3.8	1	0.90695	0.82299	0.74320	0.67094	0.60509	0.54525	0.48882	0.44711	0.39891	0.35882	0.31040	0.27518	0.24402	0.21569	
3.9	1	0.90508	0.81918	0.73702	0.66478	0.59735	0.53577	0.47982	0.42622	0.38192	0.33887	0.30117	0.26828	0.23520	0.20691	
4.0	1	0.90314	0.81531	0.73244	0.65834	0.58945	0.52725	0.47074	0.41923	0.37201	0.33036	0.29171	0.25720	0.22630	0.19869	
4.1	1	0.90057	0.81090	0.72705	0.61572	0.58216	0.51952	0.46191	0.41008	0.36265	0.32086	0.28509	0.24448	0.21801	0.19049	
4.2	1	0.89917	0.80717	0.72102	0.61163	0.57525	0.51084	0.45517	0.40159	0.35666	0.31100	0.27425	0.24023	0.20982	0.18261	
4.3	1	0.89622	0.80232	0.71563	0.65879	0.56671	0.50313	0.44742	0.39324	0.34578	0.30060	0.26574	0.23192	0.20192	0.17510	
4.4	1	0.89351	0.79861	0.71027	0.63205	0.55989	0.49552	0.43644	0.38449	0.33726	0.29518	0.25736	0.22384	0.19449	0.16781	
4.5	1	0.89199	0.79181	0.70513	0.62566	0.55243	0.48754	0.42920	0.37683	0.32879	0.28733	0.24945	0.21656	0.18657	0.16062	
4.6	1	0.89018	0.79125	0.70027	0.61909	0.54603	0.47970	0.41241	0.36783	0.32078	0.28191	0.24155	0.20871	0.17950	0.15277	
4.7	1	0.88755	0.78431	0.69482	0.62375	0.58781	0.47261	0.41259	0.36000	0.31265	0.27111	0.23386	0.20098	0.17251	0.14731	
4.8	1	0.88723	0.78281	0.69211	0.60654	0.52026	0.44777	0.38583	0.35236	0.30195	0.26326	0.22659	0.19111	0.16576	0.14109	
4.9	1	0.88383	0.77828	0.68518	0.60051	0.52542	0.44755	0.39757	0.34465	0.29765	0.25590	0.21926	0.18731	0.15923	0.13488	
5.0	1	0.88223	0.77476	0.67988	0.59414	0.51803	0.45026	0.39045	0.33680	0.28954	0.24859	0.21226	0.18055	0.15268	0.12895	
5.1	1	0.87901	0.77013	0.67587	0.58791	0.51132	0.44357	0.38217	0.32662	0.28274	0.24152	0.20552	0.17404	0.14681	0.12233	
5.2	1	0.87740	0.76714	0.66916	0.58242	0.50508	0.43609	0.37504	0.32235	0.27527	0.23146	0.19867	0.16774	0.14096	0.11798	
5.3	1	0.87543	0.76370	0.66480	0.57633	0.49659	0.42890	0.36649	0.31488	0.26626	0.22755	0.19216	0.16165	0.13529	0.11262	
5.4	1	0.87294	0.75993	0.65977	0.57052	0.49144	0.42487	0.36213	0.30810	0.26122	0.22099	0.18588	0.15565	0.12955	0.10758	
5.5	1	0.87136	0.75556	0.65448	0.56463	0.48519	0.41536	0.35428	0.30087	0.25470	0.21455	0.17966	0.14997	0.12441	0.10268	
5.6	1	0.86885	0.75232	0.65136	0.55816	0.47879	0.40855	0.34735	0.29429	0.24786	0.20803	0.17380	0.14335	0.11926	0.09798	
5.7	1	0.86733	0.74837	0.64397	0.55260	0.47233	0.40172	0.34107	0.28736	0.24116	0.20187	0.16794	0.13901	0.11428	0.09350	
5.8	1	0.86512	0.74459	0.63897	0.54701	0.46538	0.39518	0.33129	0.28152	0.24524	0.19573	0.16220	0.13379	0.10962	0.08913	
5.9	1	0.86292	0.74111	0.63395	0.54076	0.45961	0.39513	0.32778	0.27293	0.23910	0.19005	0.15677	0.12892	0.10488	0.08502	
6.0	1	0.86052	0.73714	0.62929	0.53445	0.45329	0.38213	0.32103	0.26819	0.22294	0.18112	0.15142	0.12272	0.10046	0.08101	
6.1	1	0.85868	0.73277	0.62410	0.52938	0.44717	0.37505	0.31150	0.26209	0.21702	0.17863	0.14639	0.12621	0.09613	0.07720	
6.2	1	0.85624	0.72976	0.61999	0.52429	0.44145	0.37057	0.30525	0.25595	0.21091	0.17810	0.14131	0.12150	0.09211	0.07353	
6.3	1	0.85460	0.72674	0.61597	0.51851	0.43559	0.36418	0.30293	0.24916	0.20563	0.16789	0.13628	0.10966	0.08791	0.06985	
6.4	1	0.85227	0.72277	0.61019	0.51297	0.42970	0.35792	0.29620	0.24430	0.20018	0.16284	0.13153	0.10589	0.08421	0.06664	
6.5	1	0.84960	0.71889	0.60548	0.50786	0.42379	0.35196	0.29053	0.23864	0.19461	0.15796	0.12709	0.10610	0.08059	0.06445	
6.6	1	0.84770	0.71516	0.60082	0.50297	0.41804	0.34591	0.28104	0.23291	0.18922	0.15305	0.12262	0.09761	0.07700	0.06051	
6.7	1	0.84603	0.71282	0.59702	0.49771	0.41270	0.36012	0.27892	0.22770	0.18119	0.14811	0.11834	0.09373	0.07341	0.05751</	

TABLE III.- STATIC PRESSURE RATIO ACROSS EXPANSION WAVES - Concluded

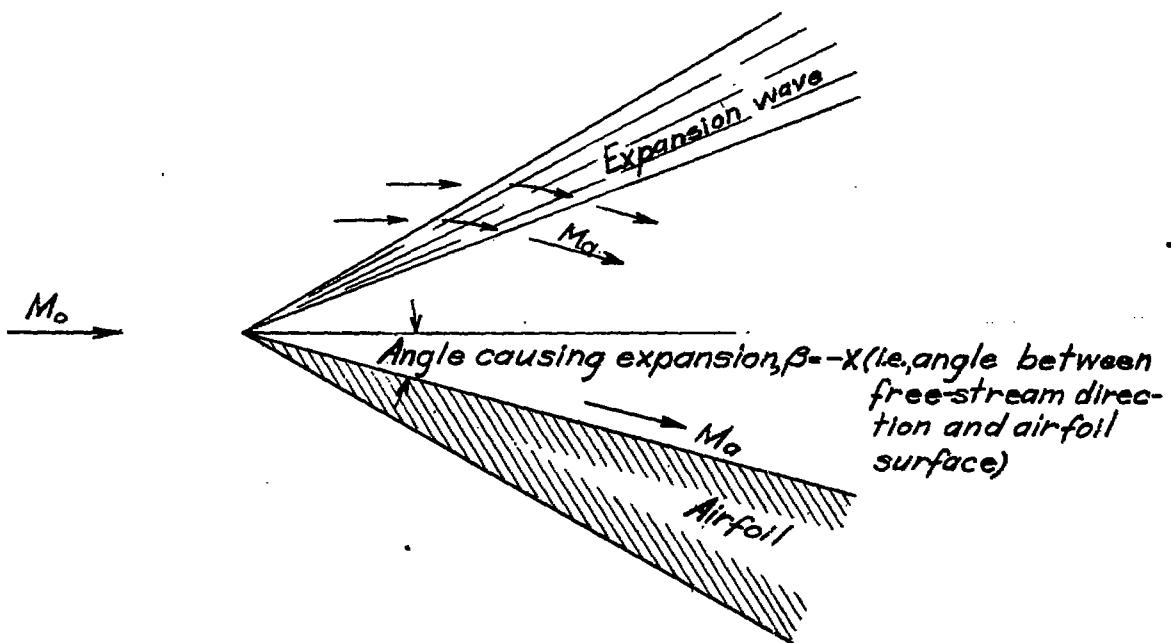
$\frac{P}{P_0}$	Ratio of static pressure after to static pressure before expansion, P_a/P_b															
K_0	15°	16°	17°	18°	19°	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	30°
1.0	0.11233	0.12075	0.13993	0.15798	0.17605	0.19410	0.21210	0.23015	0.24812	0.26610	0.28406	0.30197	0.31984	0.33771	0.35558	0.37345
1.1	0.11464	0.12322	0.14212	0.15978	0.17823	0.19668	0.21513	0.23377	0.25232	0.27177	0.29121	0.31065	0.32997	0.34921	0.36845	0.38769
1.2	0.11704	0.12652	0.14587	0.16376	0.18251	0.20138	0.22076	0.24027	0.26065	0.28098	0.30131	0.32269	0.34411	0.36542	0.38671	0.40805
1.3	0.11947	0.13063	0.15281	0.17159	0.19037	0.20914	0.22858	0.24819	0.26860	0.28878	0.30900	0.33023	0.35150	0.37373	0.39600	0.41834
1.4	0.14417	0.13970	0.15774	0.18283	0.20793	0.23027	0.25309	0.27113	0.29300	0.31559	0.33759	0.35909	0.38125	0.40390	0.42714	0.45000
1.5	0.45555	0.42862	0.40604	0.38207	0.36052	0.33989	0.31981	0.29932	0.27982	0.25932	0.23982	0.21932	0.19882	0.17832	0.15882	0.13832
1.6	0.44455	0.41877	0.39159	0.37117	0.35093	0.32776	0.30002	0.28883	0.27059	0.25338	0.23670	0.22110	0.19951	0.17451	0.15755	0.14059
1.7	0.42234	0.40652	0.38151	0.35782	0.33622	0.31561	0.29525	0.27590	0.25775	0.23090	0.21090	0.19217	0.17090	0.15152	0.13059	0.11588
1.8	0.41953	0.39375	0.36878	0.34562	0.32323	0.30233	0.28175	0.26287	0.24182	0.22801	0.21202	0.19680	0.18133	0.16959	0.15677	0.14525
1.9	0.40659	0.38058	0.35578	0.33209	0.30950	0.28859	0.26818	0.24971	0.23282	0.21535	0.19963	0.18163	0.17125	0.15808	0.14596	0.13417
2.0	0.39320	0.36657	0.34170	0.31813	0.29622	0.27521	0.25516	0.23696	0.21947	0.20305	0.18764	0.17304	0.15955	0.14675	0.13597	0.12554
2.1	0.35987	0.32551	0.32865	0.30521	0.28474	0.26224	0.24225	0.22372	0.20592	0.19082	0.17448	0.16134	0.14844	0.13598	0.12167	0.11411
2.2	0.36882	0.33959	0.31516	0.29166	0.26995	0.24858	0.22905	0.21158	0.19895	0.17902	0.16419	0.15041	0.13768	0.12558	0.11473	0.10465
2.3	0.32323	0.29628	0.29183	0.27901	0.25707	0.23673	0.21739	0.19791	0.18211	0.16767	0.15519	0.14978	0.13761	0.12584	0.11442	0.10579
2.4	0.33938	0.31363	0.28907	0.26613	0.24413	0.22107	0.20581	0.18804	0.17160	0.15491	0.13269	0.12975	0.11792	0.10682	0.09663	0.08740
2.5	0.37175	0.30091	0.27621	0.25328	0.23206	0.21256	0.19370	0.17660	0.16095	0.14604	0.13261	0.12003	0.10867	0.09802	0.08833	0.07950
2.6	0.31456	0.28858	0.26123	0.24155	0.22059	0.20062	0.18289	0.16617	0.15056	0.13623	0.12329	0.11124	0.10014	0.08973	0.08063	0.07221
2.7	0.30285	0.27657	0.25210	0.23099	0.20529	0.19003	0.17210	0.15581	0.14094	0.12705	0.11526	0.10261	0.09212	0.08243	0.07552	0.06563
2.8	0.29113	0.26198	0.21985	0.19828	0.17945	0.16202	0.15257	0.13854	0.12800	0.10581	0.09659	0.08733	0.07530	0.06696	0.05929	0.05321
2.9	0.27951	0.25111	0.23971	0.20670	0.17675	0.16255	0.15235	0.13668	0.12553	0.10969	0.09788	0.08783	0.07745	0.06859	0.06770	0.05321
3.0	0.26804	0.24267	0.21895	0.19758	0.17765	0.15972	0.14300	0.12787	0.11129	0.10167	0.09047	0.08009	0.07058	0.06255	0.05196	0.04826
3.1	0.25711	0.23171	0.20878	0.18710	0.16618	0.14616	0.13166	0.11977	0.10634	0.09415	0.08338	0.07354	0.06476	0.05688	0.04736	0.03322
3.2	0.21694	0.22161	0.19881	0.17771	0.15898	0.14167	0.12593	0.11171	0.09872	0.08725	0.07680	0.06750	0.05905	0.05194	0.04484	0.03898
3.3	0.23659	0.21180	0.18918	0.16859	0.15013	0.13795	0.12175	0.10419	0.09172	0.08062	0.07052	0.06170	0.05377	0.04667	0.04035	0.03462
3.4	0.22643	0.20208	0.18002	0.15982	0.14159	0.12511	0.11027	0.09708	0.08507	0.07410	0.06488	0.05637	0.04889	0.04217	0.03433	0.03100
3.5	0.21697	0.19886	0.17087	0.15131	0.13158	0.11751	0.10232	0.09035	0.07820	0.06865	0.05818	0.05116	0.04325	0.03805	0.03251	0.02776
3.6	0.20768	0.18528	0.16253	0.14253	0.12589	0.11254	0.09413	0.07525	0.07509	0.06327	0.05418	0.04647	0.04034	0.03412	0.02912	0.02458
3.7	0.19855	0.17628	0.15158	0.13582	0.11650	0.10251	0.09004	0.07526	0.06809	0.06290	0.05633	0.05279	0.04768	0.04263	0.03603	0.03195
3.8	0.19012	0.16693	0.14551	0.12902	0.11157	0.09539	0.07213	0.06289	0.05336	0.04563	0.03777	0.03279	0.02768	0.02219	0.01936	0.01576
3.9	0.18189	0.15916	0.13859	0.12106	0.10490	0.09079	0.07821	0.06719	0.05750	0.04829	0.04156	0.03518	0.02937	0.02477	0.02064	0.01713
4.0	0.17368	0.15153	0.13178	0.11109	0.09870	0.08791	0.07288	0.06226	0.05298	0.04190	0.03786	0.03185	0.02663	0.02213	0.01833	0.01506
4.1	0.16597	0.14121	0.12178	0.10771	0.09267	0.07936	0.06773	0.05755	0.04673	0.03673	0.03112	0.02876	0.02389	0.01975	0.01622	0.01323
4.2	0.15861	0.13721	0.11817	0.10161	0.08700	0.07675	0.06501	0.05452	0.04526	0.03576	0.03130	0.02595	0.02112	0.01756	0.01433	0.01160
4.3	0.15190	0.13017	0.10958	0.09578	0.08162	0.06915	0.05850	0.04917	0.04130	0.03411	0.02841	0.02424	0.01920	0.01562	0.01261	0.01012
4.4	0.14447	0.12393	0.10585	0.09016	0.07619	0.06459	0.05431	0.04504	0.03775	0.03125	0.02570	0.02105	0.01713	0.01382	0.01107	0.008831
4.5	0.13787	0.11776	0.10016	0.08494	0.07168	0.05932	0.04773	0.03773	0.02878	0.02228	0.01891	0.01527	0.01223	0.009717	0.007665	0.006603
4.6	0.13150	0.11172	0.09469	0.07949	0.06705	0.05612	0.04512	0.03563	0.02692	0.02100	0.01662	0.01348	0.01076	0.008566	0.006561	0.005733
4.7	0.12558	0.10612	0.08948	0.07507	0.06512	0.05416	0.04416	0.03456	0.02592	0.02026	0.01693	0.01314	0.01064	0.008142	0.006111	0.004917
4.8	0.11946	0.10262	0.08079	0.06762	0.05652	0.04616	0.03682	0.02627	0.02161	0.01517	0.01063	0.00746	0.00566	0.003416	0.002417	0.001241
4.9	0.11367	0.09762	0.06819	0.05479	0.04349	0.03474	0.02450	0.01576	0.01207	0.00919	0.00616	0.004106	0.002043	0.0009423	0.0005938	0.0002441
5.0	0.10825	0.09046	0.07522	0.06222	0.05112	0.04179	0.03391	0.02739	0.02194	0.01711	0.01373	0.01073	0.008501	0.006365	0.004837	0.003617
5.1	0.10305	0.08572	0.06749	0.05769	0.05372	0.04133	0.03248	0.02179	0.01944	0.01575	0.01230	0.009519	0.007315	0.005560	0.004164	0.002104
5.2	0.09802	0.08116	0.06686	0.05618	0.04616	0.03592	0.02878	0.02291	0.01909	0.01414	0.01039	0.008120	0.006120	0.004819	0.003617	0.00164
5.3	0.09323	0.07651	0.06297	0.05117	0.04188	0.03321	0.02619	0.01910	0.01585	0.01145	0.008712	0.006586	0.005615			
5.4	0.08860	0.07267	0.05792	0.04622	0.03625	0.02852	0.02016									
5.5	0.08124	0.06873	0.05566	0.04483	0.03577	0.02639	0.02248	0.01739	0.01413	0.01023	0.007748					
5.6	0.08003	0.06191	0.05231	0.04188	0.03324	0.02622	0.02047	0.01512	0.01212	0.00914	0.006314					
5.7	0.07592	0.06134	0.04916	0.03948	0.03086	0.02362	0.01873	0.01429	0.01092	0.008195						
5.8	0.07162	0.05792	0.04617	0.03646	0.02662	0.02228	0.01739	0.01312	0.01049	0.008195						
5.9	0.06852	0.05162	0.04152	0.03405	0.02635	0.02047	0.01649	0.01182								
6.0	0.06487	0.05156	0.04162	0.02456	0.01682	0.01128	0.00810	0.00576	0.003102							
6.1	0.06118	0.04658	0.03807	0.02657	0.01622	0.01173	0.00810	0.00576	0.003102							
6.2	0.05833	0.04179	0.03566	0.02754	0.02102	0.01586	0.01049	0.00746	0.004815	0.002417						
6.3	0.05515	0.03910	0.03310	0.02561	0.01929	0.01454	0.01070	0.00746	0.004815	0.002417						
6.4	0.05228	0.03459	0.03110	0.02379	0.01750											
6.5	0.04945	0.03819	0.02916	0.02207												
6.6	0.04677	0.03592	0.02677	0.02047			</td									

TABLE IV.- PRESSURE COEFFICIENT BASED ON FREE-STREAM DYNAMIC PRESSURE

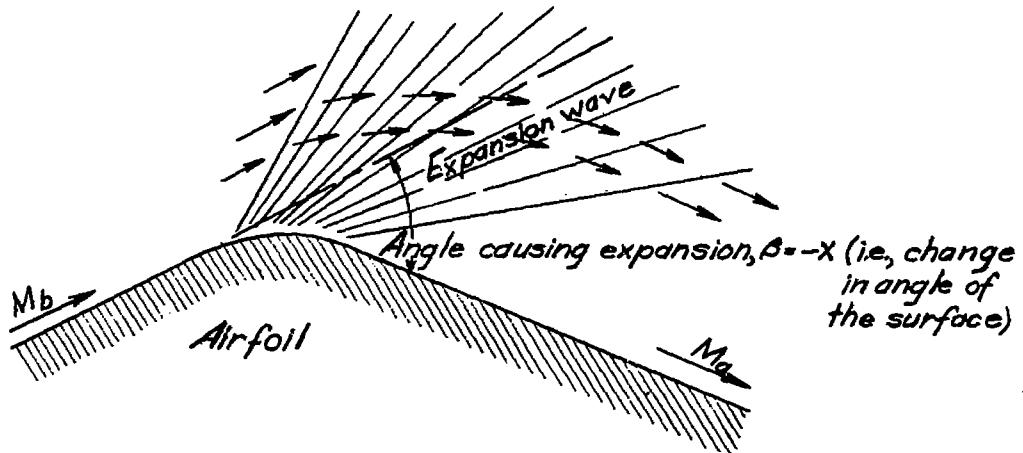
		Pressure coefficient, $\Delta p_n/q_\infty$							
M_∞	P_n/P_∞	1.0	1.25	1.5	1.75	2.0	2.5	3.0	3.5
0	-1.42857	-0.911429	-0.63492	-0.47579	-0.35714	-0.22857	-0.15873	-0.11662	
.05	-1.35714	-0.86857	-0.60317	-0.45200	-0.33929	-0.21714	-0.15079	-0.11079	
.1	-1.28571	-0.82286	-0.57143	-0.42821	-0.32143	-0.20571	-0.14286	-0.10496	
.2	-1.14286	-0.73143	-0.50794	-0.38061	-0.28571	-0.18266	-0.12698	-0.093294	
.3	-1.00000	-0.61400	-0.44444	-0.33306	-0.25000	-0.16000	-0.11111	-0.081633	
.4	-0.85714	-0.514857	-0.36094	-0.28548	-0.21429	-0.13714	-0.095238	-0.069971	
.5	-0.71429	-0.45714	-0.31746	-0.23790	-0.17857	-0.11429	-0.079365	-0.058309	
.6	-0.57143	-0.36571	-0.25397	-0.19032	-0.14286	-0.0911429	-0.063492	-0.046647	
.7	-0.42857	-0.27129	-0.19048	-0.14274	-0.10714	-0.068571	-0.047619	-0.034985	
.8	-0.28571	-0.18288	-0.12698	-0.095159	-0.0711429	-0.045714	-0.031746	-0.023224	
.9	-0.14286	0	-0.0911429	0	-0.047579	0	-0.022857	-0.015873	-0.011662
1.0	0	0	0	0	0	0	0	0	0
1.1	.11286	.0911429	.063492	.047579	.035714	.022857	.015873	.011662	
1.2	.28571	.18286	.12698	.095159	.0711429	.045714	.031746	.023324	
1.3	.42857	.27429	.19048	.14274	.10714	.068571	.047619	.034985	
1.4	.57143	.36571	.25397	.19052	.14286	.0911429	.063492	.046647	
1.5	.71429	.45714	.31746	.23790	.17857	.11429	.079365	.058309	
1.6	.85714	.54857	.38095	.28548	.21429	.13714	.095238	.069971	
1.7	1.00000	.61400	.44444	.33306	.25000	.16000	.11111	.081633	
1.8	1.14286	.73143	.20794	.38064	.28571	.18286	.12698	.093294	
1.9	1.28571	.82286	.57143	.42821	.32143	.20571	.14286	.10496	
2.0	1.42857	.91429	.63492	.47579	.35714	.22857	.15873	.11662	
2.2	1.71429	1.09714	.76190	.57095	.42857	.27429	.19048	.13994	
2.4	2.00000	1.28000	.88889	.66611	.50000	.32000	.22222	.16527	
2.6	2.28571	1.46286	1.01587	.76127	.57143	.36571	.25397	.18659	
2.8	2.57143	1.64571	1.12426	.85643	.64286	.41143	.28571	.20981	
3.0	2.85714	1.82857	1.26984	.95159	.71429	.45714	.31746	.23324	
3.2	3.11286	2.011143	1.39683	1.04675	.78571	.50286	.34921	.25656	
3.4	3.42857	2.19129	1.52381	1.11191	.85714	.54857	.38095	.27988	
3.6	3.71429	2.37714	1.65079	1.23706	.92857	.59429	.41270	.30321	
3.8	4.00000	2.56000	1.77778	1.33222	1.00000	.64000	.44444	.32652	
4.0	4.28571	2.74286	1.90476	1.42738	1.07143	.68571	.47619	.34985	
4.2	4.57143	2.92571	2.07175	1.52254	1.14286	.73143	.50794	.37318	
4.4	4.85714	3.10857	2.15873	1.61770	1.21429	.77714	.53968	.39650	
4.6	5.1286	3.29143	2.28571	1.71286	1.28571	.82286	.57143	.44983	
4.8	5.42857	3.47129	2.11270	1.80802	1.35714	.86857	.60517	.44315	
5.0	5.71429	3.65714	2.53968	1.90318	1.42657	.91429	.63492	.466147	
5.2	6.00000	3.84000	2.66667	1.99833	1.50000	.96000	.66667	.48980	
5.4	6.28511	4.02286	2.79365	2.09319	1.57143	1.00571	.69841	.51312	
5.6	6.57143	4.20571	2.92063	2.18865	1.64286	1.05143	.73016	.53644	
5.8	6.85714	4.38857	3.04762	2.28381	1.71129	1.09714	.76190	.55977	
6.0	7.14286	4.57143	3.17460	2.37897	1.78571	1.14286	.79365	.58509	
6.2	7.42857	4.75429	3.30159	2.47113	1.85714	.18857	.82540	.60641	
6.4	7.71429	4.93714	3.42857	2.56929	1.92857	1.23129	.85714	.62974	
6.6	8.00000	5.12000	3.55556	2.66145	2.00000	1.28000	.88889	.65306	
6.8	8.28571	5.30286	3.68254	2.75960	2.07143	1.32571	.92063	.67638	
7.0	8.57143	5.48571	3.80952	2.85476	2.11286	1.37143	.95238	.69971	
7.2	8.85714	5.66687	3.93651	2.94992	2.21429	1.41714	.98413	.72303	
7.4	9.14286	5.85113	4.06319	3.01508	2.28571	1.46286	1.01587	.74636	
7.6	9.42857	6.03428	4.19018	3.11024	2.35714	1.50857	1.041762	.76968	
7.8	9.71429	6.21714	4.31746	3.23540	2.42857	1.55429	1.07936	.79300	
8.0	10.00000	6.40000	4.44444	3.33056	2.50000	1.60000	1.11111	.81633	
8.2	10.28571	6.58286	4.57143	3.42572	2.57143	1.64571	1.14286	.83965	
8.4	10.57143	6.76571	4.69811	3.52087	2.61286	1.69143	1.17460	.86297	
8.6	10.85714	6.94557	4.82541	3.61603	2.71129	1.73714	1.20635	.88630	
8.8	11.14286	7.13143	4.95238	3.71119	2.78571	1.78286	1.23806	.90962	
9.0	11.42857	7.31128	5.07936	3.80635	2.85714	1.82857	1.26984	.93294	
9.2	11.71429	7.49714	5.20635	3.90151	2.92857	1.87429	1.30159	.95627	
9.4	12.00000	7.68000	5.33333	3.99667	3.00000	1.92000	1.33333	.97959	
9.6	12.28571	7.86286	5.46032	4.09183	3.07113	1.96571	1.36508	1.00292	
9.8	12.57143	8.01571	5.58730	4.18699	3.14286	2.01143	1.39682	1.02624	
10.0	12.85714	8.22857	5.71429	4.28215	3.21429	2.05714	1.42857	1.04956	

TABLE IV.- PRESSURE COEFFICIENT BASED ON FREE-STREAM DYNAMIC PRESSURE - Concluded

		Pressure coefficient, $\Delta P_{\infty}/q_0$								
M_∞	P_n/P_∞	4.0	4.5	5.0	5.5	6.0	6.5	7.0	7.5	8.0
0	-0.089286	-0.070547	-0.057143	-0.047226	-0.039683	-0.033812	-0.029155	-0.025397	-0.022321	-0.022321
.05	-0.081821	-0.067019	-0.054286	-0.044864	-0.037698	-0.032122	-0.027697	-0.024127	-0.021205	-0.021205
.1	-0.080357	-0.063492	-0.051129	-0.042503	-0.035711	-0.030431	-0.026239	-0.022857	-0.020859	-0.020859
.2	-0.071129	-0.056137	-0.045711	-0.037780	-0.031746	-0.027050	-0.023241	-0.020317	-0.017857	-0.017857
.3	-0.062500	-0.049382	-0.040000	-0.032058	-0.027778	-0.023669	-0.020108	-0.017778	-0.015625	-0.015625
.4	-0.053571	-0.042328	-0.034286	-0.028355	-0.023510	-0.020287	-0.017193	-0.015238	-0.013393	-0.013393
.5	-0.044643	-0.035273	-0.028571	-0.023613	-0.019841	-0.016906	-0.014577	-0.012698	-0.011161	-0.011161
.6	-0.035714	-0.028219	-0.022857	-0.018890	-0.015873	-0.013525	-0.011662	-0.010159	-0.0089286	-0.0089286
.7	-0.026786	-0.021164	-0.017145	-0.014168	-0.011905	-0.010144	-0.0087164	-0.0076190	-0.0066964	-0.0066964
.8	-0.017857	-0.011109	-0.011129	-0.0094451	-0.0079365	-0.0067625	-0.0058309	-0.0050794	-0.0044643	-0.0044643
.9	-0.0089286	-0.0070547	-0.0057143	-0.0047226	-0.0039683	-0.0033812	-0.0029155	-0.0025397	-0.0022321	-0.0022321
1.0	0	0	0	0	0	0	0	0	0	0
1.1	.0089286	.0070547	.0057143	.0047226	.0039683	.0033812	.0029155	.0025397	.0022321	.0022321
1.2	.017857	.011109	.011129	.0094451	.0079365	.0067625	.0058309	.0050794	.0044643	.0044643
1.3	.026786	.021164	.017145	.014168	.011905	.010144	.0087164	.0076190	.0066964	.0066964
1.4	.035714	.028219	.022857	.018890	.015873	.013525	.011662	.010159	.0089286	.0089286
1.5	.044643	.035273	.028571	.023613	.019841	.016906	.014577	.012698	.011161	.011161
1.6	.053571	.042328	.034286	.028355	.023810	.020287	.017493	.015238	.013393	.013393
1.7	.062500	.049382	.040000	.033058	.027778	.023669	.020408	.017778	.015625	.015625
1.8	.071129	.056137	.045711	.037780	.031746	.027050	.023324	.020517	.017857	.017857
1.9	.080357	.063492	.051129	.042503	.035711	.030131	.026239	.022857	.020089	.020089
2.0	.089286	.070547	.057143	.047226	.039683	.033812	.029155	.025397	.022321	.022321
2.2	.10714	.084656	.068571	.056671	.047619	.040575	.034285	.030476	.026786	.026786
2.4	.12500	.098765	.080000	.066116	.055556	.047337	.040816	.035256	.031250	.031250
2.6	.141286	.11287	.091429	.075561	.063492	.054160	.046474	.040635	.035714	.035714
2.8	.16071	.12698	.10286	.085006	.071429	.060862	.052178	.045714	.040179	.040179
3.0	.17857	.14109	.11429	.094451	.079365	.067625	.058309	.050794	.044643	.044643
3.2	.19653	.15520	.12571	.10390	.087302	.074387	.061440	.055873	.049107	.049107
3.4	.21429	.16951	.13714	.11334	.098238	.081150	.069971	.060952	.053571	.053571
3.6	.23214	.18342	.11857	.12279	.10317	.087912	.075802	.066032	.058036	.058036
3.8	.25000	.19753	.16000	.13223	.11111	.094674	.081633	.071111	.062500	.062500
4.0	.26786	.21164	.17143	.14168	.11905	.10144	.087164	.076190	.066964	.066964
4.2	.28571	.22575	.18286	.15112	.12698	.10820	.093294	.081270	.071129	.071129
4.4	.30357	.23986	.19129	.16057	.13492	.11496	.099125	.086349	.075893	.075893
4.6	.32143	.25397	.20571	.17000	.14286	.12172	.10494	.091429	.080357	.080357
4.8	.33929	.26808	.21714	.17946	.15079	.12849	.11075	.096508	.084821	.084821
5.0	.35714	.28219	.22857	.18890	.15873	.13525	.11656	.10159	.089286	.089286
5.2	.37500	.29630	.24000	.19835	.16667	.14201	.12237	.10667	.093750	.093750
5.4	.39286	.31041	.25113	.20779	.17460	.15877	.12818	.11175	.098214	.098214
5.6	.41071	.32451	.26286	.21724	.18254	.15554	.13399	.11683	.10268	.10268
5.8	.42857	.33862	.27429	.22668	.19048	.16230	.13980	.12190	.10714	.10714
6.0	.44643	.35273	.28571	.23613	.19841	.16906	.14561	.12698	.11161	.11161
6.2	.46429	.36684	.29714	.21557	.20635	.17582	.15142	.13206	.11607	.11607
6.4	.48214	.38095	.30857	.25002	.21429	.18259	.15723	.13714	.12054	.12054
6.6	.50000	.39506	.32000	.26146	.22222	.18935	.16305	.14222	.12500	.12500
6.8	.51786	.40907	.33113	.27391	.23016	.19611	.16886	.14730	.12946	.12946
7.0	.53571	.42308	.34286	.28355	.23810	.20287	.17467	.15238	.13393	.13393
7.2	.55357	.43709	.35429	.29280	.24603	.20964	.18048	.15746	.13839	.13839
7.4	.57113	.45110	.36571	.30224	.25397	.21640	.18629	.16254	.14286	.14286
7.6	.58929	.46511	.37714	.31169	.26190	.22316	.19210	.16762	.14732	.14732
7.8	.60714	.47912	.38857	.32113	.26984	.22992	.19791	.17270	.15178	.15178
8.0	.62500	.49313	.40000	.33058	.27778	.23669	.20372	.17778	.15625	.15625
8.2	.64286	.50714	.41143	.34002	.28571	.24345	.20953	.180825	.16071	.16071
8.4	.66071	.52115	.42286	.34917	.29365	.25021	.23594	.18794	.16518	.16518
8.6	.67857	.53512	.43429	.35893	.30159	.25697	.22115	.19302	.16964	.16964
8.8	.69643	.54916	.44571	.36836	.30952	.26374	.22697	.19810	.17111	.17111
9.0	.71429	.56317	.45714	.37780	.31746	.27050	.23278	.20317	.17857	.17857
9.2	.73214	.57718	.46857	.38725	.32540	.27726	.23859	.20825	.18750	.18750
9.4	.75000	.59119	.48000	.39669	.33333	.28402	.21440	.21332	.18750	.18750
9.6	.76786	.60520	.49142	.40614	.34127	.29079	.25021	.21841	.19196	.19196
9.8	.78571	.61921	.50284	.41558	.34921	.29755	.25602	.22319	.19643	.19643
10.0	.80557	.63322	.51426	.42503	.35774	.30431	.26183	.22857	.20089	.20089



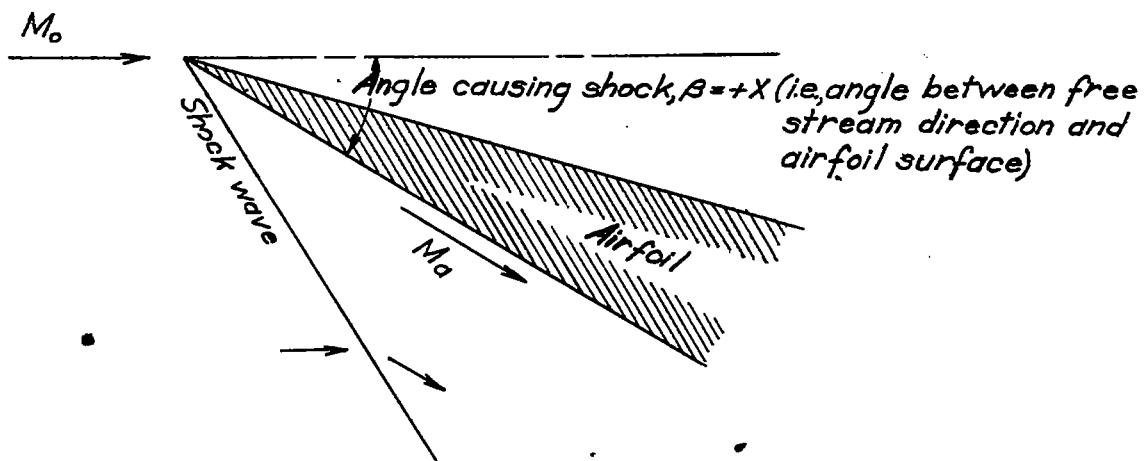
(a) Expansion at leading edge of airfoil.



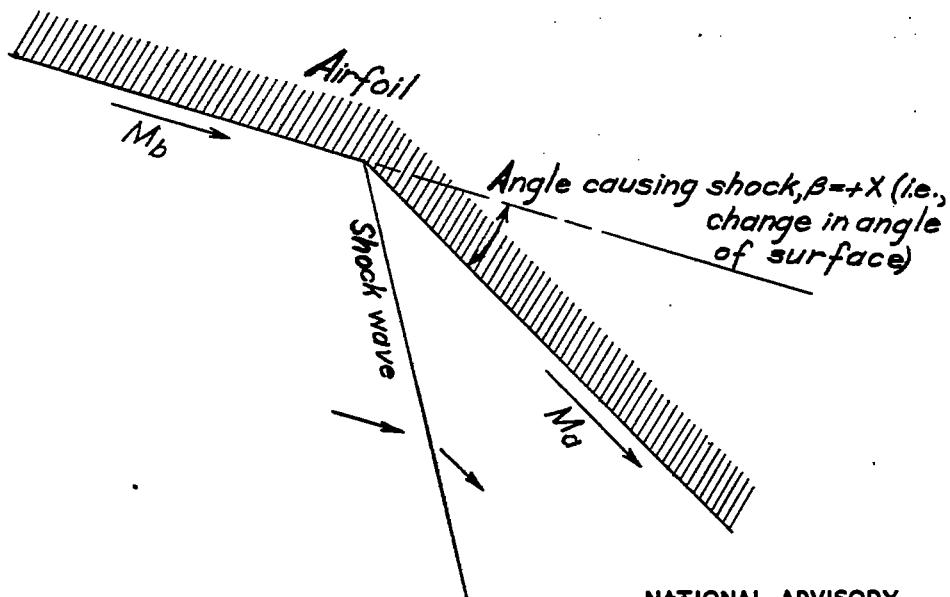
(b) Expansion along the airfoil.

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Figure 1.- Method of measuring angle causing expansion.
The angle causing expansion is always considered negative.



(a) Shock at leading edge of airfoil.

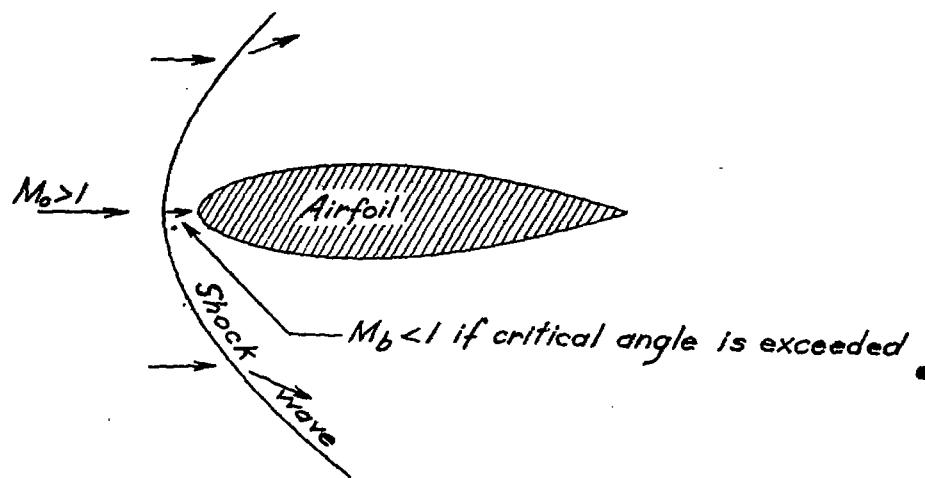
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(b) Shock at intermediate point along airfoil.

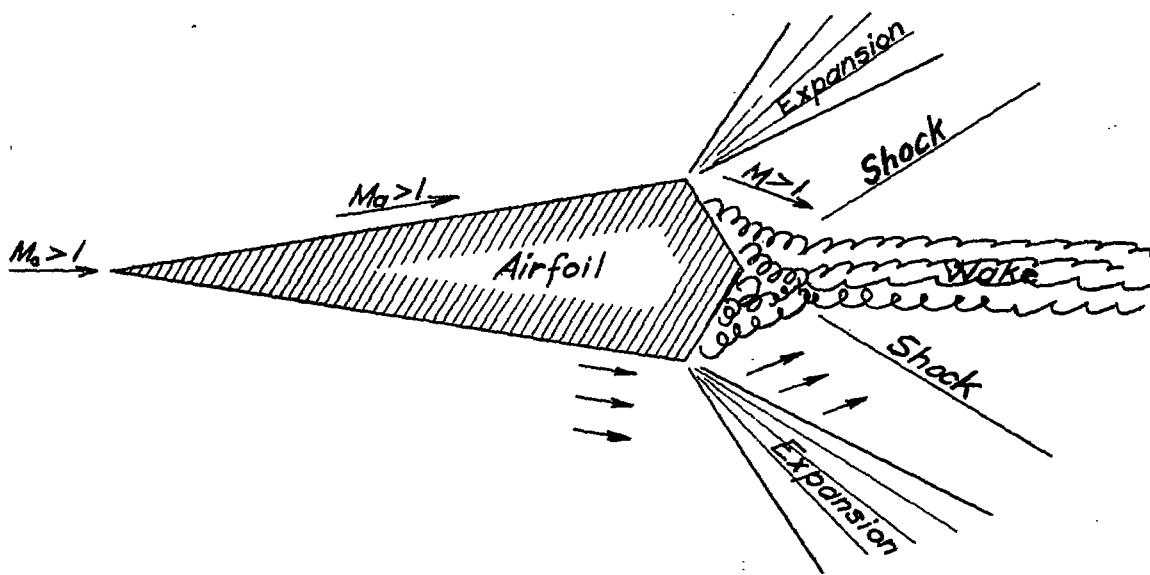
Figure 2.- Method of measuring angle causing shock. The angle causing shock is always considered positive.

Fig. 3a,b

NACA TN No. 1143



(a) Shock limitation exceeded.



(b) Expansion limitations exceeded (Turbulent wake set up.)

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Figure 3.- Effect of exceeding the limitation on angles.

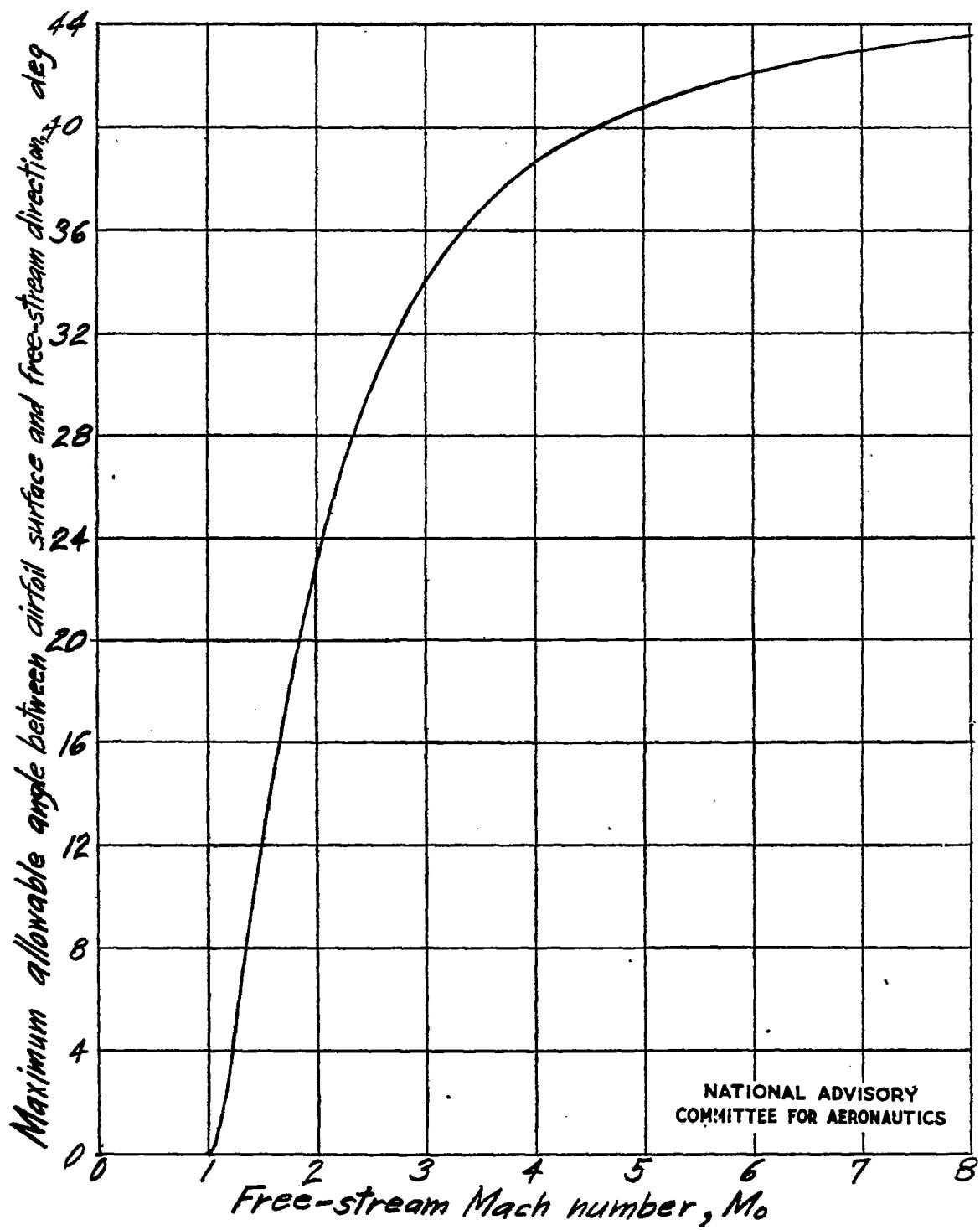


Figure 4.- Surface-angle limitation for attached shock wave.

Fig. 5

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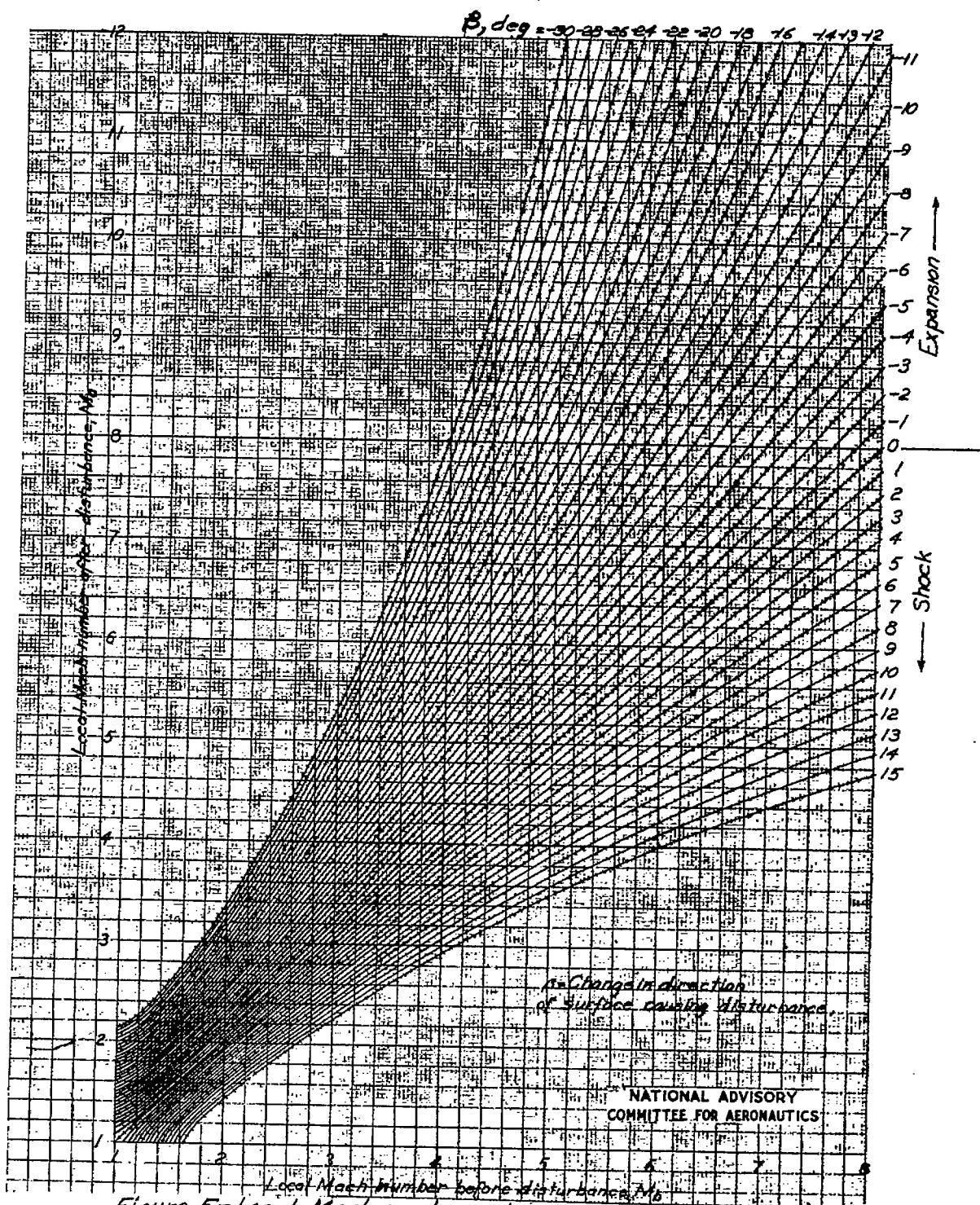


Figure 5.- Local Mach numbers before and after shocks and expansions.

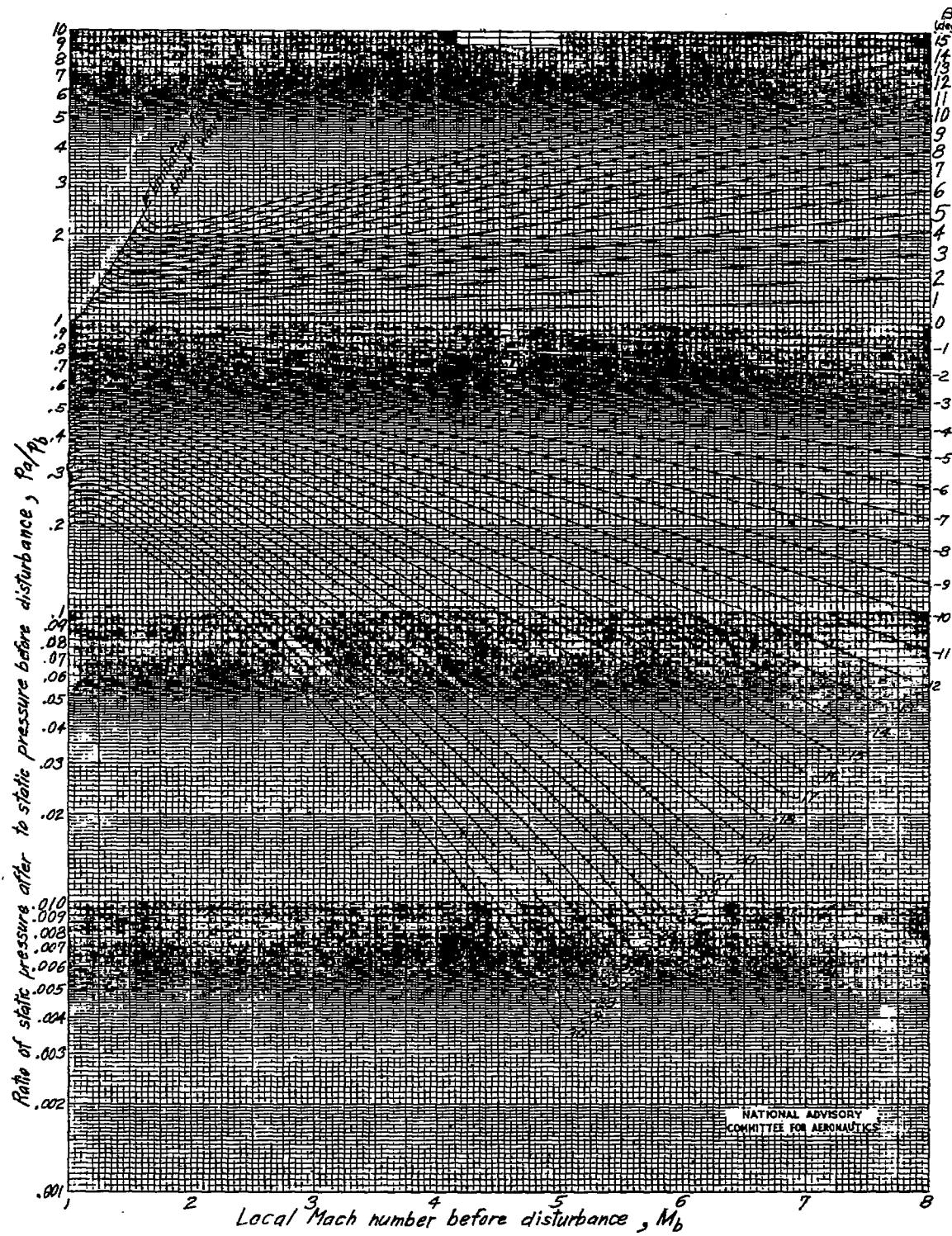
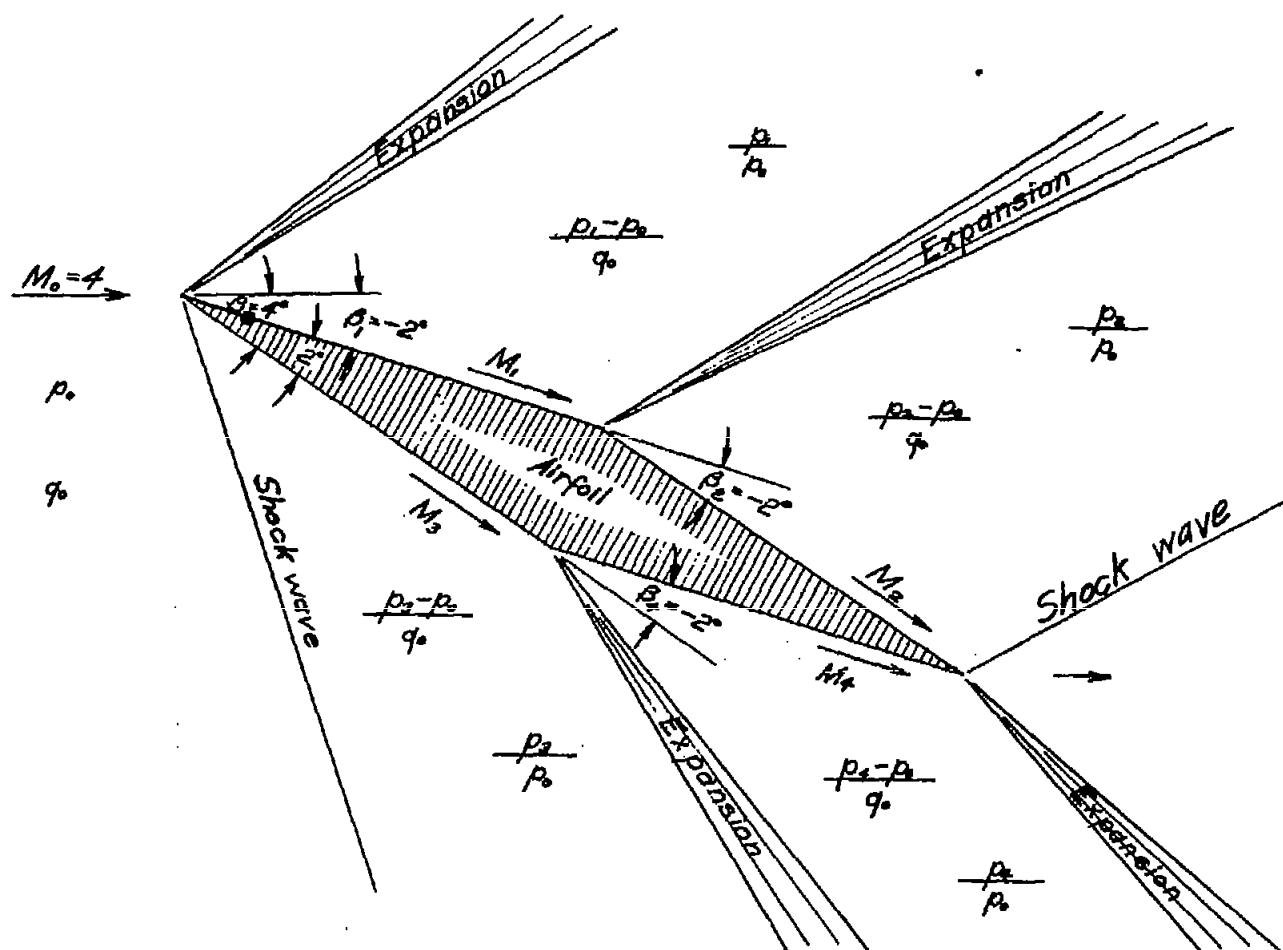


Figure 6. - Static pressure ratio across shock and expansion waves.

FIG. 7

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Figure 7.- Example airfoil (showing conditions to be determined).

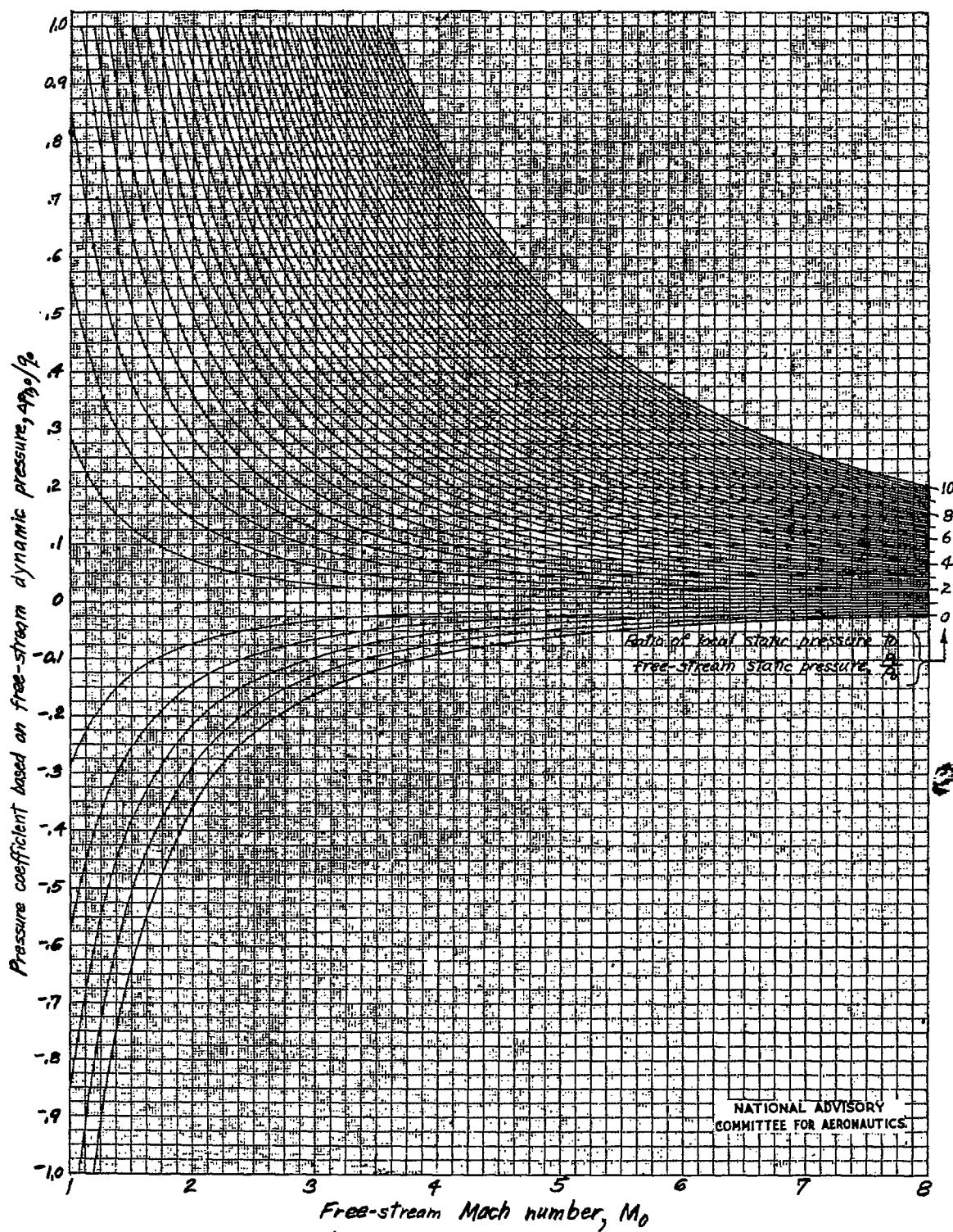


Figure 8.- Determination of pressure coefficients.

FIG. 9

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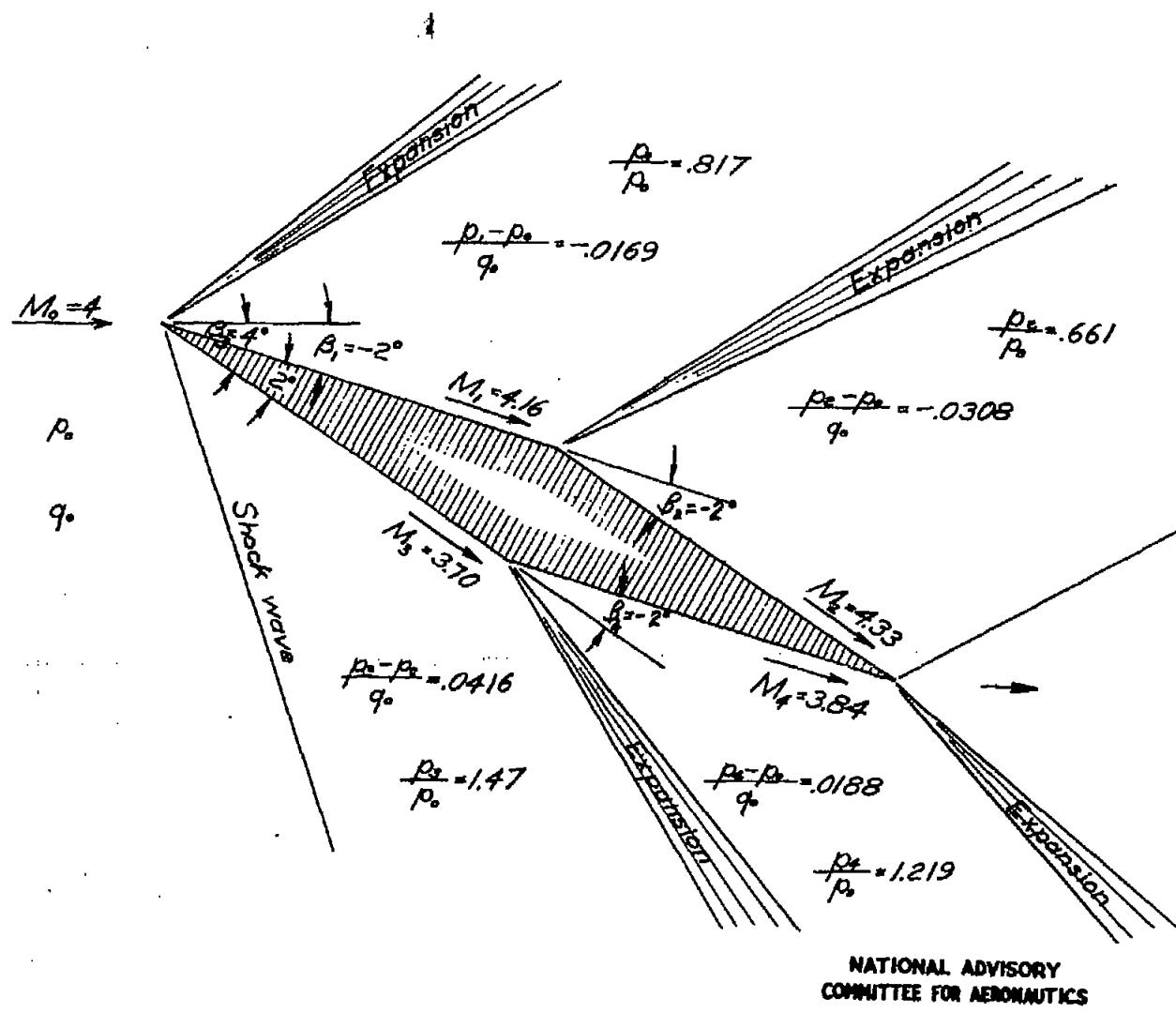
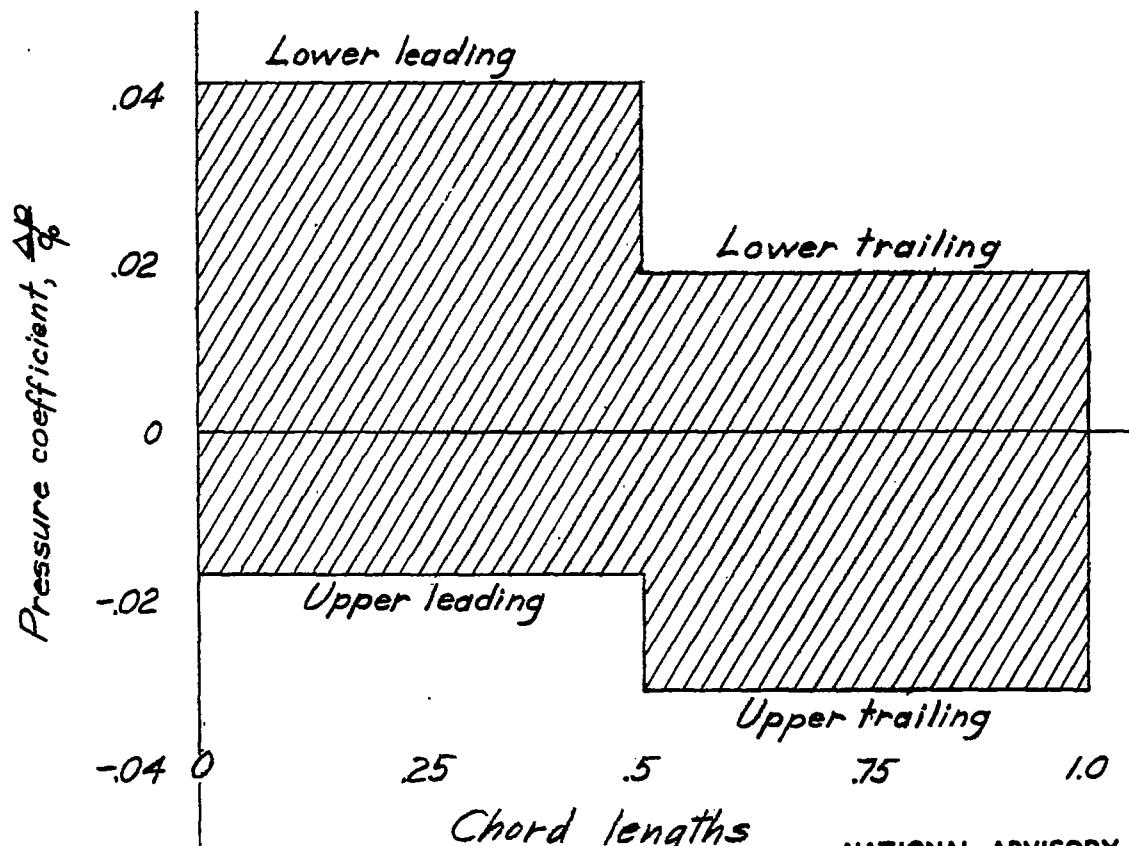


Figure 9. -- Example airfoil (showing results obtained).



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Figure 10.- Determination of lift coefficient from pressure distribution for example airfoil of figures 7 and 9. Value obtained by integrating shaded area gives lift coefficient, 0.0540.

FIG. 11

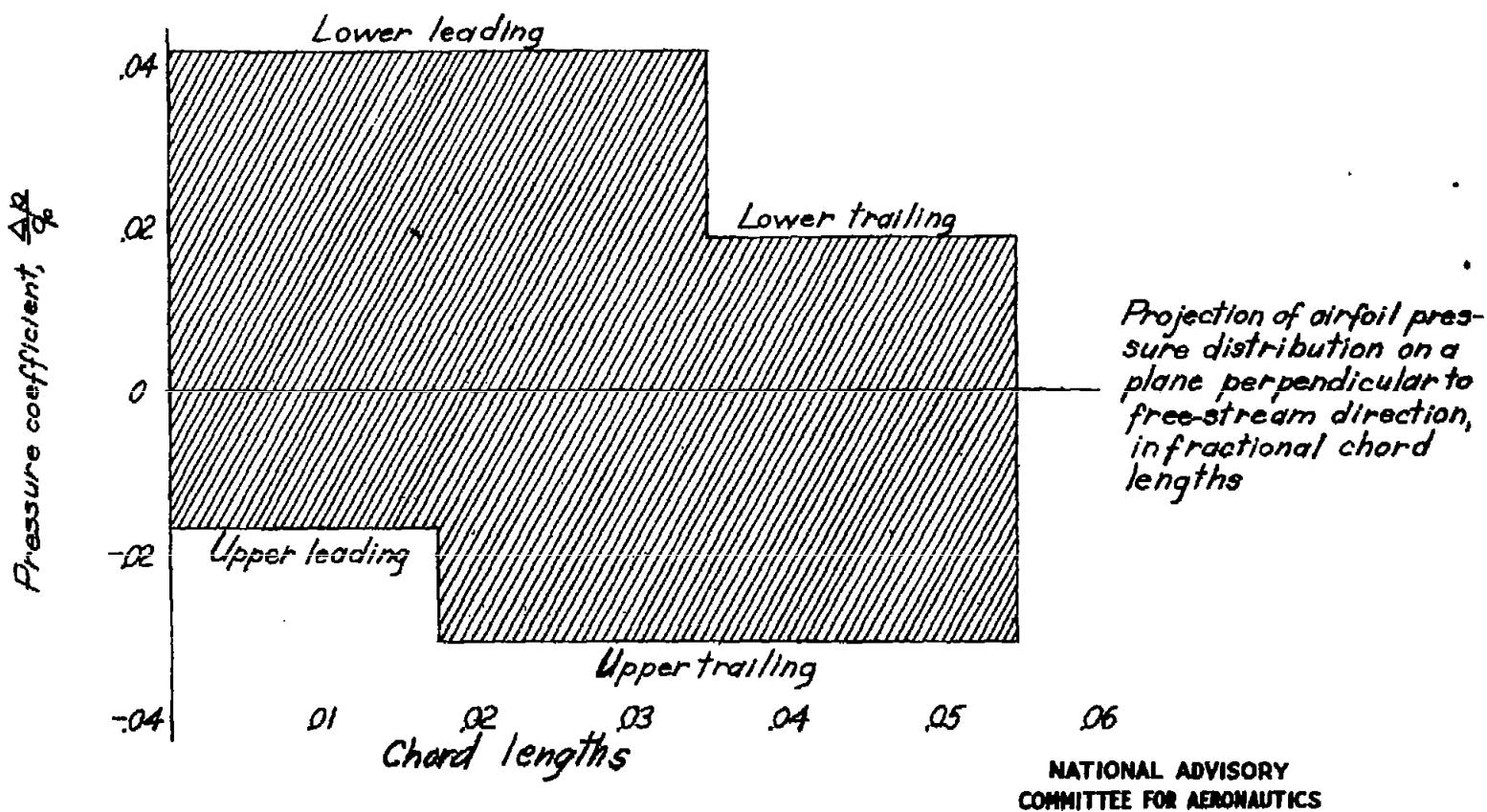


Figure 11.- Determination of drag coefficient from pressure distribution for example airfoil of figures 7 and 9. Value obtained by integrating shaded area gives pressure drag coefficient, 0.00315.

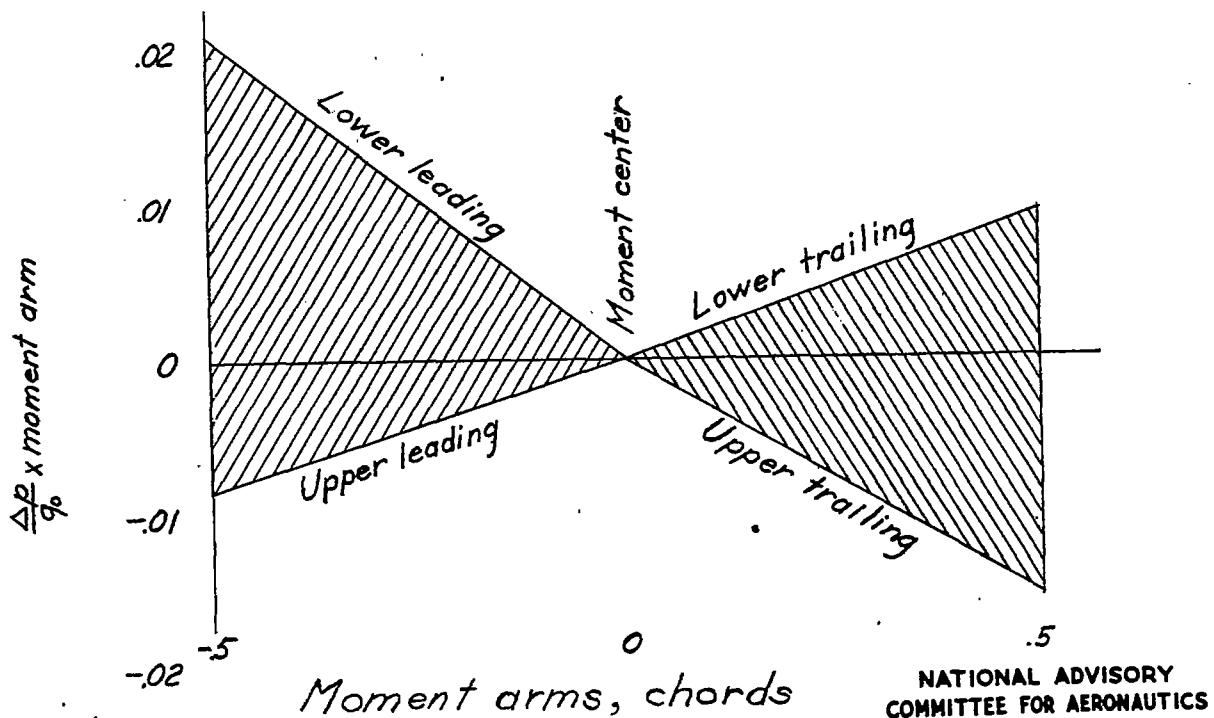


Figure 12.- Determination of moment coefficient from pressure distribution for example airfoil of figures 7 and 9. If leading and trailing surfaces give moments in the same sense add the area between "upper leading" and "lower leading" to that between "upper trailing" and "lower trailing" lines. The value obtained by integrating shaded area gives the moment coefficient about 0.50 chord, 0.0001112.

Fig. 13

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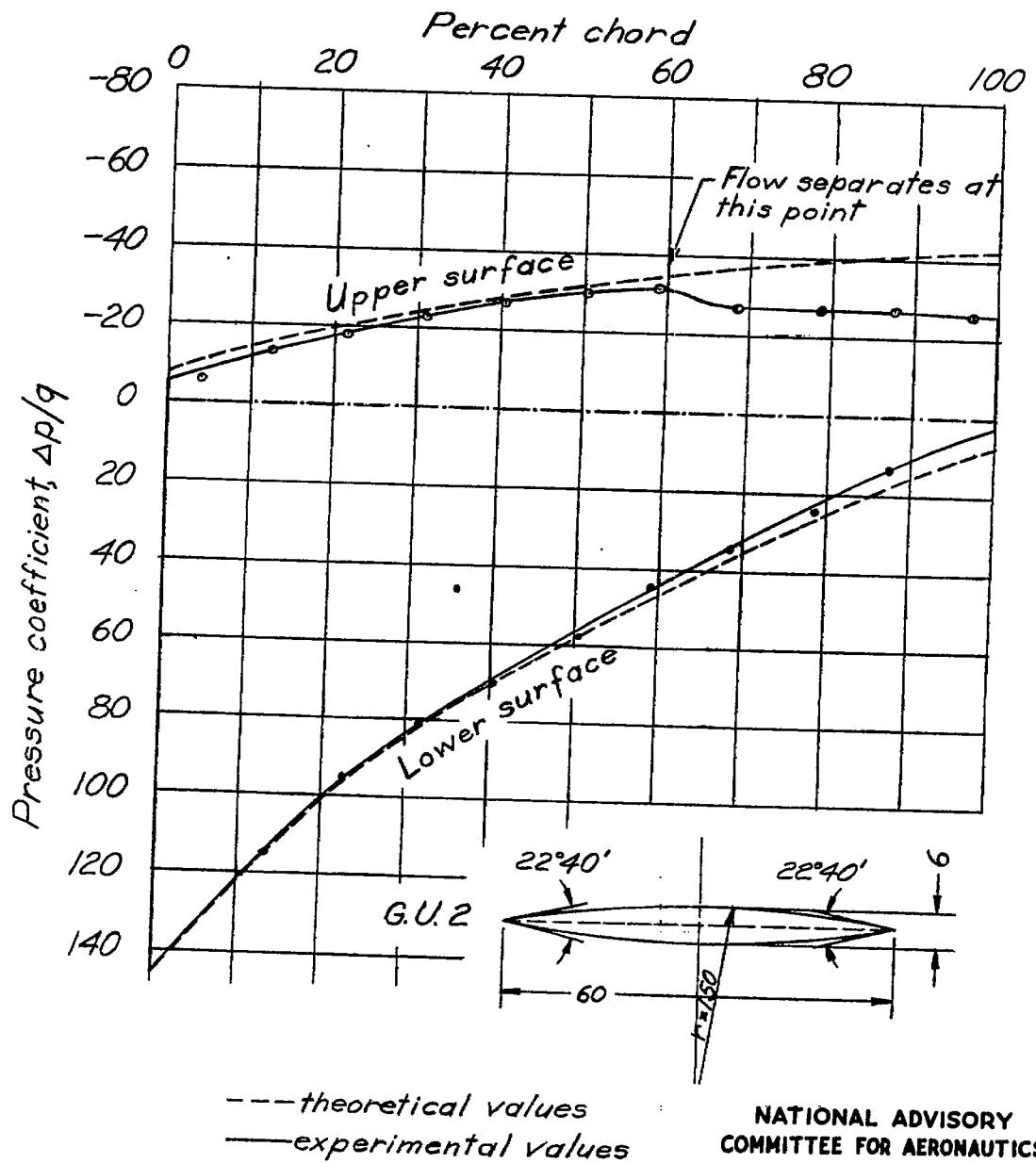


Figure 13.- Comparison of calculated and experimental results from NACA TM No. 946. $\alpha = 14^\circ$; $M_\infty = 2.13$; $R = 640,000$; thickness = 0.10 chord.

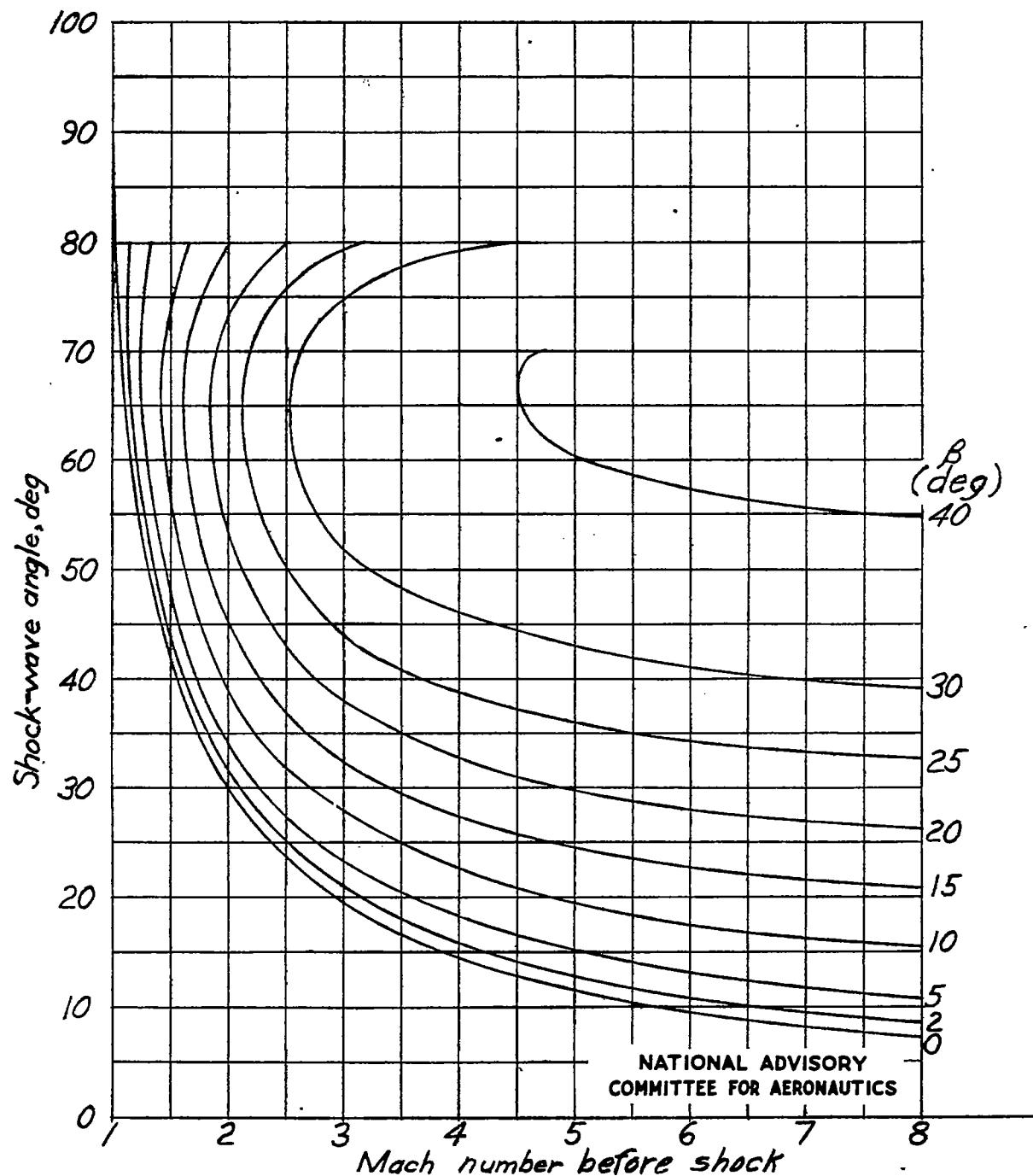


Figure 14.- Shock-wave angle for air.

A/CAC

SUPPLEMENT

NACA TECHNICAL NOTE NO. 1143

CHARTS FOR DETERMINING THE CHARACTERISTICS OF
SHARP-NOSE AIRFOILS IN TWO-DIMENSIONAL
FLOW AT SUPERSONIC SPEEDS

By H. Reese Ivey, George W. Stickle,
and Alberta Schuettler

September 1947

Since Technical Note No. 1143 was completed, the need for a more extensive version of table I, "Values of Local Mach Number, Pressure Ratio, and Pressure Coefficient across Shock Waves," has become apparent. This table is now available in expanded form; and a copy of the expanded table is included in this supplement to supersede the original table I.

Errors in the original publication are as follows:

Page 11: The first sentence of the last paragraph should begin "Tables I and III . . ." instead of "Tables I and II . . .".

Corrections in tables II and III are as follows:

Table II.-

M_b	$-\beta$	M_a
2.3	23°	3.4225
2.6	10°	3.0867
4.3	3°	4.5658
4.7	7°	5.4669
4.7	8°	5.5922
4.7	9°	5.7240
6.2	9°	7.9200

Table III.-

M_b	$-\beta$	p_a/p_b
1.4	14°	0.49071
4.7	24°	.02350

Figure 13.- Each vertical space along the scale label for pressure coefficient $\Delta p/q$ should represent 0.125 instead of 20; thus, the vertical scale should appear:

-.500
-.375
-.250
-.125
0
.125
.250
.375
.500
.625
.750
.875
1.000

(Supplement)

TABLE I.—VALUES OF LOCAL Mach NUMBER, PRESSURE RATIO,
AND PRESSURE COEFFICIENT ACROSS SHOCK WAVES

θ (deg)	β (deg)	M_1	M_2	$\frac{P_2}{P_1}$	$\frac{\rho_{2,1}}{\rho_1}$	$\frac{T_2}{T_1}$	$\frac{q_{2,1}}{q_1}$	β (deg)	M_2	M_3	$\frac{P_3}{P_2}$	$\frac{\rho_{3,2}}{\rho_2}$	$\frac{T_3}{T_2}$
8	0	1	7.18545	7.18545	1.0000	0	0	18	0	3.13504	3.23504	1.00000	0
	1	7.18025	7.17979	1.0000	.00390	1.0000	.00390	1	3.13570	3.26934	1.00000	.01138	
	2	7.18030	7.07860	1.0000	.00977	1.0000	.00977	2	3.19116	3.26934	1.00000	.02114	
9	0	1	6.92554	6.39684	1.0000	0	0	19	3.16574	3.46878	1.00000	.03119	
	1	6.87407	6.69177	1.0000	.00731	1.0000	.00731	4	3.16574	3.46878	1.00000	.04113	
	2	6.87407	7.06779	1.0000	.01200	1.0000	.01200	5	3.81570	3.64318	1.00000	.05117	
10	3	8.27834	7.54959	1.0000	.01696	1.0000	.01696	6	4.28333	3.76221	1.00000	.06204	
	4	7.18711	5.70571	1.0000	0	0	0	7	4.17143	3.97952	1.00000	.07297	
	5	7.18711	5.70571	1.0000	.00614	1.0000	.00614	8	5.21582	4.20798	2.00000	.08285	
	6	6.62339	6.28245	1.0000	.01234	1.0000	.01234	9	5.18052	4.17932	1.00000	.09289	
	7	6.62339	6.60495	1.0000	.01532	1.0000	.01532	10	5.18052	4.17932	1.00000	.10282	
	8	6.08263	7.10485	1.0000	.02136	1.0000	.02136	11	5.18052	4.17932	1.00000	.11282	
11	9	7.24092	5.20662	1.0000	0	0	0	12	7.46204	5.96259	1.00000	.12282	
	10	5.91262	5.79571	1.0000	.00716	1.0000	.00716	13	7.46204	5.96259	1.00000	.13282	
	11	6.12773	5.95518	1.0000	.00360	1.0000	.00360	14	7.46204	5.96259	1.00000	.14282	
	12	7.01059	7.01059	1.0000	.00209	1.0000	.00209	15	7.46204	5.96259	1.00000	.15282	
	13	7.83181	7.83181	1.0000	.03334	1.0000	.03334	16	7.46204	5.96259	1.00000	.16282	
12	14	7.83181	7.30617	1.0000	.04004	1.0000	.04004	17	7.46204	5.96259	1.00000	.17282	
	15	7.89777	7.89777	1.0000	0	0	0	18	7.46204	5.96259	1.00000	.18282	
	16	7.07739	4.96751	1.0000	.00739	1.0000	.00739	19	7.46204	5.96259	1.00000	.19282	
	17	7.07739	4.15796	1.0000	.01171	1.0000	.01171	20	7.46204	5.96259	1.00000	.20282	
	18	7.57938	5.38261	1.0000	.02604	1.0000	.02604	21	7.46204	5.96259	1.00000	.21282	
	19	7.57938	5.69113	1.0000	.03334	1.0000	.03334	22	7.46204	5.96259	1.00000	.22282	
	20	7.68933	7.68933	1.0000	.04004	1.0000	.04004	23	7.46204	5.96259	1.00000	.23282	
	21	7.68933	7.68933	1.0000	0	0	0	24	7.46204	5.96259	1.00000	.24282	
	22	7.80760	6.66172	1.0000	.06295	1.0000	.06295	25	7.46204	5.96259	1.00000	.25282	
	23	7.80760	5.3892	1.0000	.03334	1.0000	.03334	26	7.46204	5.96259	1.00000	.26282	
	24	7.13644	6.12865	1.0000	.01171	1.0000	.01171	27	7.46204	5.96259	1.00000	.27282	
	25	7.13644	5.37693	1.0000	.02604	1.0000	.02604	28	7.46204	5.96259	1.00000	.28282	
	26	7.10349	5.3892	1.0000	.03334	1.0000	.03334	29	7.46204	5.96259	1.00000	.29282	
	27	6.71357	5.72223	1.0000	.04004	1.0000	.04004	30	7.46204	5.96259	1.00000	.30282	
	28	6.71357	5.12865	1.0000	0	0	0	31	7.46204	5.96259	1.00000	.31282	
	29	6.13644	5.12865	1.0000	.01171	1.0000	.01171	32	7.46204	5.96259	1.00000	.32282	
	30	6.13644	5.37693	1.0000	.02604	1.0000	.02604	33	7.46204	5.96259	1.00000	.33282	
	31	6.13644	5.3892	1.0000	.03334	1.0000	.03334	34	7.46204	5.96259	1.00000	.34282	
	32	6.13644	5.3892	1.0000	0	0	0	35	7.46204	5.96259	1.00000	.35282	
	33	6.13644	5.3892	1.0000	.01171	1.0000	.01171	36	7.46204	5.96259	1.00000	.36282	
	34	6.13644	5.3892	1.0000	.02604	1.0000	.02604	37	7.46204	5.96259	1.00000	.37282	
	35	6.13644	5.3892	1.0000	.03334	1.0000	.03334	38	7.46204	5.96259	1.00000	.38282	
	36	6.13644	5.3892	1.0000	0	0	0	39	7.46204	5.96259	1.00000	.39282	
	37	6.13644	5.3892	1.0000	.01171	1.0000	.01171	40	7.46204	5.96259	1.00000	.40282	
	38	6.13644	5.3892	1.0000	.02604	1.0000	.02604	41	7.46204	5.96259	1.00000	.41282	
	39	6.13644	5.3892	1.0000	.03334	1.0000	.03334	42	7.46204	5.96259	1.00000	.42282	
	40	6.13644	5.3892	1.0000	0	0	0	41	7.46204	5.96259	1.00000	.43282	
	42	6.13644	5.3892	1.0000	.01171	1.0000	.01171	43	7.46204	5.96259	1.00000	.44282	
	44	6.13644	5.3892	1.0000	.02604	1.0000	.02604	45	7.46204	5.96259	1.00000	.45282	
	45	6.13644	5.3892	1.0000	.03334	1.0000	.03334	46	7.46204	5.96259	1.00000	.46282	
	47	6.13644	5.3892	1.0000	0	0	0	48	7.46204	5.96259	1.00000	.47282	
	49	6.13644	5.3892	1.0000	.01171	1.0000	.01171	50	7.46204	5.96259	1.00000	.48282	
	51	6.13644	5.3892	1.0000	.02604	1.0000	.02604	52	7.46204	5.96259	1.00000	.49282	
	53	6.13644	5.3892	1.0000	.03334	1.0000	.03334	54	7.46204	5.96259	1.00000	.50282	
	55	6.13644	5.3892	1.0000	0	0	0	56	7.46204	5.96259	1.00000	.51282	
	57	6.13644	5.3892	1.0000	.01171	1.0000	.01171	58	7.46204	5.96259	1.00000	.52282	
	59	6.13644	5.3892	1.0000	.02604	1.0000	.02604	60	7.46204	5.96259	1.00000	.53282	
	61	6.13644	5.3892	1.0000	.03334	1.0000	.03334	62	7.46204	5.96259	1.00000	.54282	
	63	6.13644	5.3892	1.0000	0	0	0	64	7.46204	5.96259	1.00000	.55282	
	65	6.13644	5.3892	1.0000	.01171	1.0000	.01171	66	7.46204	5.96259	1.00000	.56282	
	67	6.13644	5.3892	1.0000	.02604	1.0000	.02604	68	7.46204	5.96259	1.00000	.57282	
	69	6.13644	5.3892	1.0000	.03334	1.0000	.03334	70	7.46204	5.96259	1.00000	.58282	
	71	6.13644	5.3892	1.0000	0	0	0	72	7.46204	5.96259	1.00000	.59282	
	73	6.13644	5.3892	1.0000	.01171	1.0000	.01171	74	7.46204	5.96259	1.00000	.60282	
	75	6.13644	5.3892	1.0000	.02604	1.0000	.02604	76	7.46204	5.96259	1.00000	.61282	
	77	6.13644	5.3892	1.0000	.03334	1.0000	.03334	78	7.46204	5.96259	1.00000	.62282	
	79	6.13644	5.3892	1.0000	0	0	0	80	7.46204	5.96259	1.00000	.63282	
	81	6.13644	5.3892	1.0000	.01171	1.0000	.01171	82	7.46204	5.96259	1.00000	.64282	
	83	6.13644	5.3892	1.0000	.02604	1.0000	.02604	84	7.46204	5.96259	1.00000	.65282	
	85	6.13644	5.3892	1.0000	.03334	1.0000	.03334	86	7.46204	5.96259	1.00000	.66282	
	87	6.13644	5.3892	1.0000	0	0	0	88	7.46204	5.96259	1.00000	.67282	
	89	6.13644	5.3892	1.0000	.01171	1.0000	.01171	90	7.46204	5.96259	1.00000	.68282	
	91	6.13644	5.3892	1.0000	.02604	1.0000	.02604	92	7.46204	5.96259	1.00000	.69282	
	93	6.13644	5.3892	1.0000	.03334	1.0000	.03334	94	7.46204	5.96259	1.00000	.70282	
	95	6.13644	5.3892	1.0000	0	0	0	96	7.46204	5.96259	1.00000	.71282	
	97	6.13644	5.3892	1.0000	.01171	1.0000	.01171	98	7.46204	5.96259	1.00000	.72282	
	99	6.13644	5.3892	1.0000	.02604	1.0000	.02604	100	7.46204	5.96259	1.00000	.73282	
	101	6.13644	5.3892	1.0000	.03334	1.0000	.03334	102	7.46204	5.96259	1.00000	.74282	
	103	6.13644	5.3892	1.0000	0	0	0	104	7.46204	5.96259	1.00000	.75282	
	105	6.13644	5.3892	1.0000	.01171	1.0000	.01171	106	7.46204	5.96259	1.00000	.76282	
	107	6.13644	5.3892	1.0000	.02604	1.0000	.02604	108	7.46204	5.96259	1.00000	.77282	
	109	6.13644	5.3892	1.0000	.03334	1.0000	.03334	110	7.46204	5.96259	1.00000	.78282	
	111	6.13644	5.3892	1.0000	0	0	0						

**TABLE I.—VALUES OF LOCAL MASS NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES — Continued**

TABLE I.—VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES—Continued

θ (deg)	β (deg)	M_0	M_∞	$\frac{P_\infty}{P_0}$	$\frac{\alpha_{s,b}}{\alpha_b}$	θ (deg)	β (deg)	M_0	M_∞	$\frac{P_\infty}{P_0}$	$\frac{\alpha_{s,b}}{\alpha_b}$
30	20	4.90159	3.00520	6.84081	0.34730	34	0	1.78889	1.78889	1.00000	0
	21	5.56424	3.12679	8.86354	0.36884		1	1.80960	1.79493	1.05433	.023271
	22	6.50991	3.30392	12.49554	0.37829		2	1.87291	1.86309	1.11302	.046268
	23	8.51233	3.51723	20.96744	0.39367		3	1.91837	1.81963	1.17591	.060285
31	0	1.98160	1.94160	1.00000	0	35	0	2.01588	1.83741	1.31733	.11145
	1	1.98866	1.92285	1.05748	0.02076		1	1.85237	1.79734	1.32420	
	2	2.03868	1.96998	1.11993	0.04110		2	2.07054	1.85237	1.39240	
	3	2.09138	1.98107	1.18691	0.06106		3	2.12758	1.88470	1.48977	
	4	2.14730	1.99823	1.26023	0.08064		4	2.18849	1.88824	1.50061	.17318
32	5	2.26684	2.01760	1.34052	.09989	36	5	2.25376	1.90535	1.68638	.19304
	6	2.27049	2.03933	1.42871	.11880		6	2.38403	1.93285	1.80374	.21259
	7	2.33886	2.06359	1.52616	.13741		7	2.40006	1.95594	1.93476	.23182
	8	2.41247	2.09061	1.63149	.15574		8	2.48279	1.98784	2.08213	.25078
	9	2.49238	2.12066	1.75569	.17379		9	2.57339	2.01966	2.28923	.26948
33	10	2.57936	2.15392	1.89230	.19160	37	10	2.67317	2.05523	2.44024	.28793
	11	2.67484	2.19086	2.04755	.20916		11	2.78406	2.07095	2.66102	.30614
	12	2.78034	2.23185	2.22267	.22651		12	2.90884	2.13794	2.91930	.32413
	13	2.89789	2.27719	2.41223	.24364		13	3.04938	2.18628	3.22562	.34192
	14	3.03011	2.32809	2.67480	.26058		14	3.21114	2.24018	3.59506	.36953
34	15	3.18052	2.38468	2.96380	.27735	38	15	3.39907	2.30049	4.04968	.37696
	16	3.35393	2.44806	3.14456	.29304		16	3.62346	2.36928	4.62314	.39422
	17	3.52709	2.51939	3.49509	.31028		17	3.89559	2.44492	5.36960	.41134
	18	3.79953	2.60008	4.30204	.32668		18	4.25983	2.53215	6.38199	.42831
	19	4.09778	2.69201	5.02997	.34265		19	4.68313	2.63228	7.83454	.44517
35	20	4.47555	2.79760	6.03228	.35820	39	20	6.25346	2.88475	14.09971	.47851
	21	4.97767	2.92012	7.30125	.37484		21	7.99488	3.04745	23.15148	.49509
	22	5.69308	3.06049	9.86355	.39068		22	1.74345	1.74345	1.00000	0
	23	6.83365	3.23596	14.29389	.40644		23	1.78316	1.74787	1.05375	.02415
	24	9.13076	3.44528	25.63452	.42212		24	1.82468	1.75553	1.11126	.04774
36	0	1.88707	1.88707	1.00000	0	40	0	1.96221	1.78504	1.31116	.11545
	1	1.93413	1.89664	1.05639	0.01818		1	2.01382	1.79813	1.38987	.13710
	2	1.97596	1.90799	1.11716	0.04271		2	2.06730	1.81304	1.47363	.15834
	3	2.02958	1.92112	1.18287	0.06342		3	2.12857	1.82981	1.56832	.17918
	4	2.08253	1.93650	1.25420	0.08373		4	2.18638	1.84859	1.66810	.19966
37	5	2.13871	1.95330	1.33195	.10367	41	5	2.25928	1.86953	1.78044	.21979
	6	2.15668	1.97526	1.41711	.12326		6	2.38352	1.89278	1.90548	.23960
	7	2.26277	2.00680	1.51078	.14051		7	2.40738	1.91845	2.04521	.25910
	8	2.33167	2.01807	1.61445	.16145		8	2.48753	1.94707	2.20263	.27832
	9	2.40596	2.04748	1.72082	.18030		9	2.57688	2.38143	.29727	
38	10	2.48663	2.07445	1.89515	.19819	42	10	2.67822	2.01351	2.58644	.31996
	11	2.57474	2.10730	2.00522	.21562		11	2.79139	2.05213	2.86101	.33412
	12	2.67149	2.14373	2.17150	.23490		12	2.91598	2.09486	3.10277	.35366
	13	2.77856	2.18409	2.36269	.25215		13	3.06314	2.14298	3.43466	.37069
	14	2.89312	2.22897	2.58506	.26960		14	3.22962	2.19562	3.83673	.38953
39	15	3.03292	2.27584	2.84700	.28634	43	15	3.48442	2.29495	4.33427	.40619
	16	3.18572	2.33481	3.16503	.30390		16	3.65692	2.32162	4.96621	.42669
	17	3.36359	2.39688	3.54210	.32080		17	3.94150	2.39697	5.75616	.44103
	18	3.57385	2.46700	4.01779	.33753		18	4.30133	2.42872	6.93526	.45984
	19	3.82331	2.54630	4.62734	.35413		19	4.64442	2.49495	4.33427	.40619
40	20	4.13577	2.63661	5.43708	.37058	44	20	3.48442	2.52495	4.33427	.40619
	21	4.53231	2.74033	6.56585	.38692		21	3.65692	2.53162	4.96621	.42669
	22	5.06390	2.88280	8.89711	.40315		22	3.94150	2.59616	.44103	
	23	5.68704	3.00200	11.03366	.41921		23	4.30233	2.62126	5.09115	
	24	7.13785	3.17071	16.56204	.43531		24	5.45400	2.68921	16.16903	
41	25	9.97414	3.37616	32.42577	.45127	45	25	6.58305	2.69893	38.38910	.52291
	26	1.83608	1.83608	1.00000	0		26	1.70130	1.70130	1.00000	0
	27	1.87918	1.84413	1.07541	.00242		27	1.73953	1.70339	1.05304	.045040
	28	1.92442	1.89381	1.11497	.04453		28	1.77947	1.71085	1.10569	.061487
	29	1.97206	1.88390	1.17920	.06583		29	1.88126	1.77722	1.17033	.073358
42	30	2.08233	1.87836	1.24872	.08688	46	30	1.86536	1.72606	1.23583	.096830
	31	2.07561	1.89338	1.32426	.10752		31	1.91119	1.73654	1.30563	.11553
	32	2.13221	1.91039	1.40668	.12779		32	1.95980	1.74734	1.38117	.13489
	33	2.19298	1.92947	1.49703	.14770		33	2.01181	1.76042	1.46381	.16380
	34	2.25722	1.93082	1.59687	.16727		34	2.06595	1.77522	1.52356	.18630
43	35	2.30722	1.94082	1.70686	.18653	47	35	2.12402	1.79189	1.65178	.20639
	36	2.37451	2.00099	1.88982	.20796		36	2.18626	1.81048	1.73992	.22713
	37	2.45351	2.03026	1.96184	.22417		37	2.25305	1.83118	1.87943	.24740
	38	2.57274	2.06268	2.12398	.24259		38	2.35217	1.88448	2.01251	.26754
	39	2.67094	2.06559	2.30217	.26076		39	2.40336	1.87960	2.16172	.28728
44	40	2.77983	2.13838	2.50737	.27870	48	40	2.48870	1.90778	2.32582	.30673
	41	2.89165	2.18855	2.74709	.29943		41	2.58245	1.93889	2.52146	.32591
	42	3.03936	2.21168	3.03020	.31396		42	2.65612	1.97330	2.74261	.34483
	43	3.19659	2.28614	3.37080	.33131		43	2.80180	2.01136	2.99730	.36351
	44	3.31971	2.34772	3.48644	.35848		44	2.93215	2.05355	3.29879	.38397
45	45	3.37977	2.41669	4.30816	.36549	49	45	3.08076	2.10040	3.65994	.40022
	46	3.89704	2.49164	4.98375	.38235		46	3.25251	2.15260	4.09738	.41827
	47	4.18188	2.58339	5.88935	.39908		47	3.45439	2.21098	5.74361	.43613
	48	4.60196	2.68928	7.16241	.41569		48	3.69669	2.27695	5.34153	.45386
	49	5.17619	2.80347	9.10556	.43218		49	3.99543	2.35063	6.26779	.47141
46	50	6.03169	2.94229	12.42298	.44257	50	50	4.0889	2.53169	9.47123	.50612
	51	7.51179	3.10795	19.37661	.46487		51	5.63258	2.66431	12.62122	.52329
	52	11.19767	3.533991	43.22365	.48109		52				

TABLE I - VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES - Continued

θ (deg)	β (deg)	M_b	M_a	P_a P_b	$\frac{\rho_{a,b}}{\rho_b}$	θ (deg)	β (deg)	M_b	M_a	P_a P_b	$\frac{\rho_{a,b}}{\rho_b}$
36	27	6.85490	2.77549	18.77364	0.54035	39	17	2.51569	1.70763	2.75938	0.39689
	28	9.49197	2.93292	36.14927	0.57732		18	2.61643	1.82749	2.99641	.41661
37	0	1.66154	1.66154	1.00000	0		19	2.72771	1.86043	3.27119	.43607
1	1.66937	1.66937	1.05244	.06297		20	2.85280	1.89684	3.39373	.45529	
2	1.73705	1.66883	1.20831	.08128		21	2.99599	1.95714	3.97793	.47427	
3	1.77726	1.67443	1.16800	.07938		22	3.13879	1.98182	4.44366	.49304	
4	1.81934	1.68140	1.23196	.10011		23	3.35092	2.03163	5.02033	.51161	
5	1.86351	1.68980	1.30070	.12370		24	3.68530	2.09759	6.03867	.52999	
6	1.91000	1.69987	1.37483	.14878		25	3.89991	2.11968	6.71741	.54821	
7	1.95907	1.71107	1.45959	.16938		26	4.21505	2.22019	8.04246	.56627	
8	2.01103	1.72408	1.54221	.19153		27	4.68611	2.30037	9.97979	.58418	
9	2.06623	1.73879	1.63730	.21329		28	5.35512	2.39231	13.08374	.60196	
10	2.12508	1.75530	1.74154	.23458		29	6.41824	2.49983	15.86568	.61961	
11	2.18809	1.77373	1.82637	.25752		30	8.52952	2.68289	33.44866	.63716	
12	2.25584	1.79422	1.98358	.28612		31	1.55572	1.75572	1.00000	0	
13	2.39303	1.81694	2.18538	.30638		32	1.58540	1.75555	1.05106	.02887	
14	2.40896	1.84209	2.28541	.31643		33	1.66120	1.75877	1.16315	.05693	
15	2.49541	1.86986	2.46036	.33599		34	1.69843	1.76231	1.22384	.11085	
16	2.50099	1.90044	2.66997	.35937		35	1.73791	1.56691	1.28916	.13677	
17	2.66664	1.93445	2.90670	.37449		36	1.77912	1.77276	1.35914	.16209	
18	2.81543	1.97195	3.18269	.39349		37	1.82243	1.77953	1.43431	.18581	
19	2.94931	2.01350	3.30881	.41203		38	1.86797	1.58841	1.51532	.21098	
20	3.10242	2.05963	3.90033	.43048		39	1.91599	1.79823	1.60291	.23462	
21	3.26008	2.11101	4.37946	.44973		40	1.96679	1.60950	1.69799	.25777	
22	3.48591	2.16944	4.97971	.46679		41	2.02078	1.62230	1.80163	.28046	
23	3.74331	2.23293	5.75420	.48469		42	2.07818	1.63666	1.91919	.30672	
24	4.05823	2.30983	6.79240	.50284		43	2.13960	1.65272	.84007	.32456	
25	4.46512	2.38973	8.89775	.52004		44	2.20564	1.67062	2.17538	.34603	
26	5.02050	2.48183	10.48377	.53751		45	2.27694	1.69040	2.33224	.36713	
27	5.84360	2.59406	11.27160	.55487		46	2.35412	1.71233	2.50474	.38769	
28	7.27343	2.72343	22.17482	.57211		47	2.49044	1.73651	2.69953	.40833	
29	10.76973	2.87776	45.84307	.58927		48	2.53106	1.76318	2.92239	.42846	
30	1.62427	1.62427	1.00000	0		49	2.71794	1.82907	3.47330	.46791	
1	1.66000	1.66610	1.05191	.02691		50	2.81761	1.86290	3.82297	.48766	
2	1.69720	1.66911	1.10711	.05312		51	2.93106	1.79260	3.17655	.44832	
3	1.73592	1.68336	1.16292	.07867		52	2.74794	1.82997	4.21135	.50637	
4	1.77646	1.68334	1.22888	.10361		53	3.08399	1.90062	4.21135	.50637	
5	1.81891	1.64539	1.29635	.12796		54	3.19428	1.94465	4.71227	.53227	
6	1.86348	1.69484	1.36952	.15177		55	3.39454	1.99304	5.30688	.54396	
7	1.91042	1.66471	1.44727	.17907		56	3.63476	2.04837	6.201171	.56247	
8	1.95999	1.67607	1.53211	.19789		57	3.93174	2.10980	7.28997	.58061	
9	2.01534	1.68903	1.62841	.22023		58	4.11206	2.12916	8.79627	.60899	
10	2.06839	1.70361	1.72224	.24117		59	4.38461	2.28302	11.09366	.61702	
11	2.12800	1.71998	1.83385	.26569		60	5.37095	2.34844	14.79363	.63492	
12	2.19194	1.73387	1.95797	.28484		61	6.81144	2.47220	22.19783	.66270	
13	2.26069	1.75246	2.09337	.30562		62	9.55562	2.57613	43.84821	.67037	
14	2.33512	1.77819	2.24461	.32607		63	1.52405	1.52405	1.00000	0	
15	2.41604	1.80577	2.41163	.34261		64	1.52704	1.52310	1.05073	.08369	
16	2.50164	1.83318	2.60714	.36657		65	1.59100	1.56326	1.10441	.08392	
17	2.66229	1.86344	2.82763	.38562		66	1.62623	1.52450	1.16133	.08714	
18	2.71076	1.89688	3.08280	.40498		67	1.66286	1.58688	1.22103	.11461	
19	2.83237	1.93381	3.38091	.42398		68	1.70103	1.53043	1.28631	.14135	
20	2.97018	1.97473	3.73452	.44261		69	1.74050	1.55516	1.35521	.16743	
21	3.12834	2.02015	4.16104	.46213		70	1.78264	1.54110	1.49006	.19288	
22	3.31262	2.07078	4.6894	.47983		71	1.86614	1.51889	1.50885	.21774	
23	3.52313	2.12723	5.34815	.49809		72	1.97255	1.55577	1.59406	.24204	
24	3.79744	2.19070	6.21029	.51616		73	2.1562	1.63631	2.29637	.37764	
25	4.13302	2.26238	7.37982	.53107		74	2.28227	1.67768	2.46267	.39906	
26	4.56731	2.34390	9.05803	.55184		75	2.36721	1.67551	2.64721	.41993	
27	5.17392	2.43741	11.67110	.58647		76	2.45349	1.70337	2.85606	.44048	
28	6.10326	2.56542	16.30565	.60669		77	2.54845	1.72968	3.09460	.46073	
29	7.80869	2.67296	26.79741	.63440		78	2.69378	1.75868	3.36774	.48070	
30	12.89714	2.82162	73.38925	.66217		79	2.82152	1.77768	3.7768	.50040	
31	0	1.58902	1.58902	1.00000	0		80	2.97780	1.77780	3.95549	.52039
1	1.63367	1.58983	1.05145	.02788		81	3.0749	1.8049	3.11921	.53195	
2	1.69967	1.59190	1.10605	.05500		82	3.09588	1.86174	3.13429	.54221	
3	1.69713	1.59537	1.16416	.08314		83	3.18439	1.90468	3.15104	.55268	
4	1.73622	1.59970	1.22627	.10718		84	3.21562	1.93631	2.98637	.37764	
5	1.77709	1.60950	1.29251	.13232		85	3.26227	1.97768	2.46267	.39906	
6	1.81998	1.61261	1.36371	.15857		86	3.36721	2.01551	2.64721	.41993	
7	1.86495	1.62107	1.44035	.18087		87	3.45349	2.05337	2.85606	.44048	
8	1.92139	1.63094	1.53317	.20436		88	3.53473	1.90844	3.08756	.55807	
9	1.96235	1.64227	1.61298	.22735		89	3.44438	1.95667	2.79072	.57687	
10	2.03575	1.65531	1.71076	.24689		90	3.58607	2.01053	2.70095	.59549	
11	2.07236	1.66963	1.81770	.27200		91	3.69807	2.07098	2.98492	.61359	
12	2.13289	1.68584	1.93523	.29370		92	4.12829	2.13921	3.66220	.63221	
13	2.19774	1.70390	2.06908	.31501		93	4.98692	2.21677	12.32147	.65034	
14	2.25769	1.72394	2.20939	.33597		94	5.83108	2.30570	16.90715	.66831	
15	2.31434	1.74612	2.37081	.35689		95	7.31588	2.40671	26.70940	.68622	
16	2.42599	1.77061	2.55271	.37689		96	11.16427	2.52958	62.42147	.70398	

TABLE I.—VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES—Continued

θ (deg)	β (deg)	M_b	M_a	P_a P_b	$\frac{\Delta P_{sh}}{P_b}$	θ (deg)	β (deg)	M_b	M_a	P_a P_b	$\frac{\Delta P_{sh}}{P_b}$
42	0	1.49148	1.49148	1.00000	0	44	15	2.05902	1.50014	2.22011	0.41113
	1	1.52646	1.49255	1.03047	.03094		16	2.12083	1.51398	2.36599	.43372
	2	1.55533	1.49172	1.10379	.06096		17	2.18729	1.52938	2.52675	.45559
	3	1.59084	1.48920	1.15025	.09046		18	2.25905	1.54644	2.70657	.47767
	4	1.63013	1.49331	1.22140	.11902		19	2.33696	1.56530	2.90755	.49908
	5	1.66942	1.49592	1.28382	.14604		20	2.42205	1.58610	3.13593	.52014
	6	1.70602	1.50017	1.35186	.17270		21	2.51562	1.60901	3.36602	.54088
	7	1.74533	1.50437	1.42453	.19909		22	2.61929	1.63424	3.69573	.56132
	8	1.78759	1.51057	1.50251	.22465		23	2.73318	1.66802	4.04507	.58147
	9	1.83196	1.51756	1.58642	.24962		24	2.86606	1.69262	4.45777	.60135
	10	1.87871	1.52603	1.67703	.27402		25	3.01567	1.72639	4.95312	.62098
	11	1.92809	1.53383	1.77522	.29790		26	3.18913	1.76371	5.59510	.64038
	12	1.98043	1.54697	1.88207	.32181		27	3.39390	1.80908	6.31798	.68956
	13	2.03608	1.55958	1.99382	.34419		28	3.64100	1.85407	7.29665	.67693
	14	2.09550	1.57370	1.27067	.36697		29	3.94787	1.90240	8.60787	.69731
	15	2.15919	1.58941	2.26861	.38873		30	4.34390	1.99998	10.45639	.71592
	16	2.22779	1.60689	2.42582	.41041		31	4.88378	2.02895	13.26101	.73437
	17	2.30202	1.62622	2.60146	.43172		32	5.68455	2.09877	18.02541	.75287
	18	2.38280	1.64758	2.79914	.45263		33	7.06275	2.18337	27.91591	.77084
	19	2.47126	1.67112	3.02345	.47332		34	10.41348	2.29901	60.88204	.78888
	20	2.56883	1.69707	3.28032	.49366	45	0	1.41121	1.41121	1.00000	0
	21	2.67731	1.72566	3.57778	.51371		1	1.44426	1.40982	1.09010	.03431
	22	2.79904	1.75719	3.92561	.53350		2	1.47521	1.40658	1.10283	.08748
	23	2.93714	1.79159	4.33962	.55303		3	1.50714	1.40419	1.15836	.09960
	24	3.09586	1.83048	4.83980	.57433		4	1.54015	1.40293	1.21704	.13071
	25	3.28113	1.87316	5.45656	.59242		5	1.57434	1.40869	1.27915	.16000
	26	3.50161	1.92063	6.23811	.61030		6	1.60983	1.40348	1.34507	.19022
	27	3.77045	1.97364	7.29535	.62899		7	1.64873	1.40529	1.41516	.21871
	28	4.10893	2.03311	8.62474	.64731		8	1.68918	1.40814	1.48991	.24645
	29	4.55417	2.10024	10.69728	.66987		9	1.72536	1.41805	1.56983	.27346
	30	5.17863	2.17633	13.84204	.68408		10	1.76742	1.41703	1.65554	.29979
	31	6.11927	2.26399	19.58813	.70216		11	1.81159	1.42311	1.74775	.32949
	32	7.98864	2.38162	33.18941	.72011		12	1.88909	1.43032	1.84730	.35059
	33	14.19485	2.48414	105.09355	.73795		13	1.90720	1.43872	1.95519	.37313
	0	1.46628	1.46628	1.00000	0		14	1.95922	1.44834	2.07248	.39914
43	1	1.49735	1.46349	1.05029	.03203		15	2.01152	1.45925	2.20066	.42260
	2	1.56864	1.46179	1.10313	.06307		16	2.07352	1.47151	2.34137	.44569
	3	1.63282	1.46318	1.15911	.09319		17	2.13674	1.48521	2.46664	.46939
	4	1.59788	1.46105	1.21082	.12243		18	2.20479	1.50043	2.66397	.49047
	5	1.63395	1.46320	1.28150	.15086		19	2.27839	1.51729	2.86144	.51227
	6	1.67130	1.46984	1.34907	.17853		20	2.35843	1.53591	3.07796	.53369
	7	1.71037	1.46959	1.42075	.20474		21	2.44664	1.55643	3.32348	.55477
	8	1.75322	1.47447	1.49749	.23174		22	2.52452	1.57903	3.60444	.57553
	9	1.79404	1.48050	1.57988	.25738		23	2.61952	1.60390	3.92932	.59971
	10	1.83906	1.48772	1.66862	.28446		24	2.77011	1.63127	4.30955	.61614
	11	1.88651	1.49617	1.76452	.30590		25	2.90641	1.66142	4.76068	.63603
	12	1.93668	1.50951	1.86864	.33085		26	3.06297	1.69468	5.30568	.65567
	13	1.98991	1.51698	1.98205	.35430		27	3.21525	1.73143	5.97680	.67508
	14	2.04677	1.52347	2.10617	.37728		28	3.46192	1.77215	6.82452	.69427
	15	2.10714	1.54345	2.24267	.39983		29	3.72936	1.81741	7.98987	.71325
44	2	2.17214	1.55902	2.30362	.42196	46	30	4.05613	1.86793	9.43244	.73205
	3	2.24223	1.57689	2.56152	.44370		31	4.49028	1.92458	11.55489	.75067
	4	2.31220	1.59539	2.74923	.46927		32	5.02909	1.98849	14.97662	.76913
	5	2.40103	1.61646	2.96164	.48810		33	6.02850	2.06110	21.01927	.78144
	6	2.49191	1.63699	3.20294	.50680		34	7.75492	2.14431	34.91428	.80562
	7	2.59237	1.66928	3.48010	.52720		35	13.13487	2.24066	100.47277	.82367
	8	2.70435	1.69346	3.80196	.54731		36	1.39016	1.39016	1.00000	0
	9	2.83381	1.72502	4.18819	.56715		37	1.41969	1.38498	1.05010	.03751
	10	2.97391	1.75581	4.63254	.58765		38	1.45008	1.38088	1.10274	.06880
	11	3.13397	1.79767	5.18317	.60612		39	1.48138	1.37779	1.15813	.10294
	12	3.33334	1.83873	5.86488	.62926		40	1.51715	1.37164	1.27639	.16615
	13	3.56680	1.88443	6.73684	.65240		41	1.58181	1.37540	1.34384	.19631
	14	3.85318	1.93762	7.85996	.68693		42	1.61778	1.37744	1.48726	.22662
	15	4.21747	1.99634	9.48750	.72050		43	1.69426	1.39037	1.56926	.26181
	16	4.70573	2.06218	11.84551	.69094		44	1.73383	1.48431	1.65076	.30861
	17	5.40747	2.13722	15.70056	.72800		45	1.77783	1.53926	1.74144	.33512
	18	6.34844	2.22324	21.10298	.73634		46	1.82279	1.59513	1.83915	.36080
	19	8.93939	2.32807	43.19741	.75343		47	1.87013	1.64266	1.94478	.39889
	0	1.43955	1.43955	1.00000	0		48	1.92023	1.64102	2.05931	.41041
44	1	1.47017	1.43955	1.05016	.03135		49	1.97330	1.42055	2.18408	.43441
	2	1.50173	1.43340	1.10300	.06524		50	2.02682	1.43136	2.32064	.45790
	3	1.53339	1.43194	1.15878	.09634		51	2.09018	1.44353	2.47077	.48093
	4	1.56816	1.43154	1.21777	.12691		52	2.15595	1.45708	2.63675	.50351
	5	1.60320	1.43215	1.28033	.15581		53	2.20047	1.47422	2.82333	.52568
	6	1.63690	1.43385	1.34680	.18429		54	2.30039	1.48878	3.02792	.54746
	7	1.67754	1.43299	1.41765	.21202		55	2.38282	1.50715	3.26098	.56888
	8	1.71712	1.44044	1.49329	.23900		56	2.47309	1.52968	3.52956	.58994
	9	1.75535	1.44356	1.57743	.26532		57	2.58435	1.57419	3.83023	.61068
	10	1.80201	1.45113	1.66148	.29101		58	2.68435	1.60116	4.18338	.63112
	11	1.84773	1.45388	1.75442	.31608		59	2.80592	1.65952	4.59811	.65327
	12	1.89597	1.46707	1.87710	.34062		60	2.86404	1.70816	5.00121	.67444
	13	1.94702	1.47467	1.96734	.36461		61	2.92745	1.75922	5.53127	.69559
	14	2.00123	1.48774	2.08004	.37474		62	2.98592	1.80116	6.03277	.71671

TABLE I.—VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES — Continued

θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_{sh}}{P_b}$	θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_{sh}}{P_b}$
46	26	2.95193	1.68986	5.09384	0.87115	48	32	1.06049	1.72024	10.15639	0.81935
	27	3.11618	1.66361	5.69551	.69078		33	1.49758	1.76836	12.88553	.83605
	28	3.30874	1.69980	6.44299	.71018		34	5.10813	1.82230	16.04289	.88657
	29	3.53915	1.73988	7.39491	.78936		35	6.09125	1.88312	23.42636	.87492
	30	3.82213	1.78442	8.63246	.74833		36	7.81289	1.92221	39.16270	.89314
	31	4.18188	1.83113	10.39077	.76711		37	13.43974	2.03135	116.20903	.91181
	32	4.66173	1.88987	12.92829	.78572		0	1.32501	1.32501	1.00000	0
	33	5.34930	1.92874	17.10600	.80417		1	1.35337	1.31763	1.09548	.03937
	34	6.45951	2.08416	25.02851	.82247		2	1.38285	1.31130	1.10711	.07728
	35	8.74799	2.10599	46.03221	.84064		3	1.41230	1.30598	1.19878	.11372
	36	1.36733	1.36733	1.00000	0		4	1.44301	1.30154	1.21704	.14891
	37	1.39651	1.36141	1.02016	.03679		5	1.47465	1.29827	1.27839	.18268
	38	1.42630	1.35651	1.10280	.07219		6	1.50731	1.29535	1.34310	.21573
	39	1.47706	1.39265	1.25815	.10642		7	1.54108	1.29435	1.41151	.24753
	40	1.48878	1.34984	1.21646	.13931		8	1.57607	1.30378	1.48399	.27615
	41	1.52154	1.34797	1.27800	.17155		9	1.61239	1.32413	1.56096	.30824
	42	1.55544	1.34708	1.34320	.20259		10	1.65019	1.29540	1.64290	.33727
	43	1.59060	1.34716	1.41221	.23270		11	1.68960	1.29760	1.70387	.36449
	44	1.62712	1.34821	1.48545	.26195		12	1.73080	1.30074	1.82401	.39555
	45	1.66516	1.35021	1.56359	.29037		13	1.77397	1.30483	1.92452	.41970
	46	1.70483	1.35326	1.64707	.31804		14	1.81933	1.30991	2.03286	.44978
	47	1.74637	1.35727	1.73650	.34498		15	1.86712	1.31599	2.16994	.47123
	48	1.78993	1.36332	1.82361	.37125		16	1.91764	1.33911	2.27669	.49609
	49	1.83773	1.36841	1.93264	.39629		17	1.97121	1.33138	2.31543	.50038
	50	1.88405	1.37560	2.04839	.42293		18	2.02882	1.34065	2.56696	.54416
	51	1.93516	1.38391	2.17022	.44651		19	2.08914	1.35217	2.73362	.56711
	52	1.98543	1.39339	2.30333	.47036		20	2.15449	1.36833	2.92792	.59086
	53	2.04782	1.40411	2.44879	.49381		21	2.22493	1.37602	3.12296	.61264
	54	2.10912	1.41614	2.60525	.51820		22	2.30130	1.39053	3.32660	.63461
	55	2.17560	1.42854	2.76989	.53934		23	2.38451	1.40654	3.61170	.65619
	56	2.24736	1.44440	2.98505	.56147		24	2.47979	1.42419	3.90650	.67740
	57	2.32526	1.46084	3.20733	.58321		25	2.57667	1.44460	4.16521	.69388
	58	2.41032	1.47958	3.42870	.60498		26	2.65909	1.46804	4.43661	.71883
	59	2.50383	1.49893	3.74543	.63653		27	2.81368	1.48810	5.10116	.73068
	60	2.60741	1.52092	4.07583	.66438		28	2.95987	1.51427	5.51488	.75004
	61	2.72317	1.54507	4.46089	.66671		29	3.12998	1.54294	6.32660	.77073
	62	2.85386	1.57165	4.93178	.68633		30	3.38102	1.57379	7.16241	.79220
	63	3.00390	1.60090	5.46154	.70657		31	3.55475	1.60830	8.39036	.81742
	64	3.17532	1.63314	6.12923	.72627		32	3.81229	1.64650	9.64375	.83842
	65	3.38059	1.66877	6.96194	.74563		33	4.20888	1.68894	11.60395	.86062
	66	3.62100	1.70822	8.04246	.76977		34	4.69093	1.75688	14.50661	.87363
	67	3.93885	1.73905	9.48932	.78731		35	5.40531	1.78933	19.25024	.89287
	68	4.32733	1.80096	11.51871	.80216		36	6.55778	1.84915	28.40793	.91055
	69	4.86463	1.85579	14.60078	.82104		37	8.98961	33.52292	92869	
	70	5.66667	1.91764	19.28908	.83945		38				
	71	7.02769	1.98788	30.62894	.87772		39				
	72	10.33190	2.06836	66.44872	.87585		40				
48	0	1.34562	1.34562	1.00000	0	50	0	1.30541	1.30541	1.00000	0
	1	1.37431	1.33897	1.05028	.03803		1	1.33148	1.29731	1.05072	.04073
	2	1.40376	1.33334	1.10289	.07466		2	1.36228	1.30208	1.10380	.07991
	3	1.43104	1.32876	1.15835	.11000		3	1.39174	1.28482	1.15940	.11726
	4	1.46922	1.32935	1.21660	.14413		4	1.42204	1.27920	1.21777	.15384
	5	1.49738	1.32253	1.27799	.17712		5	1.45322	1.27510	1.27916	.18884
	6	1.53062	1.32083	1.32495	.20905		6	1.48536	1.27194	1.34383	.22263
	7	1.56467	1.32016	1.40795	.23953		7	1.51856	1.26978	1.41210	.25929
	8	1.60075	1.32034	1.48434	.27003		8	1.55892	1.26837	1.48436	.26693
	9	1.63789	1.32151	1.56125	.29919		9	1.58894	1.26795	1.56093	.31756
	10	1.67658	1.32364	1.64444	.32758		10	1.62534	1.26813	1.64237	.34789
	11	1.71700	1.32674	1.73283	.35211		11	1.66048	1.26977	1.72917	.37617
	12	1.75929	1.33077	1.82798	.36126		12	1.70486	1.27204	1.82185	.40422
	13	1.80370	1.33585	1.92931	.40817		13	1.74631	1.27582	1.92183	.43204
	14	1.85044	1.34290	2.03999	.43372		14	1.79047	1.27937	2.02809	.45811
	15	1.89980	1.34908	2.13889	.45868		15	1.83697	1.28845	2.14331	.48407
	16	1.95212	1.35736	2.28684	.48308		16	1.88692	1.29092	2.26268	.50939
	17	2.00769	1.36677	2.41042	.50696		17	1.93761	1.29760	2.40364	.53112
	18	2.06698	1.37739	2.58609	.53036		18	1.99260	1.30574	2.55161	.55897
	19	2.13050	1.38989	2.72788	.55326		19	2.05180	1.31499	2.71386	.58192
	20	2.19886	1.40253	2.94856	.57373		20	2.11391	1.32010	2.89268	.60307
	21	2.27580	1.41792	3.16158	.59779		21	2.18131	1.33703	3.03286	.62776
	22	2.35281	1.43345	3.40126	.61947		22	2.25409	1.34597	3.11189	.64002
	23	2.41121	1.45134	3.67309	.64078		23	2.33313	1.36428	3.26009	.67186
	24	2.53819	1.47103	3.94124	.66174		24	2.41947	1.38009	3.84102	.69333
	25	2.61294	1.49269	4.34433	.68238		25	2.51443	1.39749	4.16179	.71442
	26	2.76572	1.51683	4.76146	.70272		26	2.61969	1.41662	4.93171	.73318
	27	2.90369	1.54266	5.28977	.72877		27	2.73711	1.43765	5.06322	.75562
	28	3.06091	1.57217	5.85997	.74553		28	2.87044	1.46075	5.47466	.77716
	29	3.24122	1.60322	6.61167	.78209		29	3.02942	1.48613	6.08242	.79562
	30	3.46207	1.63828	7.55598	.78135		30	3.19929	1.51406	6.84082	.81301
	31	3.72728	1.67711	8.78447	.80047		31	3.40813	1.53182	7.79552	.83453
	32						32	3.66041	1.57078	9.00756	.85366
	33						33	3.97506	1.61636	10.69180	.87286
	34						34	4.30240	1.65811	12.98191	.89106

NACA TN No. 1143
(Supplement)

9

TABLE I.—VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES—Continued

θ (deg)	β (deg)	M_0	M_∞	$\frac{P_\infty}{P_0}$	$\frac{\Delta P_{a,b}}{P_0}$	θ (deg)	β (deg)	M_0	M_∞	$\frac{P_\infty}{P_0}$	$\frac{\Delta P_{a,b}}{P_0}$
50	35	4.94092	1.70467	16.51698	0.90977	52	35	4.31111	1.55729	13.29968	0.91527
	36	5.77744	1.75834	22.65537	.95611		36	4.83682	1.59767	16.78182	.96359
	37	7.24492	1.81267	35.76268	.96289		37	5.60756	1.61269	22.61361	.96163
	38	11.02198	1.88247	83.00475	.95432		38	6.90708	1.69313	34.39544	1.00000
51	0	1.28676	1.28676	1.00000	0	53	0	1.25814	1.25814	1.00000	0
	1	1.31451	1.27794	1.04220			1	1.28769	1.24189	1.05190	.04328
	2	1.34310	1.27020	1.10441	.08268		2	1.30781	1.23275	1.10605	.08838
	3	1.37229	1.26347	1.15026	.12157		3	1.33656	1.20865	1.15005	.13005
	4	1.40225	1.25773	1.21282	.15998		4	1.36600	1.21756	1.22183	.16983
	5	1.43304	1.25094	1.26033	.19901		5	1.39619	1.21142	1.28389	.20605
	6	1.46474	1.24208	1.34507	.25776		6	1.42721	1.20621	1.34907	.24481
	7	1.49745	1.24813	1.41333	.26333		7	1.45914	1.20190	1.41763	.28022
	8	1.53125	1.24408	1.44645	.29771		8	1.49205	1.19646	1.48591	.31438
	9	1.56624	1.24890	1.56163	.32718		9	1.52604	1.19589	1.56668	.34736
52	10	1.60255	1.24260	1.64290	.39762	54	10	1.56122	1.19415	1.64707	.37923
	11	1.64030	1.24317	1.75916	.39715		11	1.59770	1.19323	1.73881	.41011
	12	1.67956	1.24463	1.82118	.41982		12	1.63360	1.19319	1.82401	.44003
	13	1.72072	1.24596	1.91962	.44700		13	1.67508	1.19395	1.92126	.46904
	14	1.76374	1.25020	2.02659	.47082		14	1.71629	1.19553	2.02629	.49722
	15	1.80891	1.25434	2.12389	.49725		15	1.75941	1.19800	2.13677	.52652
	16	1.85646	1.25943	2.25176	.52301		16	1.80163	1.20130	2.25676	.55127
	17	1.90668	1.26247	2.39402	.54814		17	1.85225	1.20047	2.36629	.57724
	18	1.95988	1.27291	2.53987	.57270		18	1.90248	1.21053	2.52664	.60853
	19	2.01645	1.28059	2.69835	.59670		19	1.95566	1.21652	2.67932	.62726
53	20	2.07682	1.28975	2.87247	.62018	55	20	2.01216	1.28246	2.64613	.63139
	21	2.14152	1.30005	3.06478	.64318		21	2.07241	1.29110	3.08266	.67197
	22	2.21119	1.31155	3.27844	.66972		22	2.13693	1.24037	3.23135	.69805
	23	2.28957	1.32438	3.52474	.68782		23	2.20833	1.25044	3.49962	.72065
	24	2.36661	1.33845	3.76644	.70972		24	2.28136	1.26166	3.70619	.74880
	25	2.45843	1.35403	4.09202	.73084		25	2.36292	1.27410	3.98804	.76453
	26	2.55756	1.37119	4.44229	.75179		26	2.45212	1.28784	4.30767	.78895
	27	2.66777	1.39002	4.84829	.77281		27	2.55039	1.30899	4.67318	.80880
	28	2.79151	1.41076	5.32406	.79271		28	2.65511	1.33195	5.09652	.82739
	29	2.93197	1.43350	5.89051	.81271		29	2.78180	1.33793	5.59197	.84766
54	30	3.09355	1.45896	6.77683	.83844	56	30	2.92034	1.35803	6.17951	.86761
	31	3.26833	1.48598	7.42663	.85930		31	3.07931	1.38008	6.89921	.88726
	32	3.50735	1.51682	8.50117	.87111		32	3.26455	1.40249	7.76366	.90664
	33	3.78233	1.54666	9.19359	.89009		33	3.48454	1.43090	8.85947	.92777
	34	4.12960	1.58664	11.84954	.90886		34	3.75215	1.46019	10.30955	.94465
	35	4.58848	1.62770	14.66843	.92743		35	4.08807	1.49229	12.86335	.96339
	36	5.23674	1.67349	19.12633	.94982		36	4.52865	1.52228	15.02156	.98175
	37	6.23775	1.72479	27.42587	.96403		37	5.16517	1.56798	19.50936	1.00000
	38	8.24709	1.78263	47.75734	.98209		38	6.08851	1.61224	27.41609	1.01807
	39	1.26602	1.26602	1.00000	0		39	7.84757	1.66183	45.69954	1.03997
55	0	1.29370	1.29548	1.09344	.04370	57	13.37365	1.711693	132.92279	1.05371	
	1	1.32498	1.25103	1.10216	.08577		1	1.23606	1.23606	1.00000	0
	2	1.35392	1.24364	1.11613	.12771		2	1.26553	1.22509	1.05243	.04691
	3	1.38359	1.23720	1.12047	.15430		3	1.29152	1.21920	1.10710	.09172
	4	1.41404	1.23173	1.28189	.20140		4	1.32016	1.20650	1.15416	.13456
	5	1.44538	1.22720	1.34680	.23715		5	1.34943	1.19873	1.22383	.17560
	6	1.47766	1.23334	1.41517	.27163		6	1.37942	1.19194	1.28631	.21495
	7	1.51057	1.22209	1.48726	.30491		7	1.41018	1.18607	1.35186	.25271
	8	1.54543	1.21891	1.56357	.33709		8	1.44181	1.18109	1.42075	.28514
	9	1.58114	1.21788	1.64446	.36826		9	1.47440	1.17701	1.49329	.32417
56	10	1.61820	1.21749	1.73036	.39843	58	10	1.50801	1.17379	1.56982	.37796
	11	1.65677	1.21831	1.82188	.42773		11	1.54274	1.17135	1.65074	.39059
	12	1.69700	1.21969	1.91963	.45820		12	1.57871	1.16978	1.73668	.42214
	13	1.73795	1.22229	2.02489	.48384		13	1.61603	1.16899	1.82758	.45269
	14	1.78114	1.22597	2.13679	.51073		14	1.65887	1.16904	1.92475	.48289
	15	1.82945	1.22927	2.22601	.53965		15	1.69536	1.17087	2.02809	.51099
	16	1.87838	1.23480	2.38915	.56291		16	1.73765	1.17155	2.13897	.53888
	17	1.92290	1.24082	2.53157	.58745		17	1.78193	1.17404	2.24901	.56997
	18	1.96847	1.24781	2.66880	.61180		18	1.82618	1.17737	2.38829	.59234
	19	2.04298	1.25782	2.87703	.63861		19	1.87750	1.18134	2.52900	.61903
57	20	2.10531	1.26469	3.04455	.66591	59	20	1.96421	1.19254	2.83966	.66792
	21	2.17223	1.27507	3.29773	.69212		21	2.04264	1.19943	3.03932	.69139
	22	2.24442	1.28643	3.46272	.70408		22	2.10505	1.20749	3.21701	.71473
	23	2.32271	1.28904	3.74716	.72601		23	2.17202	1.21616	3.33770	.73756
	24	2.40812	1.31298	4.03448	.74753		24	2.24240	1.22610	3.67910	.75992
	25	2.49192	1.32833	4.36812	.76668		25	2.32241	1.23718	3.95183	.78184
	26	2.56971	1.34326	4.75217	.78947		26	2.40765	1.24945	4.55971	.80333
	27	2.71256	1.36383	5.19927	.80992		27	2.50117	1.26300	4.81443	.82443
	28	2.85217	1.38463	5.72669	.83006		28	2.60453	1.27793	5.01322	.84516
	29	3.00119	1.40663	6.35861	.84990		29	2.71975	1.29431	5.48166	.86953
58	30	3.17365	1.43123	7.13007	.86946	60	30	2.84947	1.31236	6.03330	.88958
	31	3.37870	1.45827	8.09364	.88765		31	2.90117	1.33261	7.02017	.91139
	32	3.62101	1.48806	9.33212	.90762		32	3.01523	1.35300	8.45332	.93443
	33	3.92327	1.52092	10.92415	.92665		33	3.12795	1.38166	9.69553	.95553

NACA

TABLE I.—VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES—Continued

θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\alpha_{a,b}}{\alpha_b}$	θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\alpha_{a,b}}{\alpha_b}$
54	31	2.99781	1.33913	6.62290	0.90532	56	23	2.85415	1.16282	1.90771	0.61750
	32	3.16784	1.35282	7.45613	.92477		26	2.33030	1.17622	1.97772	.63936
	33	3.36824	1.37764	8.49634	.94394		27	2.1281	1.18299	4.22908	.86066
	34	3.60863	1.40381	9.77698	.96286		28	2.13111	1.20092	4.89763	.88161
	35	3.90484	1.43262	11.47643	.98154		29	2.61718	1.21408	5.33772	.90218
	36	4.28290	1.46441	13.84205	1.00000		30	2.73212	1.22956	5.38613	.92239
	37	4.79140	1.49937	17.36337	1.01825		31	2.86157	1.24447	6.40851	.94227
	38	5.26791	1.53899	23.16703	1.03631		32	3.01204	1.26192	7.10806	.96180
	39	6.74612	1.58609	34.54341	1.05418		33	3.18337	1.28106	7.99920	.98104
	40	9.37684	1.63082	66.97239	1.07189		34	3.38442	1.30603	9.03802	1.00000
	41						35	3.62531	1.32508	10.37199	1.01869
	42						36	3.92173	1.35038	18.16581	1.03714
55	0	1.22077	1.22077	1.00000	0	57	37	4.29964	1.37622	14.67711	1.05533
	1	1.24622	1.20908	1.05305	.04864		38	4.80794	1.40693	18.35382	1.07333
	2	1.27618	1.19835	1.10831	.09501		39	5.33673	1.44289	24.41461	1.09114
	3	1.30471	1.18909	1.15995	.13927		40	6.73301	1.48097	36.18410	1.10874
	4	1.33336	1.18067	1.22617	.18160		41	9.26383	1.52256	68.94509	1.12617
	5	1.36370	1.17322	1.28917	.22014		42				
	6	1.39449	1.16672	1.35281	.26103		43				
	7	1.42970	1.16111	1.42155	.29859		44				
	8	1.45800	1.15638	1.49743	.33432		45				
	9	1.49130	1.15249	1.57436	.36894		46				
	10	1.52967	1.14643	1.65554	.40233		47				
56	11	1.56213	1.14719	1.74146	.43157	57	0	1.19236	1.19236	1.00000	0
	12	1.59808	1.14974	1.83261	.46974		1	1.21991	1.17918	1.05453	.09235
	13	1.63936	1.14509	1.98933	.49992		2	1.24792	1.18728	1.11126	.10806
	14	1.67620	1.14528	2.03266	.52516		3	1.33524	1.17922	1.13015	.14935
	15	1.71778	1.14615	2.14332	.55352		4	1.30553	1.18330	1.14541	.11908
	16	1.76127	1.14787	2.26176	.58107		5	1.35524	1.17330	1.15869	.13982
	17	1.80687	1.15039	2.38915	.60785		6	1.36563	1.17330	1.16451	.14142
	18	1.84983	1.15373	2.52664	.63391		7	1.39578	1.18330	1.17033	.14703
	19	1.90542	1.15792	2.67556	.65929		8	1.42875	1.17733	1.18221	.15084
	20	1.95896	1.16294	2.83751	.68404		9	1.46263	1.18434	1.19054	.15210
	21	2.01550	1.16805	3.01438	.70319		10	1.49550	1.10791	1.66662	.42708
	22	2.07639	1.17567	3.20958	.73178		11	1.53646	1.10441	1.75543	.46073
58	23	2.11813	1.18345	3.42257	.75463	58	12	1.56661	1.10169	1.84730	.49319
	24	2.21091	1.19222	3.66007	.77740		13	1.60407	1.09973	1.94475	.52454
	25	2.28663	1.20204	3.92521	.79949		14	1.64589	1.09954	2.04839	.55084
	26	2.36806	1.21297	4.22330	.82114		15	1.68344	1.09810	2.15888	.58418
	27	2.45778	1.22498	4.56111	.84235		16	1.72766	1.09841	2.27699	.61260
	28	2.55521	1.23843	4.94742	.86322		17	1.76982	1.09947	2.40394	.64018
	29	2.66511	1.25313	5.33734	.88370		18	1.81611	1.10126	2.53987	.66696
	30	2.78737	1.26293	5.91660	.90383		19	1.86478	1.10387	2.66988	.69300
	31	2.92972	1.28703	6.52435	.92364		20	1.91611	1.10723	2.84633	.71833
	32	3.06485	1.30648	7.28025	.94314		21	1.97041	1.11138	3.01923	.74301
	33	3.26878	1.32762	8.19757	.96236		22	2.02806	1.11636	3.20858	.76707
	34	3.48734	1.35125	9.33593	.98131		23	2.08950	1.12218	3.41603	.79094
56	35	3.75267	1.37698	10.89776	1.00000	58	24	2.15523	1.12887	3.64502	.81347
	36	4.08849	1.40531	12.88486	1.01846		25	2.22588	1.11647	3.89003	.83589
	37	4.51787	1.43666	15.81213	1.03670		26	2.30597	1.18993	5.75347	.94126
	38	5.11821	1.47111	20.31079	1.05473		27	2.36977	1.20449	6.31277	.96177
	39	6.03358	1.50947	28.33208	1.07237		28	2.49684	1.21984	6.97378	.98074
	40	7.69875	1.55221	46.23275	1.09023		29	3.11033	1.23700	7.77189	1.00000
	41	12.56283	1.60009	122.67166	1.10773		30	3.29703	1.25982	8.75397	1.01896
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TABLE I.—VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES—Continued

θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\gamma_{a,b}}{c_b}$	θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\gamma_{a,b}}{c_b}$
58	17	1.73425	1.07535	2.41543	0.93706	60	10	1.45961	1.05096	1.69801	0.48792
	18	1.79992	1.07647	2.55161	0.93419		11	1.49446	1.04530	1.78756	.50375
	19	1.85786	1.07832	2.69837	0.93054		12	1.53013	1.04043	1.88204	.53817
	20	1.89834	1.08093	2.85702	0.92616		13	1.56705	1.03711	1.98204	.57130
	21	1.93166	1.08289	3.08926	0.91608		14	1.60524	1.03411	2.05304	.60321
	22	2.00817	1.08643	3.21701	0.90535		15	1.64485	1.03183	2.20066	.63397
	23	2.06927	1.09137	3.42257	0.89903		16	1.68601	1.03028	2.38064	.66369
	24	2.13445	1.09914	3.64877	0.88213		17	1.72890	1.02941	2.44879	.69243
	25	2.20127	1.10576	3.89903	0.86489		18	1.77370	1.02824	2.58569	.72023
	26	2.27343	1.11327	4.11758	0.84764		19	1.82061	1.02776	2.73362	.74715
	27	2.35976	1.12172	4.40573	0.82932		20	1.86986	1.03098	2.89268	.77332
	28	2.44329	1.13125	4.82426	0.81145		21	1.92174	1.03580	3.06478	.79671
	29	2.53928	1.14162	5.24346	0.90215		22	1.97622	1.03553	3.25173	.82339
	30	2.64334	1.15119	5.70487	0.96047		23	2.03485	1.03889	3.45368	.84740
	31	2.76333	1.16997	6.24133	0.98041		24	2.09647	1.04299	3.67910	.87080
	32	2.89660	1.17998	6.87320	1.00000		25	2.16251	1.04789	3.92521	.89360
	33	3.04811	1.19537	7.66890	1.03265		26	2.23336	1.05350	4.19773	.91556
	34	3.22305	1.21225	8.59494	1.03820		27	2.30976	1.05996	4.50144	.93760
	35	3.42852	1.23075	9.69613	1.05686		28	2.48266	1.07350	5.22736	.97964
	36	3.67496	1.25103	11.16500	1.07923	61	29	2.58199	1.08463	5.66667	1.00000
	37	3.97568	1.27328	13.11538	1.09336		30	2.69180	1.09480	6.17265	1.03995
	38	4.36671	1.29772	15.83248	1.11124		31	2.81401	1.10602	6.76214	1.07953
	39	4.88820	1.32458	19.88200	1.12889		32	2.95196	1.11836	7.45813	1.09874
	40	5.61473	1.35421	26.58793	1.14534		33	3.10935	1.13192	8.29290	1.07761
	41	6.89470	1.38596	39.71614	1.16358		34	3.29153	1.14880	9.31323	1.09617
	42	9.62343	1.42330	77.73610	1.18063		35	3.50613	1.16310	10.59695	1.11142
	43	0	1.16663	1.16663	1.00000		36	3.76152	1.18095	12.23349	1.13239
	1	1.19150	1.15189	1.05639	0.95646		37	4.08459	1.20095	14.43171	1.16010
	2	1.22277	1.13845	1.11497	1.05825		38	4.40641	1.22397	17.52384	1.18756
	3	1.25150	1.12883	1.17591	1.06045		39	4.72576	1.24397	21.19785	1.21479
	4	1.28073	1.11915	1.23939	1.06349		40	5.05564	1.25452	22.19785	1.24218
	5	1.31096	1.10513	1.30766	1.07420		41	5.38053	1.27142	30.09240	1.28180
	6	1.34101	1.09611	1.37482	1.07776		42	5.78932	1.29997	46.29321	1.31861
	7	1.37215	1.08804	1.44742	1.08225		43	6.12250	1.33152	98.56617	1.35232
	8	1.40405	1.08087	1.52317	1.09124		0	1.14335	1.14335	1.00000	0
	9	1.43680	1.07457	1.60890	1.07722		1	1.17276	1.12694	1.07868	.06106
	10	1.47046	1.06909	1.68679	1.05376		2	1.20052	1.11195	1.11958	.11853
	11	1.50513	1.06410	1.77223	1.08866		3	1.22970	1.09268	1.18287	.17276
	12	1.54091	1.06090	1.85860	1.08263		4	1.25935	1.08582	1.24872	.22404
	13	1.57790	1.05735	1.96754	1.09515		5	1.28951	1.07449	1.31735	.27264
	14	1.61623	1.05493	2.07248	1.08692		6	1.32026	1.06422	1.38978	.31278
	15	1.65302	1.05384	2.18409	1.07682		7	1.35165	1.05944	1.45221	.36220
	16	1.69743	1.05228	2.30313	1.06611		8	1.41680	1.03914	1.68440	.44447
	17	1.74062	1.05220	2.36042	1.07446		9	1.48716	1.02912	1.80166	.51923
	18	1.78579	1.05248	2.56566	1.07047		10	1.49404	1.03253	1.91076	.58267
	19	1.83135	1.05365	2.71386	1.07259		11	1.49310	1.02912	1.98156	.65435
	20	1.88234	1.05354	2.87247	1.07547		12	1.50064	1.02170	2.09682	.72007
	21	1.93345	1.05316	3.04435	1.07964		13	1.57772	1.01742	2.16037	.78050
	22	1.99101	1.06132	3.23335	1.08412		14	1.59935	1.01388	2.21727	.84174
	23	2.05001	1.06964	3.43701	1.08797		15	1.63536	1.01104	2.22011	.88187
	24	2.11268	1.07055	3.66007	1.09122		16	1.67639	1.00880	2.34137	.92197
	25	2.18018	1.07625	3.90771	1.09392		17	1.71909	1.00745	2.47071	.97107
	26	2.25222	1.08620	4.18260	1.09608		18	1.76564	1.00668	2.60923	.73910
	27	2.33070	1.09022	4.48973	1.09774		19	1.81024	1.00659	2.75788	.76633
	28	2.41554	1.09655	4.63953	1.09874		20	1.85921	1.00727	2.91792	.79272
	29	2.50852	1.10117	5.22736	1.09570		21	1.91052	1.00843	3.09086	.81832
	30	2.61079	1.11816	5.67616	1.09005		22	1.96476	1.01038	3.27818	.84138
	31	2.72432	1.12274	6.19533	1.09000		23	2.02271	1.01302	3.48278	.86735
	32	2.85152	1.12420	6.80332	1.09159		24	2.08316	1.01836	3.70629	.89087
	33	2.95759	1.12590	7.38511	1.09283	62	25	2.11241	1.02043	3.95283	.91378
	34	3.16089	1.12637	8.39771	1.09775		26	2.17788	1.02595	4.22330	.93611
	35	3.35349	1.12762	9.74735	1.07636		27	2.29875	1.03083	4.22058	.95790
	36	3.58927	1.20520	10.83337	1.09498		28	2.37393	1.03722	4.86278	.97919
	37	3.86064	1.21574	12.60945	1.11274		29	2.46213	1.04444	5.24346	1.00000
	38	4.21032	1.24753	15.26297	1.13054		30	2.55870	1.02253	5.67616	1.04036
	39	4.66898	1.27177	16.51961	1.14610		31	2.66519	1.01614	6.17625	1.04430
	40	5.30993	1.29795	24.00218	1.16945		32	2.73639	1.01723	6.74953	1.05984
	41	6.30127	1.32704	33.86500	1.18258		33	2.82659	1.01625	7.32958	1.07900
	42	8.19969	1.39920	56.90567	1.19993		34	3.06758	1.01946	8.23136	1.09782
	0	1.15470	1.15470	1.00000	0		35	3.24135	1.10802	9.20976	1.11630
	1	1.18281	1.13913	1.05748	.05869		36	3.44462	1.12263	10.42822	1.13447
	2	1.21126	1.12492	1.17713	.11407		37	3.68722	1.13583	11.96675	1.15294
	3	1.24021	1.11200	1.17919	.16643		38	3.98431	1.13647	11.00050	1.16954
	4	1.26963	1.10024	1.24379	.23606		39	4.36069	1.13757	11.80349	1.18729
	5	1.29959	1.08956	1.31115	.26318		40	4.86049	1.15643	20.91698	1.20438
	6	1.33016	1.07951	1.38049	.30802		41	5.57221	1.12953	27.34355	1.22215
	7	1.36139	1.07123	1.47505	.35073		42	6.70976	1.14194	40.01234	1.23751
	8	1.39336	1.06349	1.53211	.39149		43	9.00334	1.12784	72.17563	1.25437
	9	1.42614	1.05661	1.61296	.43053		0	1.13257	1.11267	1.00000	0
	1	1.16134	1.16134	1.19044	1.09945		1	1.16134	1.16001	1.12226	.06356

NACA

TABLE I.—VALUES OF LOCAL MASS NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES—Continued

θ (deg)	β (deg)	K_1	K_2	$\frac{P_1}{P_2}$	$\frac{\rho_1}{\rho_2}$	$\frac{T_1}{T_2}$	$\frac{P_{local}}{P_2}$	$\frac{\theta}{(deg)}$ (deg)	β (deg)	K_1	K_2	$\frac{P_1}{P_2}$	$\frac{\rho_1}{\rho_2}$	$\frac{T_1}{T_2}$	$\frac{P_{local}}{P_2}$
62	3	1.8591	1.0893	1.1953	0.17943	63	5.40533	1.10215	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	4	1.8298	1.0737	1.0548	0.17946		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	5	1.8093	1.0587	1.0362	0.17948		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	6	1.7893	1.0437	1.0172	0.17950		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	7	1.7693	1.0287	1.0015	0.17952		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	8	1.7491	1.0137	1.0002	0.17953		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	9	1.7291	1.0037	1.0022	0.17954		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	10	1.7089	1.0017	1.0002	0.17955		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	11	1.6887	1.0017	1.0002	0.17956		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	12	1.6686	1.0013	1.0002	0.17957		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	13	1.6485	1.0013	1.0002	0.17958		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	14	1.6284	1.0013	1.0002	0.17959		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	15	1.6083	1.0013	1.0002	0.17960		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	16	1.5882	1.0013	1.0002	0.17961		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	17	1.5681	1.0013	1.0002	0.17962		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	18	1.5480	1.0013	1.0002	0.17963		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	19	1.5279	1.0013	1.0002	0.17964		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	20	1.5078	1.0013	1.0002	0.17965		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	21	1.4877	1.0013	1.0002	0.17966		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	22	1.4676	1.0013	1.0002	0.17967		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	23	1.4475	1.0013	1.0002	0.17968		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	24	1.4274	1.0013	1.0002	0.17969		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	25	1.4073	1.0013	1.0002	0.17970		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	26	1.3872	1.0013	1.0002	0.17971		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	27	1.3671	1.0013	1.0002	0.17972		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	28	1.3470	1.0013	1.0002	0.17973		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	29	1.3269	1.0013	1.0002	0.17974		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	30	1.3068	1.0013	1.0002	0.17975		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	31	1.2867	1.0013	1.0002	0.17976		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	32	1.2666	1.0013	1.0002	0.17977		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	33	1.2465	1.0013	1.0002	0.17978		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	34	1.2264	1.0013	1.0002	0.17979		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	35	1.2063	1.0013	1.0002	0.17980		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	36	1.1862	1.0013	1.0002	0.17981		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	37	1.1661	1.0013	1.0002	0.17982		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	38	1.1460	1.0013	1.0002	0.17983		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	39	1.1259	1.0013	1.0002	0.17984		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	40	1.1058	1.0013	1.0002	0.17985		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	41	1.0857	1.0013	1.0002	0.17986		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	42	1.0656	1.0013	1.0002	0.17987		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	43	1.0455	1.0013	1.0002	0.17988		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	44	1.0254	1.0013	1.0002	0.17989		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	45	1.0053	1.0013	1.0002	0.17990		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	46	9852	1.0013	1.0002	0.17991		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	47	9651	1.0013	1.0002	0.17992		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	48	9450	1.0013	1.0002	0.17993		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	49	9249	1.0013	1.0002	0.17994		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	50	9048	1.0013	1.0002	0.17995		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	51	8847	1.0013	1.0002	0.17996		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	52	8646	1.0013	1.0002	0.17997		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	53	8445	1.0013	1.0002	0.17998		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	54	8244	1.0013	1.0002	0.17999		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	55	8043	1.0013	1.0002	0.18000		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	56	7842	1.0013	1.0002	0.18001		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	57	7641	1.0013	1.0002	0.18002		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	58	7440	1.0013	1.0002	0.18003		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	59	7239	1.0013	1.0002	0.18004		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	60	7038	1.0013	1.0002	0.18005		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	61	6837	1.0013	1.0002	0.18006		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	62	6636	1.0013	1.0002	0.18007		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233	1.05233	1.05233
	63	6435	1.0013	1.0002	0.18008		5.40533	1.10213	1.6938	1.05233	1.10213	1.05233	1.05233		

TABLE I.—VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES—Continued

θ (deg)	β (deg)	M_b	M_a	P_a P_b	$\frac{dp_{a,b}}{dp_b}$	θ (deg)	β (deg)	M_b	M_a	P_a P_b	$\frac{dp_{a,b}}{dp_b}$	
65	31	2.61942	0.91052	6.40854	1.18608	67	23	2.01077	0.87166	3.83024	1.00000	
	32	2.72969	0.91653	6.97378	1.15321		24	2.07163	4.07583	1.02386		
	33	2.85227	0.93332	7.62850	1.15411		25	2.13613	4.34113	1.04696		
	34	2.98950	0.96050	8.39771	1.18230		26	2.20475	4.63661	1.08339		
	35	3.14583	0.96931	9.31323	1.20051		27	2.27607	4.96352	1.09106		
	36	3.30438	0.97882	10.42262	1.21816		28	2.35767	5.32406	1.11215		
	37	3.35313	0.98897	11.79568	1.23547		29	2.44164	5.72588	1.13265		
	38	3.76200	1.00013	13.34033	1.25247		30	2.53371	6.17951	1.15260		
	39	4.08602	1.01243	15.63259	1.26916		31	2.63420	6.69290	1.17203		
	40	4.46996	1.02600	18.98054	1.28558		32	2.74466	7.28024	1.19097		
	41	4.97763	1.04081	23.57679	1.30172		33	2.86705	7.95920	1.20946		
	42	5.59507	1.05701	30.92569	1.31762		34	3.00392	8.73357	1.22751		
	43	6.83227	1.07474	41.36510	1.33329		35	3.15864	9.69613	1.24536		
	44	9.07019	1.09416	78.87052	1.34873		36	3.33758	10.83337	1.26241		
	0	1.09463	1.09463	1.00000	0	68	37	3.66703	12.18645	1.28927		
	1	1.18598	1.07331	1.05651	.07545		38	3.78970	13.00080	1.29592		
	2	1.19578	1.05388	1.13626	.18457		39	3.98173	16.30312	1.31218		
	3	1.18829	1.05613	1.20618	.21062		40	4.15226	19.42902	1.38514		
	4	1.21761	1.01850	1.27689	.26630		41	4.33515	23.91996	1.34381		
	5	1.29245	1.00511	1.36067	.32847		42	4.60221	30.92528	1.35922		
	6	1.26523	.99197	1.44166	.36197		43	4.86773	43.56829	1.37439		
	7	1.31856	.97920	1.32615	.43233		44	5.53138	71.78450	1.38532		
	8	1.35220	.98785	1.61445	.47966		0	1.07854	1.00000	0		
	9	1.38713	.97574	1.70686	.52374		1	1.11113	1.05481	1.07157	.06281	
	10	1.42226	.94829	1.80374	.56738		2	1.14392	1.03325	1.14574	.15911	
	11	1.45577	.95000	1.89581	.60453		3	1.17698	1.01361	1.22268	.22564	
	12	1.49564	.93219	2.01255	.64630		4	1.21035	.99570	1.30359	.59508	
	13	1.53428	.95535	2.18531	.68236		5	1.24412	.97935	1.38971	.35999	
	14	1.57358	.92461	2.71796	.72238		6	1.27831	.96440	1.47229	.11267	
	15	1.61434	.91388	2.37080	.75182		7	1.31308	.95070	1.56259	.16513	
	16	1.66441	.90917	2.50474	.78349		8	1.34843	.93821	1.65466	.17616	
	17	1.70000	.90531	2.64751	.81461		9	1.38466	.92678	1.75368	.18322	
	18	1.74529	.90173	2.79914	.84378		10	1.42122	.91633	1.85916	.19765	
	19	1.79247	.89898	2.96104	.87221		11	1.45889	.90689	1.96784	.19966	
	20	1.84172	.89683	3.13593	.89998		12	1.49711	.89823	2.08216	.19946	
	21	1.89329	.88538	3.38248	.92699		13	1.53689	.89042	2.08662	.19721	
	22	1.94745	.88432	3.52698	.95148		14	1.57172	.88338	2.32987	.176322	
	23	2.00448	.88396	3.74545	.97614		15	1.61972	.87707	2.46575	.19743	
	24	2.06475	.88418	3.98424	1.00000		16	1.66311	.87146	2.60744	.19302	
	25	2.12867	.88499	4.24521	1.02312		17	1.70805	.86632	2.79338	.186151	
	26	2.19671	.88640	4.53177	1.04556		18	1.75470	.86222	2.92139	.189148	
	27	2.26913	.88840	4.84808	1.06734		19	1.80324	.85834	3.09460	.192023	
	28	2.34757	.90102	5.19927	1.08932		20	1.85387	.85546	3.20032	.19784	
	29	2.43190	.90425	5.59167	1.10913		21	1.90684	.85297	3.38010	.197441	
	30	2.52313	.90613	6.03330	1.12920		22	1.95241	.85105	3.69573	1.00000	
	31	2.62341	.91266	6.53435	1.15878		23	2.02089	.84970	3.92338	1.02468	
	32	2.73341	.91787	7.10806	1.16787		24	2.06661	.84891	4.18336	1.04892	
	33	2.82540	.92379	7.77189	1.18593		25	2.14801	.84867	4.46089	1.07156	
	34	2.99197	.93046	8.54944	1.20476		26	2.21751	.84899	4.76346	1.09387	
	35	3.14654	.93789	9.47325	1.22260		27	2.29186	.84987	5.10146	1.11548	
	36	3.34375	.94815	10.56984	1.24008		28	2.37187	.85130	5.47426	1.13643	
	37	3.53011	.95527	11.96675	1.25720		29	2.45751	.85330	5.89051	1.15682	
	38	3.77508	.96938	13.70921	1.27399		30	2.55070	.85588	6.37861	1.17661	
	39	4.07307	.97635	15.96824	1.29048		31	2.62238	.85905	6.88921	1.19588	
	40	4.44728	.98845	19.09064	1.30667		32	2.76430	.86222	7.49464	1.21464	
	41	4.93820	1.00170	23.76779	1.32265		33	2.88785	.86721	8.19757	1.23893	
	42	5.66487	1.01619	30.63690	1.33866		34	3.02637	.87222	9.01808	1.25079	
	43	6.69829	1.03204	43.38530	1.35863		0	1.07115	.87796	9.99121	1.26922	
	44	8.69172	1.04940	73.38936	1.36868		1	1.36130	.88437	11.16501	1.26587	
	0	1.08636	1.08636	1.00000	0	69	2	1.56911	.89152	12.60945	1.30195	
	1	1.11808	1.06913	.07899			3	1.68156	.89944	14.43171	1.31288	
	2	1.15002	1.04340	1.14073	.19203		4	1.71348	.90820	15.80390	1.33468	
	3	1.18225	1.02474	1.21505	.23579		5	1.84692	.91782	20.08153	1.34998	
	4	1.21482	1.00770	1.29222	.26887		6	1.97351	.92789	24.63806	1.36539	
	5	1.24780	.99213	1.37250	.31178		7	2.10747	.93997	31.82475	1.38053	
	6	1.28120	.97773	1.45602	.36687		8	2.24778	.94284	44.56641	1.39542	
	7	1.31523	.96487	1.54335	.44873		9	2.38785	.95264	53.3937	1.41006	
	8	1.34982	.95896	1.63449	.49748		10	2.53437	.96350	73.3937	1.42477	
	9	1.38909	.94213	1.78985	.53347		11	2.67298	.97796	1.00000	0	
	10	1.42113	.93223	1.88932	.58697		12	1.10473	1.04607	1.07431	.08699	
	11	1.45801	.92327	1.93479	.62619		13	1.13849	1.05334	1.15131	.16677	
	12	1.49583	.91514	2.04521	.66733		14	1.17248	1.06263	1.23120	.24025	
	13	1.53468	.90781	2.16160	.70457		15	1.20678	1.06389	1.33418	.30819	
	14	1.57467	.90123	2.26154	.74006		16	1.24146	1.06667	1.40050	.37122	
	15	1.61993	.89338	2.41466	.77395		17	1.27658	1.06998	1.49290	.42590	
	16	1.66958	.89022	2.59271	.80635		18	1.31281	1.07362	1.58421	.48469	
	17	1.70276	.88787	2.69973	.83738		19	1.34837	1.08234	1.68604	.53991	
	18	1.74864	.88197	2.85608	.86719		20	1.38237	1.09149	1.78478	.58418	
	19	1.79640	.87864	3.02345	.89573		21	1.42298	.90052	1.89230	.62952	
	20	1.84625	.87602	3.20294	.92326		22	1.46147	.89051	2.00520	.67231	
	21	1.89641	.87398	3.39662	.94976		23	1.50091	.88139	2.12398	.71277	
	22	1.95315	.87254	3.60444	.97532		24	1.54138	.87311	2.24918	.75112	
	25						25	1.58301	.86562	2.38143	.78753	

TABLE I.— VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES — Continued

θ (deg)	β (deg)	M_b	M_a	P_a P_b	$\frac{\Delta P_{sh}}{P_b}$ $\%_b$	θ (deg)	β (deg)	M_b	M_a	P_a P_b	$\frac{\Delta P_{sh}}{P_b}$ $\%_b$
69	15	1.62591	0.85887	2.52143	0.82217	71	3	1.16604	0.98126	1.29145	0.26920
16	1.67023	0.85882	2.66997	0.85118	1.20260	4	1.20260	0.96047	1.34176	.33760	
17	1.71611	0.84745	2.82795	0.88672	5	1.23951	0.94154	1.43579	.40521		
18	1.76372	0.84772	2.99643	0.91684	6	1.27684	0.92427	1.53378	.46712		
19	1.81325	0.83661	3.17635	0.94971	7	1.31463	0.90950	1.63105	.52578		
20	1.86490	0.83510	3.36974	0.97340	8	1.35311	0.89409	1.74297	.57971		
21	1.91892	0.83417	3.57758	1.00000	9	1.39220	0.88089	1.85492	.63012		
22	1.97558	0.82881	3.80196	1.04559	10	1.43197	0.86869	1.97206	.67129		
23	2.03219	0.82800	4.04907	1.09024	11	1.47280	0.85779	2.09776	.72164		
24	2.08912	0.82674	4.30955	1.07401	12	1.51449	0.84770	2.22507	.75336		
25	2.16478	0.82603	4.59891	1.09697	13	1.55727	0.83949	2.36271	.80273		
26	2.23568	0.82585	4.91372	1.11917	14	1.60124	0.83011	2.50737	.85998		
27	2.31139	0.82621	5.26577	1.14065	15	1.64653	0.82250	2.66104	.87525		
28	2.39261	0.82711	5.64126	1.16168	16	1.69333	0.81362	2.82401	.90676		
29	2.48029	0.82824	6.08824	1.18168	17	1.74175	0.80942	2.99750	.94063		
30	2.57516	0.83074	6.57643	1.20129	18	1.79200	0.80388	3.18269	.97100		
31	2.67879	0.83110	7.13007	1.22035	19	1.84426	0.79896	3.38091	1.00000		
32	2.79267	0.83682	7.73656	1.23298	20	1.89877	0.79464	3.59373	1.08773		
33	2.91883	0.83993	8.40634	1.25699	21	1.95579	0.79089	3.82897	1.05439		
34	3.05990	0.84485	9.35393	1.28461	22	2.01661	0.78771	4.07076	1.07971		
35	3.21035	0.84980	10.37199	1.30181	23	2.07888	0.78506	4.33962	1.10489		
36	3.40490	0.85180	11.60108	1.30861	24	2.14907	0.78099	4.63894	1.18779		
37	3.61415	0.86108	13.11538	1.32903	25	2.21556	0.76135	4.95112	1.25047		
38	3.86570	0.86868	15.00987	1.34103	26	2.28057	0.75027	5.30568	1.27235		
39	4.17105	0.87583	17.59364	1.35682	27	2.31073	0.74959	5.69551	1.19347		
40	4.55358	0.88439	20.91698	1.37224	28	2.35687	0.74952	6.12913	2.23390		
41	5.03564	0.89380	25.80296	1.38736	29	2.45085	0.74003	6.63167	1.83397		
42	5.74970	0.90413	33.44889	1.40421	30	2.65083	0.73099	7.16241	1.92888		
43	6.82003	0.91544	47.12910	1.41679	31	2.76121	0.72044	7.70532	1.27141		
44	8.80523	0.92782	78.67054	1.41112	32	2.88678	0.71841	8.50117	1.26916		
70	0	1.06418	1.06418	1.00000	0	3.01761	0.70690	9.33218	1.30700		
1	1.09590	1.03769	1.07737	0.99153	33	3.16927	0.69993	10.30995	1.32408		
2	1.13405	1.01384	1.15827	1.07580	34	3.34121	0.79352	11.47643	1.34071		
3	1.16883	0.99194	1.20704	1.20174	35	3.53978	0.79798	12.89486	1.32692		
4	1.20418	0.97213	1.38717	1.32233	36	3.76995	0.80242	14.65711	1.37274		
5	1.23990	0.95409	1.41710	1.38759	37	4.04566	0.80776	16.90714	1.38820		
6	1.27565	0.93764	1.51080	1.41816	38	4.38489	0.81379	19.88200	1.40330		
7	1.31270	0.92400	1.60894	1.50450	39	4.71267	0.81993	21.30995	1.42408		
8	1.34994	0.90580	1.71072	1.57724	40	4.81376	0.80487	24.00217	1.41808		
9	1.38786	0.89621	1.81769	1.60643	41	5.38613	0.80787	30.09139	1.44256		
10	1.42754	0.88110	1.93274	1.65386	42	6.20663	0.83646	40.01235	1.44674		
11	1.46606	0.87117	2.04753	1.69626	43	7.53549	0.84499	59.05905	1.46066		
12	1.50653	0.86550	2.17137	1.73736	44	10.30545	0.84192	110.60891	1.47432		
13	1.54805	0.85982	2.30216	1.78224	72	0	1.05116	1.05116	0		
14	1.59076	0.84788	2.44024	0.83307	1	1.08264	1.02154	1.08496	1.0196		
15	1.63475	0.84069	2.58643	0.84805	2	1.12618	0.99159	1.17240	1.19409		
16	1.68019	0.83423	2.74161	0.86332	3	1.16438	0.97059	1.26734	1.27778		
17	1.72722	0.82844	2.90670	0.91304	4	1.20213	0.94880	1.35830	1.35420		
18	1.77602	0.82330	3.08030	0.94331	5	1.24041	0.92693	1.45696	1.42426		
19	1.82677	0.81277	3.21719	0.97227	6	1.27910	0.91083	1.52984	1.48883		
20	1.87971	0.81485	3.47330	1.00000	7	1.31890	0.89432	1.60728	1.58081		
21	1.93506	0.81150	3.69055	1.02650	8	1.35892	0.87923	1.77966	1.63388		
22	1.99312	0.80872	3.92581	1.05216	9	1.39856	0.86543	1.97739	1.65448		
23	2.05121	0.80648	4.18053	1.07674	10	1.43982	0.85281	2.02036	1.70355		
24	2.11070	0.80478	4.45777	1.10042	11	1.48183	0.84112	2.15050	1.74590		
25	2.18704	0.80261	4.76088	1.12386	12	1.52509	0.83068	2.28775	1.79091		
26	2.26972	0.80297	5.09384	1.14531	13	1.56933	0.82108	2.43223	1.8078		
27	2.33736	0.80284	5.46154	1.16654	14	1.61452	0.81221	2.56956	1.86316		
28	2.40269	0.80324	5.86937	1.18788	15	1.66168	0.80418	2.74709	1.90391		
29	2.51077	0.80416	6.32624	1.20788	16	1.72008	0.79650	2.91930	1.93759		
30	2.60809	0.80561	6.81086	1.22658	17	1.76018	0.79031	3.10877	1.96977		
31	2.71456	0.80739	7.42463	1.24553	18	1.81218	0.78439	3.30719	1.00000		
32	2.81463	0.81212	8.02051	1.26324	19	1.86668	0.77909	3.50681	1.02890		
33	2.96148	0.81320	8.82847	1.28167	20	1.92273	0.77439	3.73432	1.05669		
34	3.10680	0.81683	9.77698	1.29903	21	1.98151	0.77026	3.97793	1.08316		
35	3.27182	0.82109	10.85776	1.31396	22	2.04382	0.76670	4.24135	1.10582		
36	3.45992	0.82598	12.16581	1.32448	23	2.10912	0.76367	4.58755	1.12325		
37	3.67970	0.83142	13.78232	1.34861	24	2.17814	0.76116	4.83980	1.15622		
38	3.94084	0.83756	15.83248	1.36439	25	2.25136	0.75916	5.18006	1.17869		
39	4.25893	0.84441	18.51961	1.37928	26	2.34936	0.75765	5.55920	1.20035		
40	4.65930	0.85199	22.19785	1.39493	27	2.44285	0.75666	5.97030	1.22183		
41	5.18634	0.86133	27.54332	1.40974	28	2.50259	0.75515	6.44239	1.24146		
42	5.92732	0.86934	36.02968	1.42427	29	2.59964	0.75313	6.96494	1.26090		
43	7.08784	0.87952	51.59763	1.43853	30	2.70923	0.75229	7.52906	1.27977		
44	9.32463	0.89066	89.41117	1.45254	31	2.80267	0.75154	8.21035	1.29806		
71	0	1.05762	1.05762	1.00000	0	33	2.94833	0.75059	9.00756	1.31451	
1	1.09363	1.02952	1.08079	1.08453	1.18416	34	3.09059	0.74994	9.91359	1.33204	
2	1.12974	1.00419	1.16453	1.18416		35	3.25068	0.74939	10.98415	1.34979	

NACA

TABLE I.—VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES—Continued

θ (deg)	β (deg)	M_b	M_a	P_a P_b	$\frac{dp_{a,b}}{q_b}$	θ (deg)	β (deg)	M_b	M_a	P_a P_b	$\frac{dp_{a,b}}{q_b}$
72	35	3.43290	0.76637	12.26933	1.36609	74	26	2.63118	0.70929	7.29563	1.29930
	36	3.64351	.76988	13.84205	1.38197		29	2.74053	.70845	7.92987	1.31813
	37	3.89188	.77395	15.81213	1.39745		30	2.86021	.70805	8.03216	1.33692
	38	1.18935	.77649	18.35282	1.41255		31	2.99222	.70811	9.46534	1.35389
	39	4.55839	.78383	21.76052	1.42730		32	3.13923	.70883	10.49639	1.37091
	40	5.03335	.78569	26.56793	1.44173		33	3.30454	.70959	11.69397	1.38740
	41	5.87920	.79621	33.86900	1.45984		34	3.49240	.71102	12.96191	1.40339
	42	6.63532	.80342	42.29378	1.46866		35	3.70963	.71292	14.66843	1.42893
	43	8.27973	.81137	72.17362	1.48320		36	3.96507	.71589	16.78188	1.44303
	44	1.04569	1.04569	1.00000	0		37	4.27222	.71815	19.50936	1.46873
73	0	1.04569	1.04569	1.00000	0	75	39	4.65840	.72151	23.18702	1.46304
	1	1.05397	1.05397	1.06599	.10202		40	5.00687	.72880	36.18410	1.49061
	2	1.12402	.98680	1.18132	.08052		41	6.79229	.73477	49.56836	1.50391
	3	1.15113	.96009	1.27177	.09267		42	8.49003	.74033	77.53807	1.51692
	4	1.20286	.93705	1.37706	.07229		43	1.03226	1.03226	1.00000	0
	5	1.24271	.91618	1.48105	.04499		44	1.07856	.99910	1.09961	.12222
	6	1.28288	.89721	1.58995	.01166		45	1.12179	.96107	1.20315	.23060
	7	1.32373	.87993	1.70293	.73707		46	1.16933	.95853	1.31088	.32718
	8	1.36318	.86116	1.82162	.62964		47	1.20854	.91894	1.42319	.41392
	9	1.40719	.84974	1.94606	.56922		48	1.29231	.88390	1.54043	.49229
74	10	1.45006	.83908	2.07677	.73256	75	49	1.29649	.88906	1.66300	.56348
	11	1.49385	.82448	2.21348	.77735		50	1.34120	.89016	1.79136	.62848
	12	1.53853	.81330	2.38984	.88009		51	1.38652	.83896	1.96601	.68810
	13	1.58466	.80333	2.51086	.88009		52	1.43266	.81277	2.06752	.74301
	14	1.63193	.79409	2.67460	.89436		53	1.47966	.80295	2.21691	.79377
	15	1.68063	.78566	2.84700	.93414		54	1.52767	.78984	2.37369	.84067
	16	1.73098	.77799	3.03020	.98796		55	1.57685	.77783	2.53987	.88472
	17	1.78310	.77102	3.22262	1.00000		56	1.62733	.76586	2.71304	.92566
	18	1.83722	.76473	3.43165	1.03043		57	1.67903	.75668	2.89209	.96384
	19	1.89357	.75907	3.65894	1.05937		58	1.73466	.74247	3.10000	1.00000
75	20	1.95539	.75401	3.90033	.98696	76	59	1.79368	.74760	3.31456	1.03329
	21	2.01800	.74593	4.15104	1.11330		60	1.85834	.73919	3.51210	1.06886
	22	2.07872	.74560	4.44156	1.13849		61	1.91438	.73151	3.78644	1.09609
	23	2.14695	.74220	4.75121	1.18682		62	1.96569	.72453	4.04968	1.12475
	24	2.21914	.73932	5.08756	1.18776		63	1.96812	.71820	4.23211	1.15915
	25	2.29582	.73562	5.45696	1.20793		64	2.03345	.71247	4.32487	1.17783
	26	2.37763	.73507	5.86488	1.22238		65	2.10206	.70733	4.45313	1.20280
	27	2.46332	.73166	6.21798	1.24998		66	2.17437	.70274	4.59717	1.22665
	28	2.55680	.73274	6.62454	1.26504		67	2.25026	.69688	5.34815	1.24988
	29	2.66217	.73269	7.39491	1.28903		68	2.33211	.69513	5.73346	1.28988
76	30	2.77382	.73231	8.04216	1.30758	77	69	2.41680	.69207	6.20177	1.27025
	31	2.86647	.73260	8.78447	1.32554		70	2.51174	.68949	6.70059	1.29061
	32	3.03231	.73376	9.63176	1.34289		71	2.61193	.68737	7.29935	1.31072
	33	3.18421	.73392	10.65120	1.35982		72	2.72057	.68670	7.88996	1.32984
	34	3.35599	.73713	11.81957	1.37621		73	2.83916	.68449	8.60767	1.34826
	35	3.55267	.73954	13.29968	1.39215		74	2.96960	.68371	9.42424	1.36603
	36	3.78166	.74246	15.09258	1.40766		75	3.11451	.68337	10.30777	1.38318
	37	4.05344	.74990	17.36356	1.42276		76	3.27645	.68247	12.31871	1.39777
	38	4.38416	.74688	20.30479	1.43749		77	3.46086	.68100	12.86632	1.41982
	39	4.79990	.75141	24.11461	1.45286		78	3.67152	.68047	14.50661	1.44138
77	40	5.34654	.75551	30.33268	1.46989	78	79	3.91840	.68039	16.34697	1.46448
	41	6.11280	.76923	39.71928	1.47962		80	4.21282	.68082	19.19633	1.48113
	42	7.31380	.77153	56.90569	1.49304		81	4.57470	.68027	22.61361	1.47338
	43	9.61969	.77860	98.56603	1.50619		82	5.03507	.68337	27.41609	1.48929
	44	1.04030	1.04030	1.00000	0		83	6.58889	.70042	46.23278	1.51592
	45	1.06137	1.06137	1.09531	.11176		84	7.96838	.70471	68.94512	1.52977
	46	1.12243	.97646	1.19148	.21712		85	1.03061	1.03061	1.00000	0
	47	1.16558	.94940	1.29290	.30905		86	1.07648	.99179	1.10613	.13086
	48	1.20491	.92914	1.39821	.39211		87	1.18221	.99764	1.21660	.24571
	49	1.24184	.83373	2.00221	.71163		88	1.18798	.92737	1.33171	.34738
78	50	1.24661	.90321	1.30868	.46756	79	89	1.21390	.90036	1.45159	.43806
	51	1.28868	.88333	1.62362	.53658		90	1.26011	.87613	1.57743	.51950
	52	1.33127	.86923	1.73490	.59964		91	1.30675	.85428	1.70892	.59309
	53	1.37447	.84878	1.86594	.65783		92	1.35393	.83451	1.84682	.66993
	54	1.41841	.83373	2.00221	.71163		93	1.40180	.81657	1.99171	.74026
	55	1.46318	.81977	2.11129	.76155		94	1.45048	.80023	2.11422	.71694
	56	1.50891	.80738	2.28780	.80502		95	1.50012	.75932	2.30509	.82850
	57	1.55273	.79586	2.44216	.81741		96	1.55087	.77170	2.47511	.87616
	58	1.60358	.78218	2.60514	.89190		97	1.60284	.75924	2.65280	.92039
	59	1.65317	.77566	2.77956	.93021		98	1.65265	.74783	2.84642	.96156
79	60	1.70411	.76684	2.96390	.96611	80	99	1.70126	.73773	3.04994	1.00000
	61	1.75876	.75879	3.16033	1.00000		100	1.75032	.72770	3.26602	1.03583
	62	1.81132	.75146	3.37020	1.03044		101	1.80087	.71740	3.45958	1.06980
	63	1.86801	.74481	3.59206	1.06241		102	1.88812	.71106	3.74909	1.10162
	64	1.92108	.73861	3.83673	1.09125		103	1.95183	.70376	4.01779	1.13164
	65	1.98683	.73341	4.09738	1.11868		104	2.08825	.69109	4.62314	1.18693
	66	2.05355	.72596	4.37946	1.14423		105	2.16174	.68565	5.06521	1.21287
	67	2.12164	.72431	4.62594	1.16978		106	2.23938	.68076	5.34155	1.23676
	68	2.19353	.72056	5.02033	1.19367		107	2.01842	.69711	5.30816	1.21602
	69	2.26771	.71735	5.36688	1.21651		108	2.08825	.69109	5.62314	1.24747
80	70	2.35078	.71162	5.79702	1.23245	81	109	2.16741	.68565	5.96521	1.27427
	71	2.43746	.71237	6.23211	1.22951		110	2.23938	.68076	5.34155	1.23676

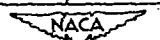


TABLE I.—VALUES OF JET NOSE NUMBER, PRESSURE RATIO, AND
 PRESSURE COEFFICIENT ALONG SHOCK WAVES—Continued

θ (deg)	β (deg)	η_0	η_s	$\frac{P_s}{P_0}$	$\frac{\Delta P_{sh}}{P_0}$	θ (deg)	β (deg)	η_0	η_s	$\frac{P_s}{P_0}$	$\frac{\Delta P_{sh}}{P_0}$
76	23	0.32175	0.67660	5.75480	1.3994	78	20	0.42213	0.63503	6.30199	1.10073
	24	0.40571	0.67273	6.20269	1.2803		21	0.42230	0.63515	6.30326	1.10087
	25	0.49040	0.66919	6.75742	1.20260		22	0.42230	0.63515	6.30326	1.10087
	26	0.58064	0.66569	7.30271	1.15235		23	0.42230	0.63515	6.30326	1.10087
	27	0.72413	0.66215	7.85388	1.10288		24	0.42230	0.63515	6.30326	1.10087
	28	0.83358	0.65865	8.40592	1.05295		25	0.42230	0.63515	6.30326	1.10087
	29	0.91350	0.65497	9.48769	1.00287		26	0.42230	0.63515	6.30326	1.10087
	30	1.05931	0.65115	10.49638	1.05260		27	0.42230	0.63515	6.30326	1.10087
	31	1.27831	0.64746	11.59455	1.10238		28	0.42230	0.63515	6.30326	1.10087
	32	1.46503	0.64377	12.69229	1.15216		29	0.42230	0.63515	6.30326	1.10087
	33	1.65670	0.63994	13.79082	1.20194		30	0.42230	0.63515	6.30326	1.10087
	34	1.84288	0.63603	14.88953	1.25172		31	0.42230	0.63515	6.30326	1.10087
	35	1.98148	0.63215	15.98826	1.30149		32	0.42230	0.63515	6.30326	1.10087
	36	2.13027	0.62826	17.08700	1.35127		33	0.42230	0.63515	6.30326	1.10087
	37	2.27943	0.62434	18.18573	1.40105		34	0.42230	0.63515	6.30326	1.10087
	38	2.42850	0.62043	19.28446	1.45083		35	0.42230	0.63515	6.30326	1.10087
	39	2.57752	0.61651	20.38319	1.50061		36	0.42230	0.63515	6.30326	1.10087
	40	2.72659	0.61258	21.48192	1.55039		37	0.42230	0.63515	6.30326	1.10087
	41	2.87566	0.60868	22.58065	1.60017		38	0.42230	0.63515	6.30326	1.10087
	42	3.02472	0.60476	23.67938	1.65005		39	0.42230	0.63515	6.30326	1.10087
	43	3.17378	0.60084	24.77811	1.70003		40	0.42230	0.63515	6.30326	1.10087
	44	3.32284	0.59692	25.87684	1.75001		41	0.42230	0.63515	6.30326	1.10087
	45	3.47190	0.59299	26.97557	1.80000		42	0.42230	0.63515	6.30326	1.10087
	46	3.62106	0.58897	28.07430	1.85000		43	0.42230	0.63515	6.30326	1.10087
	47	3.76911	0.58495	29.17303	1.90000		44	0.42230	0.63515	6.30326	1.10087
	48	3.91816	0.58093	30.27176	1.95000		45	0.42230	0.63515	6.30326	1.10087
	49	3.06721	0.57691	31.37049	2.00000		46	0.42230	0.63515	6.30326	1.10087
	50	3.21627	0.57289	32.46922	2.05000		47	0.42230	0.63515	6.30326	1.10087
	51	3.36533	0.56887	33.56795	2.10000		48	0.42230	0.63515	6.30326	1.10087
	52	3.51438	0.56485	34.66668	2.15000		49	0.42230	0.63515	6.30326	1.10087
	53	3.66344	0.56083	35.76541	2.20000		50	0.42230	0.63515	6.30326	1.10087
	54	3.81249	0.55681	36.86414	2.25000		51	0.42230	0.63515	6.30326	1.10087
	55	3.96155	0.55279	37.96287	2.30000		52	0.42230	0.63515	6.30326	1.10087
	56	4.11060	0.54877	39.06160	2.35000		53	0.42230	0.63515	6.30326	1.10087
	57	4.25965	0.54475	40.15933	2.40000		54	0.42230	0.63515	6.30326	1.10087
	58	4.40870	0.54073	41.25806	2.45000		55	0.42230	0.63515	6.30326	1.10087
	59	4.55775	0.53671	42.35679	2.50000		56	0.42230	0.63515	6.30326	1.10087
	60	4.70680	0.53269	43.45552	2.55000		57	0.42230	0.63515	6.30326	1.10087
	61	4.85585	0.52867	44.55425	2.60000		58	0.42230	0.63515	6.30326	1.10087
	62	5.00490	0.52465	45.65298	2.65000		59	0.42230	0.63515	6.30326	1.10087
	63	5.15395	0.52063	46.75171	2.70000		60	0.42230	0.63515	6.30326	1.10087
	64	5.30299	0.51661	47.85044	2.75000		61	0.42230	0.63515	6.30326	1.10087
	65	5.45204	0.51259	48.94917	2.80000		62	0.42230	0.63515	6.30326	1.10087
	66	5.60109	0.50857	50.04790	2.85000		63	0.42230	0.63515	6.30326	1.10087
	67	5.75014	0.50455	51.14663	2.90000		64	0.42230	0.63515	6.30326	1.10087
	68	5.89919	0.50053	52.24536	2.95000		65	0.42230	0.63515	6.30326	1.10087
	69	6.04824	0.49651	53.34409	3.00000		66	0.42230	0.63515	6.30326	1.10087
	70	6.19729	0.49249	54.44282	3.05000		67	0.42230	0.63515	6.30326	1.10087
	71	6.34634	0.48847	55.54155	3.10000		68	0.42230	0.63515	6.30326	1.10087
	72	6.49539	0.48445	56.64028	3.15000		69	0.42230	0.63515	6.30326	1.10087
	73	6.64444	0.48043	57.73891	3.20000		70	0.42230	0.63515	6.30326	1.10087
	74	6.79349	0.47641	58.83764	3.25000		75	0.42230	0.63515	6.30326	1.10087
	75	6.94254	0.47239	59.93637	3.30000		76	0.42230	0.63515	6.30326	1.10087
	76	7.09159	0.46837	61.03510	3.35000		77	0.42230	0.63515	6.30326	1.10087
	77	7.24064	0.46435	62.13383	3.40000		78	0.42230	0.63515	6.30326	1.10087
	78	7.38969	0.46033	63.23256	3.45000		79	0.42230	0.63515	6.30326	1.10087
	79	7.53874	0.45631	64.33129	3.50000		80	0.42230	0.63515	6.30326	1.10087

TABLE I.—VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES—Continued

θ (deg)	δ (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\alpha_{a,b}}{q_b}$	θ (deg)	δ (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\alpha_{a,b}}{q_b}$	
80	26	3.36182	-0.56747	12.62123	1.46954	83	0	1.00751	1.00751	1.00000	0	
	27	3.37242	-0.56403	14.27360	1.48592		1	1.09383	.93218	1.20849	.24893	
	28	3.61551	.56059	13.30365	1.50193		2	1.27698	.87206	1.13090	.44286	
	29	4.10344	.55835	18.86699	1.51733		3	1.26372	.82273	1.66983	.59639	
	30	4.44585	.55610	22.19783	1.53209		4	1.34874	.76138	1.92411	.72572	
	31	4.87369	.55421	26.70940	1.54624		5	1.43464	.74634	2.19890	.83214	
	32	5.12791	.55259	33.16942	1.55964		6	1.52986	.73570	2.49570	.92242	
	33	6.19057	.55153	43.19444	1.57292		7	1.61134	.69911	2.81748	1.00000	
	34	7.34537	.55072	60.88809	1.59552		8	1.70348	.66568	3.16775	1.05743	
	35	9.43104	.55025	100.47898	1.59767		9	1.79843	.64487	3.55072	1.12661	
	81	0	1.01247	1.01247	1.00000		10	1.87748	.62627	3.97144	1.17901	
	1	1.08029	.59273	1.16228	.98933		11	2.00118	.60955	4.13611	1.22574	
	2	1.18803	.90300	1.33333	.96130		12	2.11041	.59447	4.95229	1.26770	
	3	1.21520	.86093	1.51100	.97285		13	2.22621	.58080	5.22474	1.30562	
	4	1.26848	.62457	1.70929	.63296		14	2.34981	.56838	6.17952	1.34007	
	5	1.35020	.79307	1.90317	.71166		15	2.48270	.55705	6.91764	1.37152	
	6	1.41668	.76247	2.12398	.79779		16	2.62677	.54671	7.16366	1.40036	
	7	1.48224	.74071	2.35410	.87339		17	2.78134	.53725	8.14365	1.42693	
	8	1.55918	.73880	2.60016	.94031		18	2.95847	.52858	9.05298	1.45189	
	9	1.63184	.69915	2.88404	1.00000		19	3.15317	.52004	11.26064	1.47428	
	10	1.70656	.68144	3.14793	1.05361		20	3.37388	.51336	12.91636	1.49550	
	11	1.78371	.66942	3.45440	1.10204		21	3.62824	.50688	14.56338	1.51531	
	12	1.86370	.65087	3.78664	1.14604		22	3.92270	.50018	17.51852	1.53360	
	13	1.94698	.63763	4.14761	1.18621		23	4.28613	.49496	20.56744	1.55127	
	14	2.03408	.62354	4.54266	1.22306		24	4.73801	.49261	23.63451	1.56767	
	15	2.12558	.61449	4.97544	1.25699		25	5.32518	.48517	32.42573	1.58314	
	16	2.22218	.60438	5.45345	1.28837		26	6.14449	.48093	43.22632	1.59771	
	17	2.32169	.59111	5.98393	1.31748		27	7.41885	.47703	63.09215	1.61163	
	18	2.43409	.58662	6.57641	1.34458		28	9.86743	.47342	111.74018	1.62480	
	19	2.53155	.57883	7.24934	1.36968		84	0	1.00551	1.00551	1.00000	0
	20	2.67718	.77161	7.99053	1.39334		1	1.19255	.91901	1.24370	.28484	
	21	2.81680	.56917	8.86354	1.41503		2	1.20403	.89207	1.30615	.49878	
	22	2.96887	.56259	9.86353	1.43877		3	1.30210	.79835	1.78977	.66545	
	23	3.13708	.55716	11.03386	1.45693		4	1.40075	.75410	2.09743	.79902	
	24	3.32953	.54882	12.42986	1.47361		5	1.50063	.71689	2.43252	.90893	
	25	3.54049	.54434	14.09971	1.49292		6	1.60319	.68510	2.79315	1.00000	
	26	3.78811	.54030	16.18903	1.50973		7	1.70869	.67128	3.20220	1.07758	
	27	4.07944	.53668	18.77364	1.52973		8	1.81113	.63320	3.64771	1.14426	
	28	4.43060	.53346	22.17882	1.54098		9	1.93368	.61223	4.14307	1.20221	
	29	4.86743	.53063	26.79740	1.55953		10	2.05312	.59336	4.69748	1.25307	
	30	5.43471	.52817	33.44887	1.56945		11	2.18107	.57616	5.32259	1.29610	
	31	6.21880	.52607	43.84824	1.58278		12	2.31797	.56185	6.63330	1.33826	
	32	7.41570	.52433	62.46239	1.59557		13	2.46747	.54752	6.84903	1.37433	
	33	9.61661	.52292	109.08934	1.60766		14	2.66881	.53507	7.79953	1.40462	
	82	0	1.00983	1.00983	1.00000		15	2.80428	.52373	8.90771	1.43652	
	1	1.08989	.94136	1.18238	.82096		16	3.00225	.51342	10.83417	1.46355	
	2	1.16106	.88669	1.37561	.89604		17	3.22630	.50399	11.84448	1.48834	
	3	1.23989	.84318	1.55802	.94323		18	3.48487	.49535	13.84205	1.51117	
	4	1.31088	.80449	1.79930	.66449		19	3.78761	.48744	16.38441	1.53228	
	5	1.38645	.77094	2.03652	.70734		20	4.15390	.48019	19.74410	1.55187	
	6	1.46004	.74207	2.28218	.8574		21	4.61191	.47341	24.37688	1.57010	
	7	1.54104	.71648	2.55026	.93257		22	5.21284	.46744	31.18958	1.58712	
	8	1.62087	.69379	2.83905	1.00000		23	6.04172	.46177	41.95408	1.60280	
	9	1.70597	.67352	3.15125	1.09369		24	7.40162	.45673	63.04960	1.61803	
	10	1.78780	.65933	3.43004	1.11294		25	10.10199	.45480	117.59103	1.63212	
	11	1.87587	.63893	3.65950	1.16075		26	1.00392	1.00392	1.00000	0	
	12	1.96776	.62407	4.26328	1.20359		27	1.18109	.90298	1.29371	.32466	
	13	2.06412	.61058	4.70774	1.24320		28	1.24128	.82102	1.61438	.57056	
	14	2.16569	.59889	5.38927	1.27904		29	1.35748	.76828	1.56621	.71924	
	15	2.27337	.58706	5.74613	1.31319		30	1.47948	.75391	2.35391	.88844	
	16	2.38822	.57680	6.35862	1.34217		31	1.60374	.68174	2.78387	1.00000	
	17	2.51150	.56740	7.04792	1.37016		32	1.72126	.64870	3.26362	1.09187	
	18	2.64422	.55879	7.83617	1.39612		33	1.85197	.60041	3.80263	1.16768	
	19	2.79013	.55089	8.73972	1.42089		34	1.98883	.55586	4.13105	1.23265	
	20	2.94995	.54369	9.78928	1.44286		35	2.13493	.57436	5.11052	1.26834	
	21	3.12533	.53694	11.00824	1.46375		36	2.29200	.55535	5.91560	1.33674	
	22	3.30734	.53095	12.40953	1.48381		37	2.46261	.53823	6.85590	1.37922	
	23	3.55722	.52859	13.29389	1.50732		38	2.65087	.52326	7.96937	1.41683	
	24	3.81669	.52035	16.52503	1.52013		39	2.85089	.50964	9.30959	1.49037	
	25	4.13307	.51573	19.37661	1.53692		40	3.09929	.49731	10.95474	1.48050	
	26	4.21462	.51158	23.15118	1.55261		41	3.37530	.48612	13.02379	1.50771	
	27	4.49958	.50763	28.36911	1.56761		42	3.70268	.47594	15.70654	1.53244	
	28	5.63407	.50447	36.14927	1.58158		43	4.10319	.46666	19.38633	1.55001	
	29	6.45408	.50189	40.84302	1.59542		44	4.61399	.45817	24.48172	1.57572	
	30	8.01831	.49827	73.36928	1.60646		45	5.30513	.45040	32.41900	1.59479	



TABLE I.—VALUES OF LOCAL MACH NUMBER, PRESSURE RATIO, AND
PRESSURE COEFFICIENT ACROSS SHOCK WAVES — Concluded

θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_{a,b}}{q_b}$	θ (deg)	β (deg)	M_b	M_a	$\frac{P_a}{P_b}$	$\frac{\Delta P_{a,b}}{q_b}$
85	20	6.33047	0.44327	16.23224	1.61242	87	5	2.01901	0.58198	4.54750	1.25076
	21	5.12762	.43674	16.31580	1.62876		6	2.28571	0.51608	5.78317	1.23156
86	0	1.00244	1.00000	0	0	7	2.50093	0.48246	7.08269	1.20371	
1	1.15055	.87934	1.37080	.39921		8	2.81262	0.42410	9.87715	1.15677	
2	1.28551	.79401	1.78307	.05612		9	3.23409	0.47324	12.00848	1.30273	
3	1.44179	.78527	2.24673	.05980		10	3.78118	.45507	25.94670	1.34176	
4	1.59085	.67901	2.77153	1.00000		11	4.38111	.43910	22.16916	1.37728	
5	1.74555	.63805	3.37086	1.11156		12	5.37539	.48409	33.44909	1.36442	
6	1.90650	.60405	4.06208	1.20096		13	7.80410	.41238	60.21636	1.42999	
7	2.08259	.57589	4.86077	1.28748		14	13.86155	.40059	904.45147	1.05262	
8	2.27139	.55060	5.8213	1.33251	88	0	1.00061	1.00061	1.00000	0	
9	2.47941	.53814	6.97050	1.38744		1	1.49222	.79113	1.77309	.66653	
10	2.71274	.51031	8.37701	1.45208		2	1.58155	.67540	2.75534	1.00000	
11	2.97592	.49369	10.14682	1.47087		3	1.69445	.59961	4.01932	1.20029	
12	3.29358	.47880	12.42731	1.50911		4	2.24473	.54437	5.70487	1.31388	
13	3.67355	.46548	15.50082	1.53505		5	2.66202	.50254	8.09068	1.42944	
14	4.15389	.45349	19.86017	1.56394		6	3.19358	.46933	11.17174	1.50122	
15	4.79538	.44264	26.53113	1.58608		7	3.93732	.44219	17.89540	1.57114	
16	5.73359	.43279	38.06839	1.60789		8	5.15650	.41520	50.61260	1.60396	
17	7.35053	.42382	62.56901	1.62771		9	8.01393	.40060	74.70644	1.63870	
18	11.43133	.41364	131.51613	1.64980	89	0	1.00015	1.00015	1.00000	0	
87	0	1.00137	1.00137	1.00000		1	1.58174	.67190	2.75333	1.00000	
1	1.15742	.84687	1.50153	.49959		2	2.52822	.52285	2.67634	1.53341	
2	1.39082	.74753	2.08399	.79976		3	3.17002	.46702	11.55363	1.20031	
3	1.58698	.67690	2.76207	1.00000		4	5.03780	.41669	89.43369	1.60049	
	1.79219	.63346	3.57035	1.14321							

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